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Geometric uncertainty in intracranial aneurysm rupture status discrimination: a two-site retrospective study.

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Abstract

Objectives: Assessing the risk associated with unruptured intracranial aneurysms (IA) is essential in clinical decision making. Several geometric risk parameters have been proposed for this purpose. However, performance of these parameters has been inconsistent. This study evaluates the performance and robustness of geometric risk parameters on two datasets and compare it to the uncertainty inherent in assessing these parameters and quantifies inter-parameter correlations.

Methods: Two datasets containing 244 IA geometries from 178 patients were retrospectively analyzed. IAs were stratified by anatomical region, based on the PHASES score locations. 37 geometric risk parameters representing four groups (size, neck, non-dimensional, and curvature parameters) were assessed. Analysis included standardized absolute differences (SAD) between ruptured and unruptured IAs, ratios of SAD to median relative uncertainty (MRU) associated with the parameters, and inter-parameter correlation.

Results: The ratio of SAD to MRU was lower for higher-dimensional size parameters (i.e., areas and volumes) than for one-dimensional size parameters. Non-dimensional size parameters performed comparatively well with regard to SAD and MRU. SAD was higher in the posterior anatomical region. Correlation of parameters was strongest within parameter (sub)groups and between size and curvature parameters, while anatomical region did not strongly affect correlation patterns.

Conclusion: Non-dimensional parameters and few parameters from other groups were comparatively robust, suggesting that they might generalize better to other datasets. The data on discriminative performance and inter-parameter correlations presented in this study may aid in developing and choosing robust geometric risk parameters for use in rupture risk models.

Introduction

A relevant part of the general population harbors one or more unruptured intracranial aneurysms (IAs), with the overall prevalence estimated around 3% [1]. While most IAs do not rupture [2], the question of whether and when to treat them remains relevant due to the poor prognosis of ruptured IAs [3, 4] as well as the risk of intervention [3, 5]. Current American Heart Association/American Stroke Association guidelines list several modifiable and non-modifiable risk factors for IA growth and/or rupture, including IA location, growth rate, morphology, smoking status, alcohol consumption, hypertension, age, sex, previous IA, and family history [6]. Attempts have been made to develop scoring systems to quantify rupture risk, growth risk, and/or support treatment decisions, these include the PHASES score by Greving et al. [7], the UIATS by Etminan et al. [8] and the ELAPSS score by Backes et al. [9]. All three of these scores are based on clinically available data and all include geometric rupture risk parameters: IA size in case of the PHASES score [7], surface irregularity, size ratio, as well as aspect ratio in case of the UIATS [8], and IA size as well as surface irregularity for the ELAPSS score [9]. While these metrics were designed to support clinical decision making, performance on clinical data has been mixed [10-12] and improvements, particularly for patients harboring multiple IAs, are desired by clinicians [13].

The aim of this paper is to assess the ability of a broad number of proposed geometric risk parameters to differentiate between unruptured and ruptured IAs while also comparing their discriminative ability relative to the uncertainty encountered in determining them. Any acquisition of patient-specific IA geometries and subsequent use of these geometries to derive geometric risk parameters is affected by a number of uncertainty-introducing factors. Starting with the medical imaging acquisition itself, which is followed by image data pre-processing, segmentation, geometry reconstruction including post-processing (e.g., smoothing, checking of topology), and finally calculation of the geometric risk parameters. All these processing steps are associated with some errors, resulting in uncertainty, which negatively affects the ability of parameters to discriminate IA rupture status. Discrimination of rupture status on an individual IA level is, however, necessary if these parameters are to support the clinical decision-making process, including any decisions regarding treatment modalities. Previous studies found high variability in the uncertainty of different geometric risk parameters as well as differences in their ability to differentiate between ruptured and unruptured IAs [14-16]. Furthermore, for geometric risk parameters with multiple alternative definitions, the specific implementation can affect the discriminative performance of the parameter itself and any derived parameters, as demonstrated by Lauric et al. for parameters incorporating IA and neck size [17].

The current study was performed to facilitate optimal selection of geometric rupture risk parameters by identifying geometric parameters, which are good discriminators while also exhibiting low uncertainty. The analysis is performed on two datasets processed by different research groups and is differentiated by

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3 anatomical region, in order to assess how the predictive suitability of the geometric risk parameters is
4 affected by geometry processing as well as anatomical location. Additionally, correlation of the geometric
5 risk parameters with each other is assessed.
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Methods

Medical imaging data

IA geometries were retrospectively reconstructed and segmented from 3D rotational angiography data acquired for routine clinical indications. 142 IAs were acquired in the Helios Klinikum Berlin-Buch (Berlin, Germany), 38 in KRH Klinikum Nordstadt (Hanover, Germany), 23 in the University Medical Center Schleswig-Holstein (UKSH) (Kiel, Germany), and 41 in the University Hospital Magdeburg (Magdeburg, Germany). Processing of the imaging data, including segmentation, was performed at two sites: Berlin, which processed 142 IAs from Helios Klinikum Berlin-Buch (dataset 1), and Magdeburg, which processed 102 IAs from KRH Klinikum Nordstadt, UKSH, and University Hospital Magdeburg (dataset 2). Overall, 244 IAs from 178 patients were included, from which geometric risk parameters were subsequently calculated. Based on the PHASES score [7], aneurysm location was classified into four anatomical regions: internal carotid artery (ICA), middle cerebral artery (MCA), anterior region (all vessels anterior of the ICA/MCA), and posterior region (all vessels posterior of the ICA/MCA). The distribution of the individual IA locations and their assignment to the four anatomical regions are shown in Table 1.

Table 1: Frequency and rupture status of individual IA locations by dataset. ACA: anterior cerebral artery, AComA: anterior communicating artery, AChA: anterior choroidal artery, ICA: internal carotid artery, MCA: middle cerebral artery, PComA: posterior communicating artery, PCA: posterior cerebral artery, SCA: superior cerebellar artery, BA: basilar artery, PICA: posterior inferior cerebellar artery, VA: vertebral artery.

Anatomical region	Vessel	Dataset 1 unruptured	Dataset 1 ruptured	Dataset 2 unruptured	Dataset 2 ruptured
Anterior	ACA	3	1	2	2
	AComA	10	22	11	5
ICA	AChA	0	1	1	2
	ICA	29	8	19	4
MCA	MCA	28	10	31	8
Posterior	PComA	8	10	2	4
	PCA	0	1	0	0
	SCA	0	0	1	1
	BA	4	3	3	4
	PICA	0	4	1	0
	VA	0	0	0	1

Geometric risk parameters

Historically, a large number of geometric parameters for IA rupture risk assessment have been proposed. In order to have access to information on parameter uncertainty, the parameters chosen for this study were limited to a subset of the parameters reported in Goubergrits et al. [14], a parameter uncertainty study

performed on segmentation data obtained during the Multiple Aneurysms AnaTomy Challenge (MATCH) 2018 [18]. For a detailed description of the parameters and the rationale for choosing the parameters, the interested reader is referred to Goubergrits et al. [14]. Table 2 lists the geometric parameters and their abbreviations.

Table 2: List of the investigated geometric parameters, their descriptions, and median relative uncertainties (MRU). Note that terminology and implementation in the references might differ subtly. Derived and modified from tables 1-5 from Goubergrits et al. [14], used under Creative Commons Attribution License (CC BY 4.0). The CC BY 4.0 license text is available at <https://creativecommons.org/licenses/by/4.0/>.

Parameter group	Parameter name, unit [exemplary reference]	Parameter abbreviation	Short description	MRU
Size	Height, mm [19]	H	Maximum perpendicular distance from the neck plane to the aneurysm surface	0.140
	Maximum dimension, mm [20]	L_{\max}	Maximum distance between two points on the aneurysm surface	0.057
	Maximum height, mm [15]	H_{\max}	Maximum distance between the centroid of the neck and the aneurysm surface	0.057
	Maximum diameter, mm [17]	D_{\max}	Maximum neck plane-parallel distance between two points on the aneurysm surface	0.057
	Bulge height, mm [19]	H_b	Distance between the neck plane and the maximum diameter	0.057
	Surface area, mm ² [15]	A	Surface area of the aneurysm	0.057
	Convex hull surface area, mm ² [15]	A_{CH}	Surface area of the aneurysm's convex hull	0.057
	Minimal bounding sphere surface area, mm ² [21]	A_{MBS}	Surface area of the aneurysm's minimal bounding sphere	0.057
	Closed surface area, mm ²	A_{closed}	Surface area of the neck-closed aneurysm	0.083
	Volume, mm ³ [15]	V	Volume of the neck-closed aneurysm	0.092
	Convex hull volume, mm ³ [15]	V_{CH}	Volume of the aneurysm's convex hull	0.099
Minimal bounding sphere volume, mm ³ [21]	V_{MBS}	Volume of the aneurysm's minimal bounding sphere	0.051	
Neck	Minimum neck diameter, mm [17]	$D_{\text{neck,min}}$	Minimum distance between two opposite points on the neck perimeter	0.206
	Maximum neck diameter, mm [22]	$D_{\text{neck,max}}$	Maximum distance between two points on the neck perimeter	0.348
	Neck perimeter, mm [19]	P_{neck}	Perimeter of the aneurysm neck	0.374
	Equivalent neck diameter, mm [19]	$D_{\text{neck,equiv}}$	Hydraulic diameter of the aneurysm neck	0.276
	Neck area, mm ² [19]	A_{neck}	Area of the aneurysm neck	0.593

	Elliptical neck area, mm ²	$A_{\text{neck,elliptical}}$	Neck area calculated as the product of the minimum and maximum neck diameter	0.650
Non-dimensional	Aspect ratio [22]	AR	Ratio of height to maximum neck diameter	0.293
	Equivalent aspect ratio [19]	eAR	Ratio of height to equivalent neck diameter	0.326
	Bottleneck factor [19]	BF	Ratio of maximum diameter to maximum neck diameter	0.201
	Bulge location [19]	BL	Ratio of bulge height to height	0.001
	Nonsphericity index [15]	NSI	Normalized ratio of volume to surface area relative to a hemisphere	0.008
	Aneurysm volume to bounding sphere volume [21]	AVSV	Ratio of volume to minimal bounding sphere volume	0.073
	Aneurysm surface area to bounding sphere area [21]	AASA	Ratio of surface area to minimal bounding sphere surface area	0.005
	Undulation index [15]	UI	1 minus the ratio of volume to convex hull volume	0.009
	Ellipticity index [15]	EI	Normalized ratio of convex hull volume to convex hull surface area relative to a hemisphere	0.001
Curvature	Mean of mean curvature, mm ⁻¹ [19]	MAA	Surface average of local mean curvature	0.001
	Mean of absolute mean curvature, mm ⁻¹	absMAA	Surface average of the magnitude of the local mean curvature	0.001
	Standard deviation of mean curvature, mm ⁻¹	MSD	Standard deviation of the local mean curvature	1.000
	High mean curvature, % [21]	HMC	Relative increase of the mean of absolute mean curvature over the mean curvature of the minimal bounding sphere	0.001
	L2-norm of mean curvature [19]	MLN	Scale invariant measure of surface irregularity, uses mean curvature	0.001
	Mean of Gaussian curvature, mm ⁻² [19]	GAA	Surface average of local Gaussian curvature	0.001
	Mean of absolute Gaussian curvature, mm ⁻²	absGAA	Surface average of the magnitude of the local Gaussian curvature	0.001
	Standard deviation of Gaussian curvature, mm ⁻²	GSD	Standard deviation of the local Gaussian curvature	1.000
	High Gaussian curvature, % [21]	HGC	Relative increase of the mean of absolute Gaussian curvature over the Gaussian curvature of the minimal bounding sphere	0.822
L2-norm of Gaussian curvature [19]	GLN	Scale invariant measure of surface irregularity, uses Gaussian curvature	0.545	

Since the diameter of the parent vessel was not available for all IAs studied, size ratio could not be calculated and was excluded. Furthermore, UI and CR as well as NSI and NPR are directly related through $CR = 1 - UI$ and $IPR = \frac{\sqrt[3]{18\pi}}{1 - NSI}$, respectively. CR and IPR were therefore not included in the analysis, in order to avoid redundancy. Geometric risk parameters were calculated from the IA geometries using MATLAB (version R2017b, MathWorks, Natick, USA), Python (version 3.7.1, Python Software Foundation, Delaware, USA), and ZIBAmira (version 2015.28, Zuse Institute Berlin, Germany). The individual parameter values, IA location, and rupture status for each IA in this study, as well as the exact values of the inter-parameter correlation coefficients are provided as supplemental material 1 and 2 respectively.

Statistical analysis

Since most of the geometric risk parameters were non-normally distributed, as assessed by Q-Q plots and Shapiro-Wilk tests, the median was used to quantify central tendency and the interquartile range was used to quantify dispersion. Correlations were quantified using Pearson's r with correlations $|r| \geq 0.75$ referred to as strong, while those with $0.75 > |r| \geq 0.25$ and $|r| < 0.25$ referred to as moderate and weak, respectively. Statistical analysis was performed using SPSS (version 28.0.0.0, IBM, Armonk, USA) and MATLAB.

The discriminative ability of the individual parameters was assessed by standardizing the absolute difference between the medians of the ruptured and unruptured IAs with the weighted arithmetic mean of the IQRs of the two groups. This measure of effect size will be referred to as the standardized absolute group difference (SAD). Furthermore, the ratio of the SAD to the relative uncertainty, a measure of the uncertainty associated with parameter calculation, from Goubergrits et al. [14] was calculated for all parameters and will be referred to as the group difference-uncertainty ratio (DUR). The equations for SAD and DUR are thus $SAD = \frac{(n_r + n_u) \cdot |m_r - m_u|}{n_r IQR_r + n_u IQR_u}$ and $DUR = \frac{SAD}{MRU}$, where n_i , m_i , and IQR_i are the sample sizes, median values, and interquartile ranges of the ruptured (subscript r) and unruptured (subscript u) samples, while MRU is the median relative uncertainty from Goubergrits et al. [14], which is also listed in Table 2. SAD and DUR may take any value ≥ 0 with higher values indicating stronger discriminative ability and a better ratio of discriminative ability to uncertainty, respectively. SAD and DUR values of zero would indicate no discriminative ability and the worst possible ratio of discriminative ability to uncertainty, respectively. Additionally, the correlation coefficients between the parameters were calculated. Analysis of SAD and DUR as well as the correlation coefficients was performed individually for each anatomical region and each dataset.

Patient and public involvement

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3 Due to the purely retrospective manner of this study, no involvement of patients or the general public was
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Results

Error! Reference source not found. shows SAD for all geometric risk parameters by anatomical region and dataset. Considering both datasets, the following parameters achieved the comparatively highest SAD for each anatomical region: curvature (HMC, MLN, HGC, GLN) and non-dimensional (AR, eAR, AVSV, AASA) parameters in the anterior region, curvature (HMC, HGC) and non-dimensional (NSI, AASA, EI) parameters in the ICA, non-dimensional (AR, eAR, BL, AVSV, AASA) parameters in the MCA, and size (H , L_{\max} , A , A_{MBS}) and curvature (MSD, absGAA, GSD) parameters in the posterior region. Compared to the other anatomical regions, SAD was higher in the posterior region and more parameters exhibited relatively high SAD. Looking at all anatomical regions combined, curvature (HMC, MLN, absGAA, HGC, GLN) and non-dimensional (AR, eAR, AVSV, AASA) parameters as well as one neck ($D_{\text{neck,min}}$) and one size (H_b) parameter show comparatively high SAD in both datasets. Furthermore, the differences between the two datasets become less pronounced when combining all anatomical regions.

Error! Reference source not found. shows DUR for all geometric risk parameters by anatomical region and dataset. Considering both datasets, the following parameters achieved the comparatively highest DUR for each anatomical region: non-dimensional (AASA, EI) and one curvature (MLN) parameter in the anterior region, non-dimensional (EI, AASA, NSI) parameters in the ICA, non-dimensional (AASA, EI) parameters in the MCA, and size parameters (H , L_{\max} , H_{\max} , A), curvature (MAA, absMAA), and one non-dimensional (EI) parameter in the posterior region. Similar to SAD, DUR in the posterior region was overall higher and more parameters exhibited relatively high DUR, compared to the other anatomical regions. Looking at all anatomical regions combined, non-dimensional (NSI, AVSV, AASA, EI) and curvature (absMAA, MLN) parameters show comparatively high DUR in both datasets. As for SAD, the differences between the two datasets are less pronounced when looking at all anatomical regions combined.

Figures **Error! Reference source not found.** and **Error! Reference source not found.** show correlation coefficients between the geometric risk parameters by anatomical region for both datasets. The following general features are present in most data correlation plots: The size parameters (H , L_{\max} , H_{\max} , D_{\max} , H_b , A , A_{CH} , A_{MBS} , A_{closed} , V , V_{CH} , V_{MBS}) are generally strongly correlated with each other. Similarly, the neck parameters ($D_{\text{neck,min}}$, $D_{\text{neck,max}}$, P_{neck} , $D_{\text{neck,equiv}}$, A_{neck} , $A_{\text{neck,elliptical}}$) are also generally strongly correlated with each other.

Within the non-dimensional parameter group, there are two distinct subgroups in most plots: one formed by AR, eAR, BF, and BL and one formed by NSI, AVSV, AASA, UI, and EI. Within the latter subgroup, several of the correlations are negative but their magnitude is overall moderate to strong. The curvature parameters also form two subgroups, one formed by dimensional curvature parameters (MAA, absMAA, MDS, GAA, absGAA, GSD) and one by non-dimensional curvature parameters (HMC, MLN, HGC, GLN).

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3 With regard to correlations between parameter groups, there is generally moderate to strong correlation
4 between the size and neck parameters. Additionally, the size and neck parameters are generally moderately
5 correlated with the curvature parameters, the direction of the correlation being positive for the non-
6 dimensional curvature parameters and negative for the dimensional curvature parameters.
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Discussion

Previous research has assessed the impact of uncertainty on geometric risk parameters in a limited fashion. Ma et al. examined the influence of random noise on the calculation of 14 geometric risk parameters, finding curvature parameters more susceptible to random noise than size, neck, and non-dimensional parameters [19]. Others have examined the influence of imaging modality [23] and CT angiography reconstruction kernel [24] on geometric risk parameters. Regarding image acquisition, Ramachandran et al. have examined the influence of imaging modality [23], while O'Meara et al. [24] and Berg et al. [25] have focused on the reconstruction kernel's effect on geometric and hemodynamic risk parameters, respectively. Other sensitivity and uncertainty aspects of computational fluid dynamics approaches to IAs have been explored, e.g., by Cebral et al. [26], Sarrami-Foroushani et al. [27], and Schneiders et al. [28]. To the authors' knowledge there is, however, no comprehensive publication relating discriminative performance and uncertainty of geometric risk parameters, while also providing detailed data on their correlation with each other.

Looking at the parameter groups examined in this study, the following findings can be made: the size and neck parameters measuring areas (A , A_{CH} , A_{MBS} , A_{closed} , A_{neck} , $A_{neck,elliptical}$) and volumes (V , V_{CH} , V_{MBS}) generally do not achieve high DUR, despite having SAD similar to the size and neck parameters measuring length (H , L_{max} , H_{max} , D_{max} , H_b , $D_{neck,min}$, $D_{neck,max}$, P_{neck} , $D_{neck,equiv}$). The cause is the higher uncertainty encountered in determining the higher-dimensional parameters when compared to the one-dimensional parameters [14]. This suggests that higher-dimensional size parameters tend to be less robust and thus less suitable for use in practical risk models than one-dimensional size parameters. Similar to Lauric et al. [17], there are instances of noticeable differences in the discriminative performance of parameters capturing the same aspect of IA geometry, e.g. for the neck size parameters. The non-dimensional parameters exhibit comparatively high SAD and DUR, with the exception of BL and UI, which exhibit lower discriminative ability and/or higher uncertainty in their calculation. The curvature parameters show substantial variability in SAD and DUR depending on the anatomical region and the particular parameter, with MLN performing comparatively well overall. It is notable that the posterior region tends to exhibit higher SAD and DUR than the other regions, indicating more pronounced geometric differences between ruptured and unruptured IAs in this region. Regarding the differences in SAD and DUR between datasets 1 and 2, it is likely that differences in the patient collectives, subsample sizes, and reconstruction techniques are the main causes. The latter could in the future be tackled through the use of machine learning-based segmentation methods, which can reduce operator-induced uncertainty. Examples of such methods have previously been presented, e.g., in the context of the CADA challenge [29].

Regarding the correlation patterns, there is substantial similarity between all analyzed anatomical regions and datasets. Parameters tend to be most strongly correlated with other parameters from the same parameter

group, with the exception of the non-dimensional and curvature parameters, which form two subgroups each. This is reasonable, given that the parameters within each parameter group capture similar aspects of IA geometry. For the size and neck parameter groups this is fairly obvious, since they both capture aspects of IA and neck size, respectively. The two distinct correlation subgroups within the non-dimensional parameter group are likely caused by the underlying parameter subgroups capturing different aspects of aneurysm shape. While the parameters of the first subgroup (AR, eAR, BF, BL) are simply ratios of one-dimensional size parameters, the second subgroup (NSI, AVSV, AASA, UI, EI) is formed by parameters relating aneurysm area and/or volume to geometric reference objects, e.g., the minimal bounding sphere or convex hull. The negative correlation between AVSV and AASA with the other parameters from the second subgroup is due to the parameter definitions, which cause AVSV and AASA to increase with increasing sphericity, while the other parameters tend to decrease with increasing sphericity. The curvature parameters also form two subgroups, with the first subgroup consisting of the dimensional parameters quantifying the mean or dispersion of IA surface curvature (MAA, absMAA, MSD, GAA, absGAA, GSD) and the second subgroup consisting of non-dimensional, scale invariant curvature parameters (HMC, MLN, HGC, GLN). Since the former parameters intrinsically decrease with IA size, while the latter parameters increase with IA size, the negative correlation of the two subgroups with each other makes sense. It should be noted that the positive correlation of the non-dimensional curvature parameters with IA size is not an intrinsic property of the non-dimensional parameters themselves, since they are designed to be scale invariant. It rather indicates that curvature and irregularities of the IA surface increase in larger IAs.

For a geometric risk parameter to be a good candidate for rupture risk prediction, it should generally have a high SAD, in order to be able to differentiate between ruptured and unruptured IAs. Additionally, DUR should be high, indicating low sensitivity of the parameter to the particular imaging, segmentation, and calculation workflow, by which it is calculated. This is desirable because it allows models including such parameters to generalize well to other datasets. Finally, when choosing a set of parameters, data from the correlation analysis can be used to identify parameters that are not strongly correlated. Neyazi et al. have previously used this method to derive a two-parameter rupture status prediction model from a set of 49 geometric and hemodynamic rupture risk parameters, identifying AR and the maximal relative residence time as the most suitable model parameters [13]. Other attempts to identify suitable rupture status prediction models based on geometric risk parameters have been attempted, e.g., Dhar et al. [15] and Zhang et al. [30], but results have generally been inconsistent. Possible reasons for the discrepant findings regarding optimal parameter choice are the sample sizes used and the uncertainty inherent in the workflow by which the parameters are calculated. This may lead to the selection of less robust parameters that perform well on a given dataset but generalize less well to others. Based on the results of this study and considering SAD,

DUR, as well as the correlation between geometric risk parameters, examples of more robust parameter choices could look as follows:

- H_{\max} , $D_{\text{neck},\text{min}}$, AR, AASA, and MLN for the anterior region.
- L_{\max} , P_{neck} , AR, AASA, and HGC for the ICA.
- D_{\max} , $D_{\text{neck},\text{min}}$, eAR, AASA, and HMC for the MCA.
- L_{\max} , $D_{\text{neck},\text{min}}$, BL, EI, and absMAA for the posterior region.
- H_b , $D_{\text{neck},\text{min}}$, AR, AASA, and MLN if looking at all anatomical regions combined.

Overall, while individual size, neck, and curvature parameters achieved good discriminative performance and robustness, the non-dimensional parameters tended to perform well as a group. This suggests that non-dimensional geometric risk parameters can provide comparatively good discriminative performance, while the nondimensionalization itself mitigates some of the uncertainty introduced through the workflow by which the parameters are calculated [14].

Limitations

IAs were grouped by anatomical region because IA location is an important determinant of rupture risk, as demonstrated by its weight in current risk scores [7-9]. However, by analyzing the datasets by anatomical region, some subsamples become quite small. Small sample size might affect the accuracy of the median and interquartile range estimates derived from these groups. This limitation is, however, partially mitigated by also analyzing all anatomical regions combined and using two datasets, in order to get a more comprehensive picture of the risk parameters' performance. Another potential limitation are the uncertainty values from Goubergrits et al. [14], which were used to calculate DUR. These values were calculated on a sample containing MCA and posterior region IAs [14]. While it does not seem particularly probable, it is possible that IA location might affect the uncertainty inherent in calculating the geometric risk parameters in a relevant manner, which in turn could influence DUR results. A more fundamental limitation is the focus on geometric risk parameters. These parameters serve as proxies for the pathophysiological processes leading to IA rupture through the latter's influence on the geometry of the IA surface. Due to their nature, geometric risk parameters cannot directly capture the hemodynamic, mechanical, or biochemical aspects of IA rupture. Nevertheless, they are among the most intensely researched types of IA rupture risk parameters, due to the comparative ease with which they can be calculated from clinical data.

Conclusion

Based on datasets from two research groups, the present study provides location-specific estimates of the discriminative ability of a large set of geometric risk parameters for IA rupture risk assessment, while also considering uncertainty. Additionally, correlation patterns between the parameters are identified. The presented data is potentially useful in evaluating geometric risk parameters for use in rupture risk models or

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3 when choosing input parameters for machine learning approaches to rupture risk prediction. It may also be
4 helpful when designing future geometric risk parameters for clinical use.
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Conflict of interest statement

The authors declare that there is no conflict of interest.

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Data Availability Statement

All individual parameter values as well as the correlation coefficients are made available as supplemental material.

- supplemental material 1: individual parameter values, IA location, and rupture status for each IA
- supplemental material 2: exact values of the inter-parameter correlation coefficients

Ethical approval statements

In this study, patient-specific 3D reconstructions of intracranial aneurysms based on routine information were evaluated retrospectively. Use of retrospective data was approved by the local ethics committees (Ethikkommission der Charité - Universitätsmedizin Berlin: EA2/222/19; Ethikkommission der Med. Hochschule Hannover: NOVA Nr. 68/20).

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Author contributions

All roles according to CRediT (contributor roles taxonomy). Conceptualization: LG, JS, FH, JB, and PB. Methodology: FH, JS, and LG. Resources: AS, IES, OB, NL, SS, and PB. Investigation: JB, FH, and JS. Formal Analysis: FH. Funding acquisition: LG, PB, and SS. Supervision: LG. Writing – original draft: FH, LG, and JB. Writing – review & editing: PB, SS, AS, IES, OB, NL, and JS.

References

1. Vlak, M.H., A. Algra, R. Brandenburg, and G.J. Rinkel, *Prevalence of unruptured intracranial aneurysms, with emphasis on sex, age, comorbidity, country, and time period: a systematic review and meta-analysis*. *Lancet Neurol*, 2011. **10**(7): p. 626-36.
2. Brown, R.D., Jr. and J.P. Broderick, *Unruptured intracranial aneurysms: epidemiology, natural history, management options, and familial screening*. *Lancet Neurol*, 2014. **13**(4): p. 393-404.
3. Wiebers, D.O., J.P. Whisnant, J. Huston, 3rd, I. Meissner, R.D. Brown, Jr., D.G. Piepgras, G.S. Forbes, K. Thielen, D. Nichols, W.M. O'Fallon, J. Peacock, L. Jaeger, N.F. Kassell, G.L. Kongable-Beckman, J.C. Torner, and I. International Study of Unruptured Intracranial Aneurysms, *Unruptured intracranial aneurysms: natural history, clinical outcome, and risks of surgical and endovascular treatment*. *Lancet*, 2003. **362**(9378): p. 103-10.
4. Rackauskaite, D., E. Svanborg, E. Andersson, K. Lowhagen, L. Csajbok, and B. Nellgard, *Prospective study: Long-term outcome at 12-15 years after aneurysmal subarachnoid hemorrhage*. *Acta Neurol Scand*, 2018. **138**(5): p. 400-407.
5. Pontes, F.G.B., E.M. da Silva, J.C. Baptista-Silva, and V. Vasconcelos, *Treatments for unruptured intracranial aneurysms*. *Cochrane Database Syst Rev*, 2021. **5**: p. CD013312.
6. Thompson, B.G., et al., *Guidelines for the Management of Patients With Unruptured Intracranial Aneurysms: A Guideline for Healthcare Professionals From the American Heart Association/American Stroke Association*. *Stroke*, 2015. **46**(8): p. 2368-400.
7. Greving, J.P., M.J. Wermer, R.D. Brown, Jr., A. Morita, S. Juvela, M. Yonekura, T. Ishibashi, J.C. Torner, T. Nakayama, G.J. Rinkel, and A. Algra, *Development of the PHASES score for prediction of risk of rupture of intracranial aneurysms: a pooled analysis of six prospective cohort studies*. *Lancet Neurol*, 2014. **13**(1): p. 59-66.
8. Etminan, N., et al., *The unruptured intracranial aneurysm treatment score: a multidisciplinary consensus*. *Neurology*, 2015. **85**(10): p. 881-9.
9. Backes, D., et al., *ELAPSS score for prediction of risk of growth of unruptured intracranial aneurysms*. *Neurology*, 2017. **88**(17): p. 1600-1606.
10. Juvela, S., *PHASES score and treatment scoring with cigarette smoking in the long-term prediction of rupturing of unruptured intracranial aneurysms*. *J Neurosurg*, 2022. **136**(1): p. 156-162.
11. Molenberg, R., M.W. Aalbers, A. Mazuri, G.J. Luijckx, J.D.M. Metzemaekers, R.J.M. Groen, M. Uyttenboogaart, and J.M.C. van Dijk, *The Unruptured Intracranial Aneurysm Treatment Score as a predictor of aneurysm growth or rupture*. *Eur J Neurol*, 2021. **28**(3): p. 837-843.
12. Hernandez-Duran, S., D. Mielke, V. Rohde, and V. Malinova, *Is the unruptured intracranial aneurysm treatment score (UIATS) sensitive enough to detect aneurysms at risk of rupture?* *Neurosurg Rev*, 2021. **44**(2): p. 987-993.
13. Neyazi, B., V.M. Swiatek, M. Skalej, O. Beuing, K.P. Stein, J. Hattingen, B. Preim, P. Berg, S. Saalfeld, and I.E. Sandalcioglu, *Rupture risk assessment for multiple intracranial aneurysms: why there is no need for dozens of clinical, morphological and hemodynamic parameters*. *Ther Adv Neurol Disord*, 2020. **13**: p. 1756286420966159.
14. Goubergrits, L., F. Hellmeier, J. Bruening, A. Spuler, H.C. Hege, S. Voss, G. Janiga, S. Saalfeld, O. Beuing, and P. Berg, *Multiple Aneurysms AnaTomy CHallenge 2018 (MATCH): uncertainty quantification of geometric rupture risk parameters*. *Biomed Eng Online*, 2019. **18**(1): p. 35.
15. Dhar, S., M. Tremmel, J. Mocco, M. Kim, J. Yamamoto, A.H. Siddiqui, L.N. Hopkins, and H. Meng, *Morphology parameters for intracranial aneurysm rupture risk assessment*. *Neurosurgery*, 2008. **63**(2): p. 185-96; discussion 196-7.
16. Detmer, F.J., B.J. Chung, F. Mut, M. Slawski, F. Hamzei-Sichani, C. Putman, C. Jimenez, and J.R. Cebal, *Development and internal validation of an aneurysm rupture probability model based on patient characteristics and aneurysm location, morphology, and hemodynamics*. *Int J Comput Assist Radiol Surg*, 2018. **13**(11): p. 1767-1779.

17. Lauric, A., M.I. Baharoglu, and A.M. Malek, *Ruptured status discrimination performance of aspect ratio, height/width, and bottleneck factor is highly dependent on aneurysm sizing methodology*. Neurosurgery, 2012. **71**(1): p. 38-45.
18. Berg, P., et al., *Multiple Aneurysms AnaTomy CHallenge 2018 (MATCH): Phase I: Segmentation*. Cardiovasc Eng Technol, 2018. **9**(4): p. 565-581.
19. Ma, B., R.E. Harbaugh, and M.L. Raghavan, *Three-dimensional geometrical characterization of cerebral aneurysms*. Ann Biomed Eng, 2004. **32**(2): p. 264-73.
20. Lauric, A., E.L. Miller, M.I. Baharoglu, and A.M. Malek, *3D shape analysis of intracranial aneurysms using the writhe number as a discriminant for rupture*. Ann Biomed Eng, 2011. **39**(5): p. 1457-69.
21. Chien, A., J. Sayre, and F. Vinuela, *Comparative morphological analysis of the geometry of ruptured and unruptured aneurysms*. Neurosurgery, 2011. **69**(2): p. 349-56.
22. Ujiie, H., Y. Tamano, K. Sasaki, and T. Hori, *Is the aspect ratio a reliable index for predicting the rupture of a saccular aneurysm?* Neurosurgery, 2001. **48**(3): p. 495-502; discussion 502-3.
23. Ramachandran, M., R. Retarekar, R.E. Harbaugh, D. Hasan, B. Policeni, R. Rosenwasser, C. Ogilvy, and M.L. Raghavan, *Sensitivity of Quantified Intracranial Aneurysm Geometry to Imaging Modality*. Cardiovasc Eng Technol, 2013. **4**(1): p. 75-86.
24. O'Meara, B., J.P. Rahal, A. Lauric, and A.M. Malek, *Benefit of a sharp computed tomography angiography reconstruction kernel for improved characterization of intracranial aneurysms*. Neurosurgery, 2014. **10 Suppl 1**: p. 97-105; discussion 105.
25. Berg, P., S. Saalfeld, S. Voss, T. Redel, B. Preim, G. Janiga, and O. Beuing, *Does the DSA reconstruction kernel affect hemodynamic predictions in intracranial aneurysms? An analysis of geometry and blood flow variations*. J Neurointerv Surg, 2018. **10**(3): p. 290-296.
26. Cebal, J.R., M.A. Castro, S. Appanaboyina, C.M. Putman, D. Millan, and A.F. Frangi, *Efficient pipeline for image-based patient-specific analysis of cerebral aneurysm hemodynamics: technique and sensitivity*. IEEE Trans Med Imaging, 2005. **24**(4): p. 457-67.
27. Sarrami-Foroushani, A., T. Lassila, and A.F. Frangi, *Virtual endovascular treatment of intracranial aneurysms: models and uncertainty*. Wiley Interdiscip Rev Syst Biol Med, 2017. **9**(4).
28. Schneiders, J.J., H.A. Marquering, L. Antiga, R. van den Berg, E. VanBavel, and C.B. Majoie, *Intracranial aneurysm neck size overestimation with 3D rotational angiography: the impact on intra-aneurysmal hemodynamics simulated with computational fluid dynamics*. AJNR Am J Neuroradiol, 2013. **34**(1): p. 121-8.
29. Ivantsits, M., et al., *Detection and analysis of cerebral aneurysms based on X-ray rotational angiography - the CADA 2020 challenge*. Med Image Anal, 2021. **77**: p. 102333.
30. Zheng, Y., F. Xu, J. Ren, Q. Xu, Y. Liu, Y. Tian, and B. Leng, *Assessment of intracranial aneurysm rupture based on morphology parameters and anatomical locations*. J Neurointerv Surg, 2016. **8**(12): p. 1240-1246.

Figures

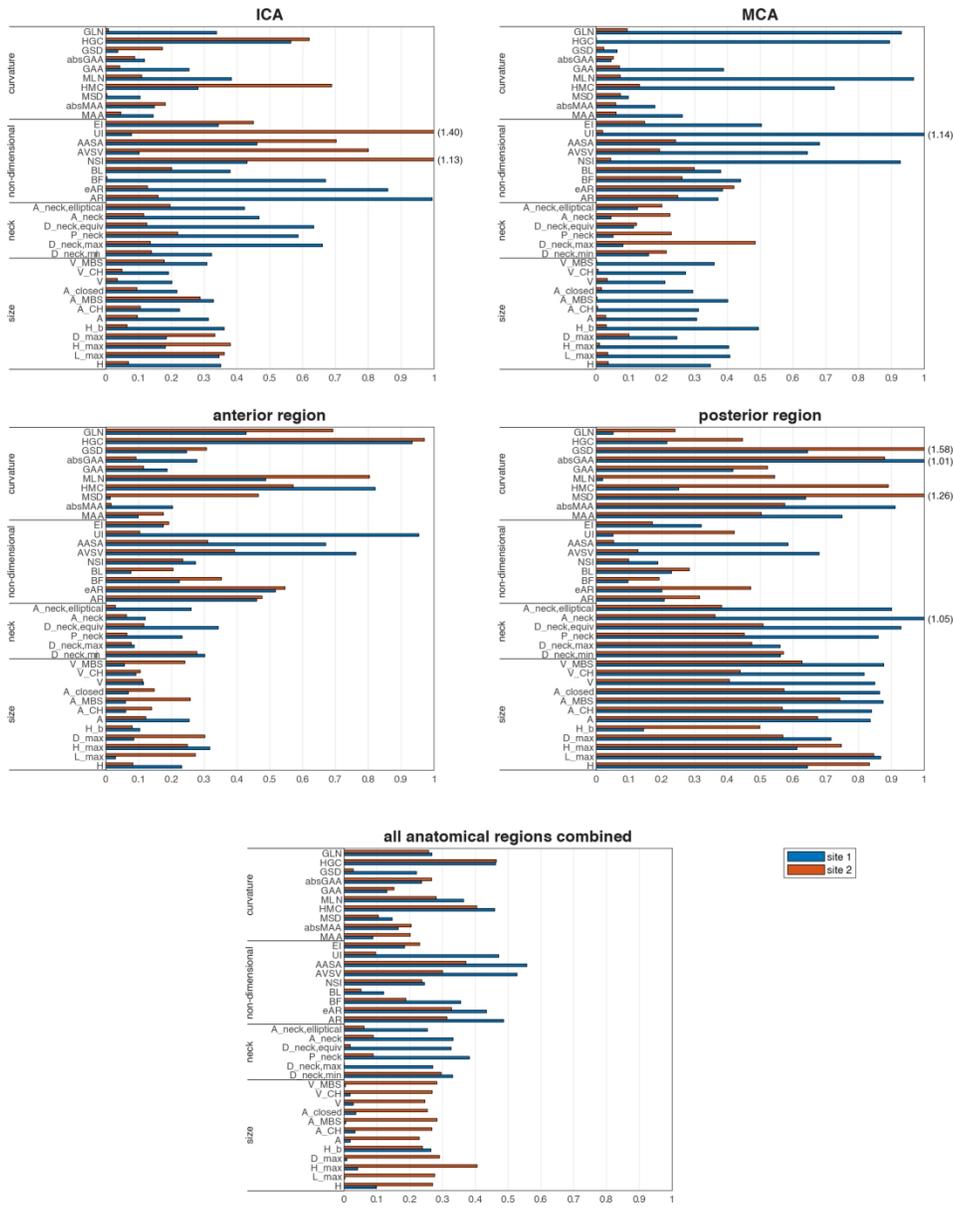
Figure 1: Standardized absolute group difference (SAD) for each anatomical region and dataset.

Figure 2: Group difference-uncertainty ratio (DUR) for each anatomical region and dataset.

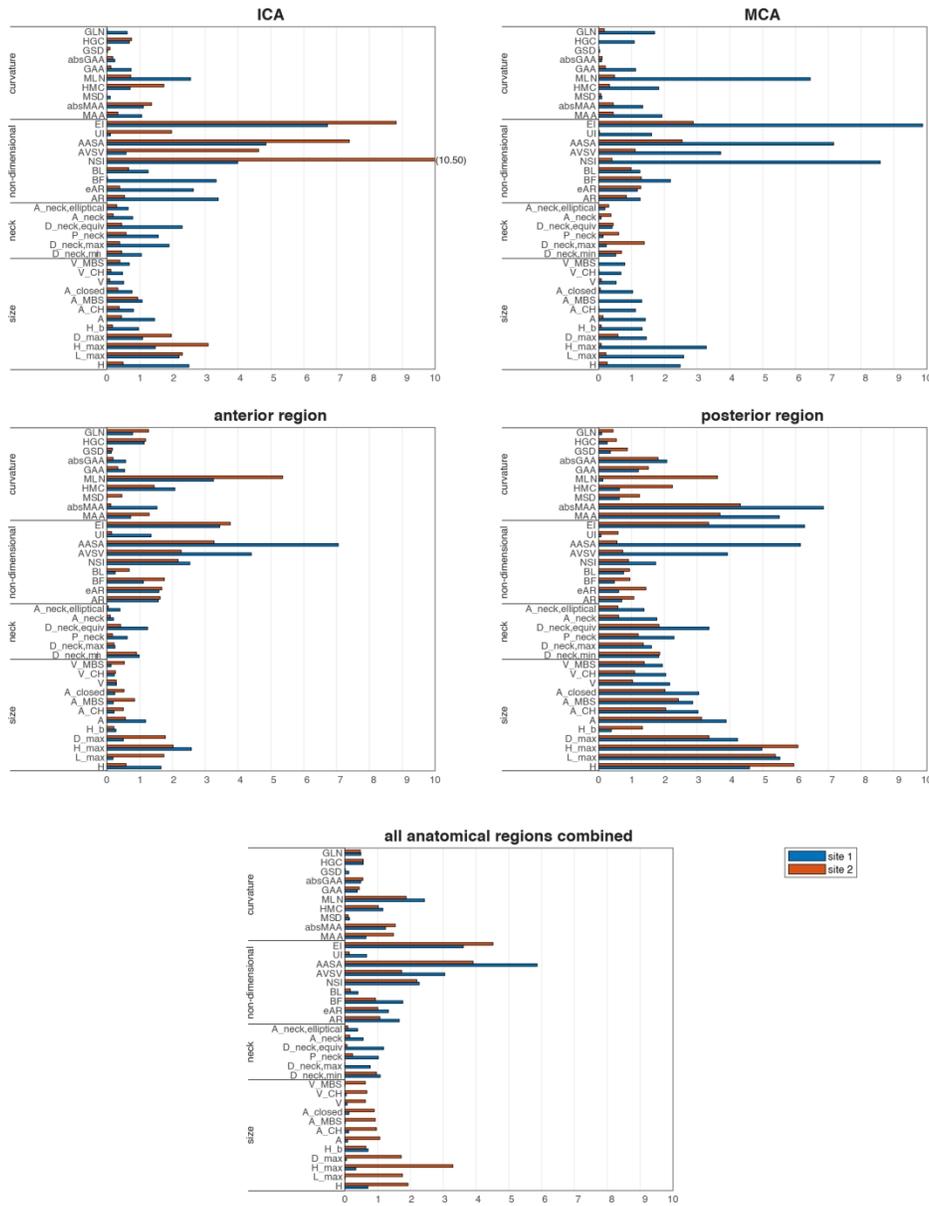
Figure 3: Pearson's r for correlation between geometric risk parameters by anatomical region for dataset 1.

Figure 4: Pearson's r for correlation between geometric risk parameters by anatomical region for dataset 4.

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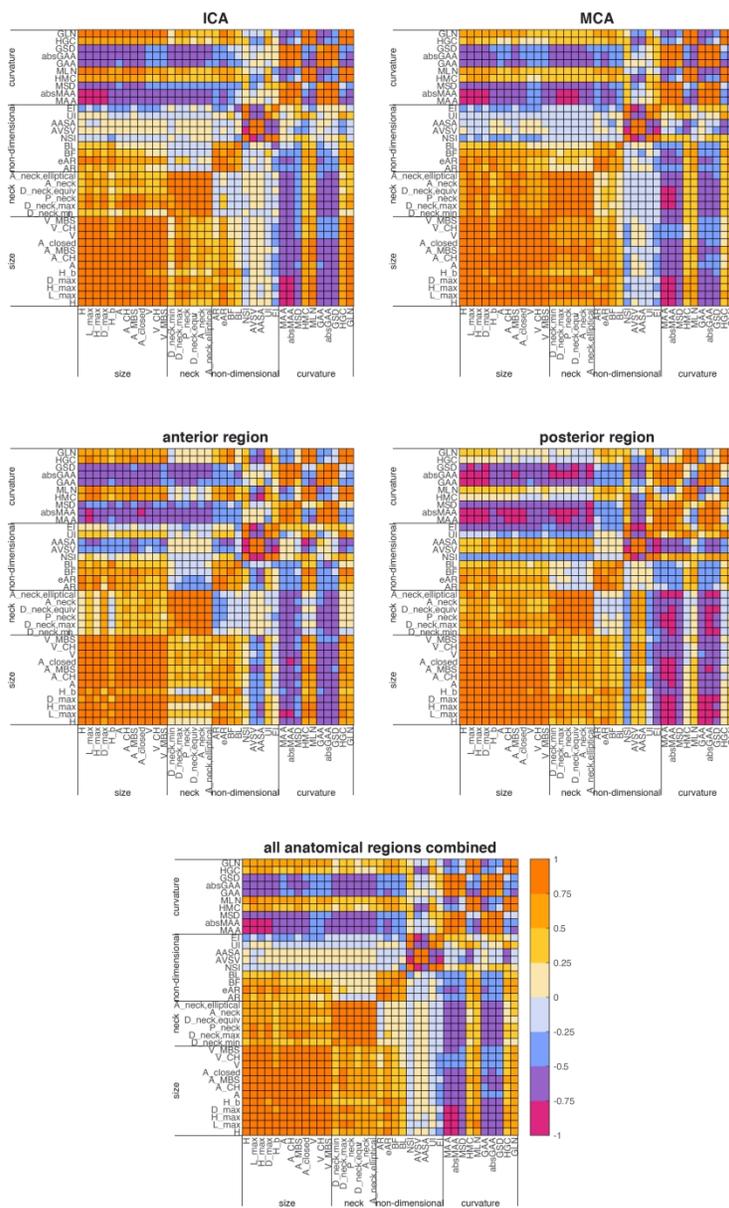


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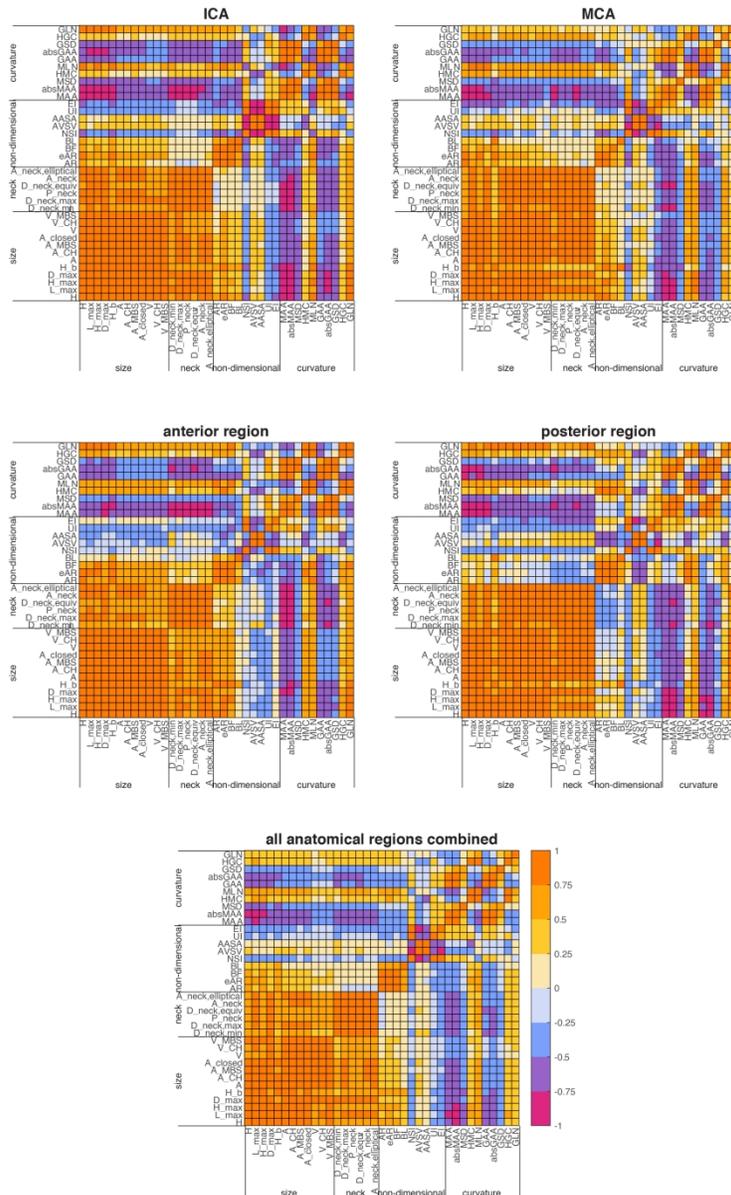


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	Pearson's r	H	L_max	H_max	D_max	H_b	A	A_CH
3	H	1.000	0.872	0.968	0.610	0.836	0.867	0.830
4	L_max	0.872	1.000	0.950	0.884	0.648	0.962	0.960
5	H_max	0.968	0.950	1.000	0.728	0.783	0.922	0.894
6	D_max	0.610	0.884	0.728	1.000	0.349	0.873	0.900
8	H_b	0.836	0.648	0.783	0.349	1.000	0.653	0.605
9	A	0.867	0.962	0.922	0.873	0.653	1.000	0.993
10	A_CH	0.830	0.960	0.894	0.900	0.605	0.993	1.000
11	A_MBS	0.835	0.973	0.919	0.863	0.596	0.967	0.957
12	A_closed	0.827	0.957	0.890	0.899	0.606	0.992	1.000
14	V	0.779	0.917	0.842	0.869	0.565	0.980	0.988
15	V_CH	0.778	0.924	0.846	0.880	0.548	0.982	0.988
16	V_MBS	0.769	0.918	0.857	0.822	0.522	0.934	0.919
18	D_neck,mir	0.220	0.402	0.246	0.535	0.125	0.415	0.484
19	D_neck,ma	0.153	0.466	0.248	0.642	-0.049	0.426	0.520
20	P_neck	0.059	0.376	0.158	0.554	-0.075	0.353	0.454
21	D_neck,eqt	0.159	0.428	0.224	0.609	-0.014	0.417	0.508
22	A_neck	0.089	0.392	0.170	0.583	-0.064	0.390	0.491
23	A_neck,elli	0.179	0.448	0.240	0.630	0.028	0.450	0.541
25	AR	0.867	0.582	0.784	0.236	0.849	0.579	0.503
26	eAR	0.879	0.639	0.819	0.304	0.801	0.608	0.536
27	BF	0.701	0.727	0.749	0.684	0.595	0.735	0.682
28	BL	0.627	0.461	0.580	0.273	0.884	0.464	0.423
29	NSI	0.173	0.275	0.235	0.216	-0.021	0.142	0.129
31	AVSV	-0.393	-0.491	-0.481	-0.331	-0.275	-0.315	-0.287
32	AASA	-0.455	-0.558	-0.551	-0.378	-0.337	-0.380	-0.350
33	UI	0.405	0.494	0.463	0.437	0.137	0.365	0.356
34	EI	0.012	0.091	0.067	0.013	-0.075	-0.034	-0.050
35	MAA	-0.661	-0.763	-0.698	-0.727	-0.481	-0.702	-0.740
36	absMAA	-0.692	-0.755	-0.711	-0.701	-0.547	-0.710	-0.747
38	MSD	-0.504	-0.453	-0.465	-0.370	-0.517	-0.489	-0.513
39	HMC	0.672	0.801	0.776	0.698	0.434	0.706	0.672
40	MLN	0.727	0.775	0.790	0.706	0.500	0.745	0.704
42	GAA	-0.627	-0.693	-0.655	-0.632	-0.443	-0.590	-0.621
43	absGAA	-0.647	-0.688	-0.659	-0.626	-0.534	-0.639	-0.672
44	GSD	-0.547	-0.567	-0.541	-0.507	-0.511	-0.550	-0.584
45	HGC	0.618	0.783	0.727	0.735	0.322	0.710	0.685
46	GLN	0.614	0.729	0.698	0.731	0.300	0.711	0.681

	A_MBS	A_closed	V	V_CH	V_MBS	D_neck,min	D_neck,max	P_neck
1								
2								
3	0.835	0.827	0.779	0.778	0.769	0.220	0.153	0.059
4	0.973	0.957	0.917	0.924	0.918	0.402	0.466	0.376
5	0.919	0.890	0.842	0.846	0.857	0.246	0.248	0.158
6	0.863	0.899	0.869	0.880	0.822	0.535	0.642	0.554
7	0.596	0.606	0.565	0.548	0.522	0.125	-0.049	-0.075
8	0.967	0.992	0.980	0.982	0.934	0.415	0.426	0.353
9	0.957	1.000	0.988	0.988	0.919	0.484	0.520	0.454
10	1.000	0.952	0.939	0.953	0.984	0.346	0.375	0.290
11	0.952	1.000	0.989	0.988	0.913	0.494	0.526	0.462
12	0.939	0.989	1.000	0.998	0.920	0.486	0.503	0.457
13	0.953	0.988	0.998	1.000	0.940	0.460	0.485	0.430
14	0.984	0.913	0.920	0.940	1.000	0.298	0.302	0.223
15	0.346	0.494	0.486	0.460	0.298	1.000	0.685	0.681
16	0.375	0.526	0.503	0.485	0.302	0.685	1.000	0.952
17	0.290	0.462	0.457	0.430	0.223	0.681	0.952	1.000
18	0.361	0.516	0.504	0.485	0.310	0.907	0.870	0.857
19	0.321	0.500	0.503	0.477	0.263	0.780	0.944	0.974
20	0.377	0.550	0.543	0.517	0.316	0.909	0.909	0.886
21	0.568	0.498	0.454	0.459	0.527	-0.127	-0.328	-0.375
22	0.610	0.529	0.473	0.480	0.553	-0.208	-0.214	-0.304
23	0.753	0.675	0.643	0.668	0.743	0.043	-0.096	-0.153
24	0.362	0.427	0.370	0.348	0.268	0.087	-0.061	-0.064
25	0.334	0.113	0.080	0.131	0.361	-0.197	-0.061	-0.176
26	-0.501	-0.273	-0.225	-0.261	-0.486	0.179	0.068	0.160
27	-0.558	-0.337	-0.288	-0.320	-0.535	0.160	0.041	0.130
28	0.494	0.340	0.273	0.321	0.477	-0.152	0.134	-0.008
29	0.166	-0.065	-0.072	-0.032	0.209	-0.227	-0.193	-0.269
30	-0.636	-0.743	-0.667	-0.654	-0.529	-0.582	-0.679	-0.648
31	-0.627	-0.752	-0.683	-0.661	-0.516	-0.646	-0.664	-0.637
32	-0.379	-0.521	-0.510	-0.474	-0.310	-0.620	-0.396	-0.402
33	0.801	0.661	0.604	0.639	0.770	-0.028	0.133	-0.011
34	0.753	0.697	0.631	0.658	0.708	-0.009	0.127	-0.014
35	-0.547	-0.622	-0.527	-0.520	-0.433	-0.446	-0.584	-0.543
36	-0.551	-0.678	-0.607	-0.582	-0.440	-0.652	-0.603	-0.580
37	-0.453	-0.592	-0.545	-0.515	-0.360	-0.695	-0.549	-0.547
38	0.811	0.672	0.627	0.670	0.805	-0.029	0.180	0.038
39	0.748	0.672	0.626	0.664	0.737	-0.038	0.158	0.024
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	D_neck, equi	A_neck	A_neck, ellipt	eAR	BF	BL	NSI	
1								
2								
3	0.159	0.089	0.179	0.867	0.879	0.701	0.627	0.173
4	0.428	0.392	0.448	0.582	0.639	0.727	0.461	0.275
5	0.224	0.170	0.240	0.784	0.819	0.749	0.580	0.235
6	0.609	0.583	0.630	0.236	0.304	0.684	0.273	0.216
7								
8	-0.014	-0.064	0.028	0.849	0.801	0.595	0.884	-0.021
9	0.417	0.390	0.450	0.579	0.608	0.735	0.464	0.142
10	0.508	0.491	0.541	0.503	0.536	0.682	0.423	0.129
11	0.361	0.321	0.377	0.568	0.610	0.753	0.362	0.334
12	0.516	0.500	0.550	0.498	0.529	0.675	0.427	0.113
13	0.504	0.503	0.543	0.454	0.473	0.643	0.370	0.080
14	0.485	0.477	0.517	0.459	0.480	0.668	0.348	0.131
15	0.310	0.263	0.316	0.527	0.553	0.743	0.268	0.361
16	0.907	0.780	0.909	-0.127	-0.208	0.043	0.087	-0.197
17	0.870	0.944	0.909	-0.328	-0.214	-0.096	-0.061	-0.061
18	0.857	0.974	0.886	-0.375	-0.304	-0.153	-0.064	-0.176
19	1.000	0.927	0.953	-0.267	-0.298	-0.034	-0.040	-0.113
20	0.927	1.000	0.949	-0.353	-0.317	-0.119	-0.074	-0.157
21	0.953	0.949	1.000	-0.266	-0.247	-0.036	0.004	-0.155
22	-0.267	-0.353	-0.266	1.000	0.946	0.687	0.672	0.175
23	-0.298	-0.317	-0.247	0.946	1.000	0.669	0.627	0.253
24	-0.034	-0.119	-0.036	0.687	0.669	1.000	0.525	0.300
25	-0.040	-0.074	0.004	0.672	0.627	0.525	1.000	-0.267
26	-0.113	-0.157	-0.155	0.175	0.253	0.300	-0.267	1.000
27	0.141	0.175	0.161	-0.403	-0.468	-0.491	-0.075	-0.823
28	0.129	0.153	0.138	-0.450	-0.524	-0.532	-0.148	-0.751
29	0.019	-0.021	-0.047	0.320	0.427	0.442	-0.027	0.824
30	-0.219	-0.243	-0.226	0.085	0.141	0.157	-0.325	0.922
31	-0.656	-0.622	-0.632	-0.337	-0.379	-0.384	-0.446	0.044
32	-0.678	-0.632	-0.667	-0.377	-0.393	-0.371	-0.492	0.103
33	-0.516	-0.461	-0.553	-0.319	-0.252	-0.158	-0.456	0.370
34	0.017	-0.024	0.030	0.536	0.649	0.764	0.318	0.542
35	0.022	-0.028	0.035	0.591	0.685	0.804	0.463	0.314
36	-0.543	-0.499	-0.495	-0.365	-0.417	-0.365	-0.436	-0.045
37	-0.634	-0.575	-0.635	-0.368	-0.375	-0.327	-0.513	0.183
38	-0.631	-0.563	-0.640	-0.296	-0.265	-0.203	-0.488	0.303
39	0.077	0.033	0.055	0.449	0.560	0.753	0.186	0.602
40	0.064	0.022	0.042	0.453	0.551	0.779	0.234	0.427
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3	-0.393	-0.455	0.405	0.012	-0.661	-0.692	-0.504	0.672
4	-0.491	-0.558	0.494	0.091	-0.763	-0.755	-0.453	0.801
5	-0.481	-0.551	0.463	0.067	-0.698	-0.711	-0.465	0.776
6	-0.331	-0.378	0.437	0.013	-0.727	-0.701	-0.370	0.698
7	-0.275	-0.337	0.137	-0.075	-0.481	-0.547	-0.517	0.434
8	-0.315	-0.380	0.365	-0.034	-0.702	-0.710	-0.489	0.706
9	-0.287	-0.350	0.356	-0.050	-0.740	-0.747	-0.513	0.672
10	-0.501	-0.558	0.494	0.166	-0.636	-0.627	-0.379	0.801
11	-0.273	-0.337	0.340	-0.065	-0.743	-0.752	-0.521	0.661
12	-0.225	-0.288	0.273	-0.072	-0.667	-0.683	-0.510	0.604
13	-0.261	-0.320	0.321	-0.032	-0.654	-0.661	-0.474	0.639
14	-0.486	-0.535	0.477	0.209	-0.529	-0.516	-0.310	0.770
15	0.179	0.160	-0.152	-0.227	-0.582	-0.646	-0.620	-0.028
16	0.068	0.041	0.134	-0.193	-0.679	-0.664	-0.396	0.133
17	0.160	0.130	-0.008	-0.269	-0.648	-0.637	-0.402	-0.011
18	0.141	0.129	0.019	-0.219	-0.656	-0.678	-0.516	0.017
19	0.175	0.153	-0.021	-0.243	-0.622	-0.632	-0.461	-0.024
20	0.161	0.138	-0.047	-0.226	-0.632	-0.667	-0.553	0.030
21	-0.403	-0.450	0.320	0.085	-0.337	-0.377	-0.319	0.536
22	-0.468	-0.524	0.427	0.141	-0.379	-0.393	-0.252	0.649
23	-0.491	-0.532	0.442	0.157	-0.384	-0.371	-0.158	0.764
24	-0.075	-0.148	-0.027	-0.325	-0.446	-0.492	-0.456	0.318
25	-0.823	-0.751	0.824	0.922	0.044	0.103	0.370	0.542
26	1.000	0.988	-0.699	-0.776	0.120	0.070	-0.205	-0.736
27	0.988	1.000	-0.667	-0.702	0.177	0.129	-0.138	-0.785
28	-0.699	-0.667	1.000	0.556	-0.297	-0.203	0.211	0.706
29	-0.776	-0.702	0.556	1.000	0.257	0.273	0.377	0.341
30	0.120	0.177	-0.297	0.257	1.000	0.974	0.558	-0.424
31	0.070	0.129	-0.203	0.273	0.974	1.000	0.709	-0.339
32	-0.205	-0.138	0.211	0.377	0.558	0.709	1.000	0.032
33	-0.736	-0.785	0.706	0.341	-0.424	-0.339	0.032	1.000
34	-0.488	-0.536	0.586	0.075	-0.511	-0.427	0.009	0.912
35	0.207	0.254	-0.399	0.184	0.968	0.923	0.460	-0.446
36	0.021	0.088	-0.094	0.314	0.933	0.973	0.764	-0.290
37	-0.118	-0.050	0.060	0.393	0.798	0.880	0.904	-0.119
38	-0.689	-0.718	0.778	0.366	-0.422	-0.320	0.097	0.961
39	-0.487	-0.516	0.661	0.173	-0.452	-0.345	0.122	0.881
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3		0.727	-0.627	-0.647	-0.547	0.618	0.614
4		0.775	-0.693	-0.688	-0.567	0.783	0.729
5		0.790	-0.655	-0.659	-0.541	0.727	0.698
6		0.706	-0.632	-0.626	-0.507	0.735	0.731
7		0.500	-0.443	-0.534	-0.511	0.322	0.300
8		0.745	-0.590	-0.639	-0.550	0.710	0.711
9		0.704	-0.621	-0.672	-0.584	0.685	0.681
10		0.753	-0.547	-0.551	-0.453	0.811	0.748
11		0.697	-0.622	-0.678	-0.592	0.672	0.672
12		0.631	-0.527	-0.607	-0.545	0.627	0.626
13		0.658	-0.520	-0.582	-0.515	0.670	0.664
14		0.708	-0.433	-0.440	-0.360	0.805	0.737
15		-0.009	-0.446	-0.652	-0.695	-0.029	-0.038
16		0.127	-0.584	-0.603	-0.549	0.180	0.158
17		-0.014	-0.543	-0.580	-0.547	0.038	0.024
18		0.022	-0.543	-0.634	-0.631	0.077	0.064
19		-0.028	-0.499	-0.575	-0.563	0.033	0.022
20		0.035	-0.495	-0.635	-0.640	0.055	0.042
21		0.591	-0.365	-0.368	-0.296	0.449	0.453
22		0.685	-0.417	-0.375	-0.265	0.560	0.551
23		0.804	-0.365	-0.327	-0.203	0.753	0.779
24		0.463	-0.436	-0.513	-0.488	0.186	0.234
25		0.314	-0.045	0.183	0.303	0.602	0.427
26		-0.488	0.207	0.021	-0.118	-0.689	-0.487
27		-0.536	0.254	0.088	-0.050	-0.718	-0.516
28		0.586	-0.399	-0.094	0.060	0.778	0.661
29		0.075	0.184	0.314	0.393	0.366	0.173
30		-0.511	0.968	0.933	0.798	-0.422	-0.452
31		-0.427	0.923	0.973	0.880	-0.320	-0.345
32		0.009	0.460	0.764	0.904	0.097	0.122
33		0.912	-0.446	-0.290	-0.119	0.961	0.881
34		1.000	-0.519	-0.372	-0.166	0.886	0.941
35		-0.519	1.000	0.888	0.724	-0.438	-0.459
36		-0.372	0.888	1.000	0.937	-0.231	-0.256
37		-0.166	0.724	0.937	1.000	-0.051	-0.034
38		0.886	-0.438	-0.231	-0.051	1.000	0.939
39		0.941	-0.459	-0.256	-0.034	0.939	1.000
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1	1	Berlin	Berlin	AComA	anterior	1	5.748
2	2	Berlin	Berlin	PComA	posterior	0	8.261
3	3	Berlin	Berlin	PICA	posterior	1	6.023
4	4	Berlin	Berlin	AComA	anterior	1	5.698
5	5	Berlin	Berlin	ACA	anterior	0	5.667
6	6	Berlin	Berlin	MCA	MCA	0	2.849
7	7	Berlin	Berlin	ICA	ICA	0	19.575
8	8	Berlin	Berlin	MCA	MCA	0	4.199
9	9	Berlin	Berlin	MCA	MCA	0	3.795
10	10	Berlin	Berlin	AComA	anterior	1	5.051
11	11	Berlin	Berlin	MCA	MCA	0	6.789
12	12	Berlin	Berlin	ICA	ICA	1	7.610
13	13	Berlin	Berlin	MCA	MCA	0	8.157
14	14	Berlin	Berlin	AComA	anterior	1	2.542
15	15	Berlin	Berlin	PComA	posterior	1	3.196
16	16A	Berlin	Berlin	ICA	ICA	1	9.587
17	16B	Berlin	Berlin	ACA	anterior	0	1.879
18	17A	Berlin	Berlin	ICA	ICA	0	12.261
19	17B	Berlin	Berlin	ICA	ICA	0	2.791
20	17C	Berlin	Berlin	AComA	anterior	0	4.530
21	18	Berlin	Berlin	MCA	MCA	1	5.597
22	19	Berlin	Berlin	AComA	anterior	1	5.177
23	20	Berlin	Berlin	PComA	posterior	1	10.569
24	21	Berlin	Berlin	ICA	ICA	0	4.966
25	22	Berlin	Berlin	ICA	ICA	0	7.908
26	23	Berlin	Berlin	MCA	MCA	1	4.598
27	24	Berlin	Berlin	ICA	ICA	0	2.906
28	25	Berlin	Berlin	BA	posterior	0	8.473
29	26	Berlin	Berlin	MCA	MCA	1	4.210
30	27	Berlin	Berlin	AComA	anterior	1	4.597
31	28	Berlin	Berlin	MCA	MCA	1	5.480
32	29	Berlin	Berlin	ICA	ICA	0	12.780
33	30A	Berlin	Berlin	ICA	ICA	0	4.078
34	30B	Berlin	Berlin	AComA	anterior	0	3.135
35	30C	Berlin	Berlin	AComA	anterior	1	5.085
36	30D	Berlin	Berlin	MCA	MCA	0	2.715
37	30E	Berlin	Berlin	PICA	posterior	1	4.983
38	31	Berlin	Berlin	MCA	MCA	0	4.542
39	32	Berlin	Berlin	ICA	ICA	0	9.475
40	33	Berlin	Berlin	AComA	anterior	1	6.212
41	34	Berlin	Berlin	AComA	anterior	0	3.383
42	35	Berlin	Berlin	ICA	ICA	1	11.690
43	36	Berlin	Berlin	BA	posterior	0	20.748
44	37	Berlin	Berlin	AComA	anterior	1	5.543
45	38	Berlin	Berlin	AComA	anterior	0	8.400
46	39	Berlin	Berlin	ICA	ICA	1	4.290
47	40	Berlin	Berlin	PComA	posterior	1	13.786

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2	41	Berlin	Berlin	ACoMA	anterior	1	4.301
3	42	Berlin	Berlin	PCoMA	posterior	0	5.891
4	43	Berlin	Berlin	ICA	ICA	0	6.872
5	44	Berlin	Berlin	PICA	posterior	1	4.213
6	45A	Berlin	Berlin	ICA	ICA	0	2.414
7	45B	Berlin	Berlin	ICA	ICA	1	3.501
8	45C	Berlin	Berlin	ICA	ICA	0	2.297
9	46	Berlin	Berlin	BA	posterior	0	11.175
10	47	Berlin	Berlin	ICA	ICA	0	4.636
11	48	Berlin	Berlin	MCA	MCA	0	2.204
12	49	Berlin	Berlin	MCA	MCA	1	16.986
13	50	Berlin	Berlin	PCoMA	posterior	1	7.588
14	51	Berlin	Berlin	ACoMA	anterior	0	5.047
15	52	Berlin	Berlin	ACA	anterior	1	2.779
16	53	Berlin	Berlin	AChA	ICA	1	6.830
17	54	Berlin	Berlin	PCoMA	posterior	1	4.857
18	55	Berlin	Berlin	ACoMA	anterior	0	3.330
19	56	Berlin	Berlin	MCA	MCA	1	2.092
20	57A	Berlin	Berlin	ICA	ICA	0	2.831
21	57B	Berlin	Berlin	ICA	ICA	0	4.277
22	57C	Berlin	Berlin	ICA	ICA	0	4.910
23	57D	Berlin	Berlin	ACoMA	anterior	1	2.565
24	57E	Berlin	Berlin	MCA	MCA	0	6.612
25	57F	Berlin	Berlin	MCA	MCA	0	1.536
26	57G	Berlin	Berlin	MCA	MCA	0	3.139
27	58	Berlin	Berlin	PCoMA	posterior	1	3.998
28	59	Berlin	Berlin	ICA	ICA	0	4.875
29	60A	Berlin	Berlin	MCA	MCA	0	8.547
30	60B	Berlin	Berlin	MCA	MCA	0	3.172
31	61	Berlin	Berlin	ACoMA	anterior	1	10.866
32	62	Berlin	Berlin	ICA	ICA	1	4.541
33	63	Berlin	Berlin	ACoMA	anterior	1	5.524
34	64	Berlin	Berlin	ICA	ICA	1	13.839
35	65	Berlin	Berlin	ICA	ICA	0	7.768
36	66	Berlin	Berlin	ACoMA	anterior	1	3.652
37	67	Berlin	Berlin	MCA	MCA	1	4.031
38	68	Berlin	Berlin	ACoMA	anterior	1	2.672
39	69	Berlin	Berlin	ICA	ICA	0	11.746
40	70	Berlin	Berlin	ACoMA	anterior	1	2.739
41	71	Berlin	Berlin	PCoMA	posterior	0	3.684
42	72A	Berlin	Berlin	PCoMA	posterior	0	9.969
43	72B	Berlin	Berlin	ACoMA	anterior	0	3.769
44	73	Berlin	Berlin	ACoMA	anterior	1	7.640
45	74	Berlin	Berlin	ICA	ICA	0	2.422
46	75A	Berlin	Berlin	PCoMA	posterior	0	2.277
47	75B	Berlin	Berlin	BA	posterior	1	4.556
48	76	Berlin	Berlin	PCoMA	posterior	1	4.974
49	77	Berlin	Berlin	MCA	MCA	0	10.165
50	78	Berlin	Berlin	MCA	MCA	0	5.020
51	79	Berlin	Berlin	ICA	ICA	0	9.202
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2	80	Berlin	Berlin	AComA	anterior	1	8.132
3	81	Berlin	Berlin	ICA	ICA	0	21.514
4	82A	Berlin	Berlin	ICA	ICA	0	2.039
5	82B	Berlin	Berlin	MCA	MCA	0	3.698
6	82C	Berlin	Berlin	ACA	anterior	0	1.486
7	83	Berlin	Berlin	PComA	posterior	0	10.503
8	84A	Berlin	Berlin	ICA	ICA	0	6.331
9	84B	Berlin	Berlin	MCA	MCA	0	3.509
10	85	Berlin	Berlin	MCA	MCA	0	2.996
11	86	Berlin	Berlin	MCA	MCA	0	2.575
12	87	Berlin	Berlin	AComA	anterior	1	3.971
13	88A	Berlin	Berlin	MCA	MCA	0	1.489
14	88B	Berlin	Berlin	MCA	MCA	0	2.304
15	89	Berlin	Berlin	ICA	ICA	0	5.728
16	90	Berlin	Berlin	MCA	MCA	0	4.016
17	91	Berlin	Berlin	AComA	anterior	0	6.147
18	92	Berlin	Berlin	PComA	posterior	0	7.023
19	93	Berlin	Berlin	PComA	posterior	1	10.373
20	94	Berlin	Berlin	MCA	MCA	0	19.183
21	95	Berlin	Berlin	AComA	anterior	1	6.261
22	96	Berlin	Berlin	ICA	ICA	0	5.202
23	97A	Berlin	Berlin	ICA	ICA	0	1.702
24	97B	Berlin	Berlin	AComA	anterior	0	5.381
25	98	Berlin	Berlin	PICA	posterior	1	4.524
26	99	Berlin	Berlin	PComA	posterior	0	6.067
27	100A	Berlin	Berlin	MCA	MCA	1	6.738
28	100B	Berlin	Berlin	ICA	ICA	0	2.364
29	100C	Berlin	Berlin	ICA	ICA	0	8.467
30	100D	Berlin	Berlin	MCA	MCA	0	2.488
31	100E	Berlin	Berlin	MCA	MCA	0	1.914
32	101	Berlin	Berlin	PComA	posterior	1	5.048
33	102	Berlin	Berlin	AComA	anterior	1	5.931
34	103	Berlin	Berlin	PCA	posterior	1	5.602
35	104	Berlin	Berlin	MCA	MCA	0	4.629
36	105	Berlin	Berlin	ICA	ICA	1	7.092
37	106	Berlin	Berlin	MCA	MCA	1	8.177
38	107	Berlin	Berlin	PComA	posterior	1	8.598
39	108	Berlin	Berlin	AComA	anterior	1	3.886
40	109	Berlin	Berlin	BA	posterior	1	13.918
41	110	Berlin	Berlin	BA	posterior	0	12.591
42	111	Berlin	Berlin	AComA	anterior	0	6.025
43	112	Berlin	Berlin	BA	posterior	1	7.000
44	113A	Berlin	Berlin	MCA	MCA	0	9.488
45	113B	Berlin	Berlin	MCA	MCA	0	6.242
46	114	Berlin	Berlin	MCA	MCA	1	3.622
47	115A	Hanover	Magdeburg	MCA	MCA	1	4.340
48	115B	Hanover	Magdeburg	MCA	MCA	0	1.149
49	116A	Hanover	Magdeburg	AComA	anterior	1	4.055
50	116B	Hanover	Magdeburg	AComA	anterior	0	1.031
51	117A	Hanover	Magdeburg	BA	posterior	1	8.476
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2	117B	Hanover	Magdeburg	ACoMA	anterior	0	4.088
3	118A	Hanover	Magdeburg	ACoMA	anterior	0	5.039
4	118B	Hanover	Magdeburg	PCoMA	posterior	1	4.528
5	119	Hanover	Magdeburg	MCA	MCA	1	1.132
6	120A	Hanover	Magdeburg	MCA	MCA	1	4.881
7	120B	Hanover	Magdeburg	ICA	ICA	1	2.325
8	121	Hanover	Magdeburg	ICA	ICA	1	18.704
9	122	Hanover	Magdeburg	ICA	ICA	0	6.667
10	123A	Hanover	Magdeburg	PCoMA	posterior	1	5.230
11	123B	Hanover	Magdeburg	MCA	MCA	0	2.984
12	124A	Hanover	Magdeburg	ACA	anterior	1	2.914
13	124B	Hanover	Magdeburg	ACoMA	anterior	0	1.201
14	124C	Hanover	Magdeburg	ACoMA	anterior	0	2.671
15	125	Hanover	Magdeburg	ICA	ICA	0	7.204
16	126A	Hanover	Magdeburg	MCA	MCA	1	8.466
17	126B	Hanover	Magdeburg	MCA	MCA	0	5.410
18	127A	Hanover	Magdeburg	ACoMA	anterior	1	2.663
19	127B	Hanover	Magdeburg	MCA	MCA	0	2.098
20	128A	Hanover	Magdeburg	ICA	ICA	1	1.429
21	128B	Hanover	Magdeburg	ICA	ICA	0	1.275
22	129A	Hanover	Magdeburg	BA	posterior	1	2.818
23	129B	Hanover	Magdeburg	SCA	posterior	0	1.293
24	130A	Hanover	Magdeburg	MCA	MCA	1	7.171
25	130B	Hanover	Magdeburg	ACoMA	anterior	0	4.247
26	131A	Hanover	Magdeburg	BA	posterior	0	4.863
27	131B	Hanover	Magdeburg	BA	posterior	1	3.992
28	132A	Hanover	Magdeburg	PCoMA	posterior	0	4.359
29	132B	Hanover	Magdeburg	ACoMA	anterior	1	16.578
30	133A	Hanover	Magdeburg	BA	posterior	1	6.042
31	133B	Hanover	Magdeburg	ACoMA	anterior	0	3.105
32	134A	Hanover	Magdeburg	MCA	MCA	1	6.298
33	134B	Hanover	Magdeburg	MCA	MCA	0	3.067
34	135	Hanover	Magdeburg	ICA	ICA	0	2.406
35	136A	Kiel	Magdeburg	MCA	MCA	0	1.108
36	136B	Kiel	Magdeburg	MCA	MCA	0	6.352
37	137	Kiel	Magdeburg	MCA	MCA	0	3.274
38	138	Kiel	Magdeburg	MCA	MCA	0	4.033
39	139	Kiel	Magdeburg	MCA	MCA	0	6.259
40	140	Kiel	Magdeburg	MCA	MCA	0	10.513
41	141	Kiel	Magdeburg	MCA	MCA	0	8.471
42	142	Kiel	Magdeburg	MCA	MCA	0	6.008
43	143	Kiel	Magdeburg	MCA	MCA	0	5.184
44	144	Kiel	Magdeburg	MCA	MCA	0	10.421
45	145	Kiel	Magdeburg	MCA	MCA	0	8.720
46	146A	Kiel	Magdeburg	MCA	MCA	0	6.242
47	146B	Kiel	Magdeburg	ACA	anterior	0	2.012
48	147A	Kiel	Magdeburg	MCA	MCA	0	5.580
49	147B	Kiel	Magdeburg	MCA	MCA	0	0.684
50	147C	Kiel	Magdeburg	MCA	MCA	0	0.573
51	147D	Kiel	Magdeburg	ACA	anterior	0	3.651
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2	147E	Kiel	Magdeburg	AComA	anterior	0	1.213
3	147F	Kiel	Magdeburg	AComA	anterior	0	1.384
4	148	Kiel	Magdeburg	MCA	MCA	0	4.650
5	149	Kiel	Magdeburg	MCA	MCA	0	6.489
6	150	Kiel	Magdeburg	MCA	MCA	0	4.962
7	151	Kiel	Magdeburg	MCA	MCA	0	3.962
8	152	Magdeburg	Magdeburg	MCA	MCA	0	5.866
9	153	Magdeburg	Magdeburg	ACA	anterior	1	3.594
10	154	Magdeburg	Magdeburg	PCoMA	posterior	1	9.941
11	155A	Magdeburg	Magdeburg	ACoMA	anterior	1	2.543
12	155B	Magdeburg	Magdeburg	ACoMA	anterior	0	3.589
13	155C	Magdeburg	Magdeburg	MCA	MCA	0	5.120
14	156A	Magdeburg	Magdeburg	ICA	ICA	0	7.048
15	156B	Magdeburg	Magdeburg	ICA	ICA	0	1.214
16	156C	Magdeburg	Magdeburg	ICA	ICA	0	1.765
17	156D	Magdeburg	Magdeburg	ICA	ICA	0	2.037
18	157	Magdeburg	Magdeburg	VA	posterior	1	5.194
19	158	Magdeburg	Magdeburg	AChA	ICA	0	3.248
20	159	Magdeburg	Magdeburg	MCA	MCA	0	5.645
21	160A	Magdeburg	Magdeburg	AChA	ICA	1	2.988
22	160B	Magdeburg	Magdeburg	ICA	ICA	0	2.842
23	161A	Magdeburg	Magdeburg	ICA	ICA	1	5.684
24	161B	Magdeburg	Magdeburg	ICA	ICA	0	2.089
25	161C	Magdeburg	Magdeburg	PICA	posterior	0	2.497
26	162	Magdeburg	Magdeburg	AChA	ICA	1	4.811
27	163	Magdeburg	Magdeburg	ICA	ICA	0	4.981
28	164	Magdeburg	Magdeburg	MCA	MCA	0	3.817
29	165A	Magdeburg	Magdeburg	MCA	MCA	0	3.419
30	165B	Magdeburg	Magdeburg	PCoMA	posterior	0	5.533
31	165C	Magdeburg	Magdeburg	BA	posterior	0	2.856
32	165D	Magdeburg	Magdeburg	SCA	posterior	1	4.595
33	166	Magdeburg	Magdeburg	ICA	ICA	0	3.638
34	167	Magdeburg	Magdeburg	ICA	ICA	0	3.481
35	168	Magdeburg	Magdeburg	ICA	ICA	0	6.061
36	169	Magdeburg	Magdeburg	ICA	ICA	0	7.142
37	170	Magdeburg	Magdeburg	ICA	ICA	0	5.557
38	171	Magdeburg	Magdeburg	ICA	ICA	0	11.276
39	172A	Magdeburg	Magdeburg	ACoMA	anterior	1	3.283
40	172B	Magdeburg	Magdeburg	MCA	MCA	0	2.319
41	173A	Magdeburg	Magdeburg	MCA	MCA	1	4.176
42	173B	Magdeburg	Magdeburg	ICA	ICA	0	3.188
43	174	Magdeburg	Magdeburg	ICA	ICA	0	3.711
44	175	Magdeburg	Magdeburg	MCA	MCA	0	4.156
45	176	Magdeburg	Magdeburg	ACoMA	anterior	0	3.397
46	177A	Magdeburg	Magdeburg	PCoMA	posterior	1	6.322
47	177B	Magdeburg	Magdeburg	BA	posterior	0	1.516
48	178	Magdeburg	Magdeburg	MCA	MCA	1	5.269
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	maximum c	maximum h	maximum d	bulge height	surface area	convex hull	minimal box	closed area	volume
	L_max	H_max	D_max	H_b	A	A_CH	A_MBS	A_closed	V
	mm	mm	mm	mm	cm ²	cm ²	cm ²	cm ²	ml
5	6.629	5.790	5.713	0.877	0.887	1.018	1.495	1.003	0.083
6	11.888	8.544	10.931	3.003	2.391	2.722	4.652	2.537	0.269
7	7.306	6.133	4.862	0.313	0.742	0.914	1.677	0.888	0.064
8	7.867	6.544	7.165	3.567	1.018	1.146	1.979	1.122	0.097
9	7.336	6.315	6.104	1.929	0.888	1.022	1.749	1.014	0.085
10	6.275	4.482	5.783	0.575	0.693	0.906	1.269	0.900	0.074
11	23.888	20.508	23.475	9.621	12.495	13.243	18.371	13.239	4.106
12	6.597	4.534	6.403	1.473	0.746	0.934	1.422	0.924	0.076
13	5.837	3.939	5.183	0.070	0.568	0.802	1.099	0.795	0.060
14	6.518	5.449	5.861	2.398	0.713	0.822	1.338	0.809	0.059
15	8.495	6.902	7.441	3.391	1.540	1.813	2.341	1.803	0.215
16	11.246	9.797	10.200	3.153	1.755	1.899	3.981	1.853	0.195
17	11.394	8.611	10.972	4.429	2.218	2.475	4.079	2.459	0.334
18	7.308	4.479	7.292	0.287	0.574	0.844	1.684	0.826	0.059
19	4.672	3.411	4.157	0.033	0.354	0.489	0.729	0.486	0.027
20	13.627	11.834	11.081	4.341	3.153	3.480	5.839	3.381	0.526
21	2.875	1.899	2.875	0.057	0.126	0.180	0.276	0.178	0.006
22	14.303	12.591	12.333	6.473	3.921	4.285	6.591	4.242	0.730
23	3.763	2.874	3.382	1.302	0.281	0.342	0.445	0.341	0.018
24	5.669	4.725	4.473	2.104	0.553	0.648	1.015	0.643	0.044
25	7.910	6.289	6.673	3.770	1.024	1.175	1.970	1.151	0.101
26	6.439	5.233	5.830	1.474	0.815	0.991	1.327	0.978	0.081
27	12.632	11.229	10.859	3.425	3.001	3.307	5.029	3.293	0.523
28	8.453	6.020	7.820	1.936	0.987	1.244	2.245	1.236	0.112
29	9.521	8.035	9.229	3.504	2.125	2.439	2.878	2.433	0.344
30	8.530	5.733	7.294	1.949	1.050	1.420	2.328	1.397	0.132
31	4.793	3.005	4.741	0.075	0.310	0.479	0.797	0.470	0.025
32	14.667	10.280	13.848	1.293	4.122	5.440	6.782	5.419	1.129
33	7.677	4.990	6.526	2.190	0.873	1.094	1.890	1.060	0.085
34	8.500	5.691	8.412	2.083	1.088	1.325	2.270	1.310	0.124
35	10.420	6.548	10.246	2.938	1.204	1.480	3.411	1.377	0.112
36	15.754	13.711	11.401	3.704	3.516	3.937	7.802	3.868	0.564
37	6.137	4.508	5.343	2.007	0.663	0.820	1.184	0.817	0.063
38	6.677	3.854	6.460	1.201	0.590	0.769	1.402	0.757	0.054
39	6.751	5.481	4.736	1.330	0.577	0.716	1.432	0.696	0.045
40	3.661	2.760	3.246	1.172	0.232	0.303	0.424	0.301	0.014
41	6.655	5.163	5.034	1.727	0.691	0.832	1.391	0.823	0.062
42	8.135	5.839	7.993	1.423	1.186	1.438	2.167	1.417	0.142
43	16.986	10.740	15.845	2.213	5.926	6.882	9.209	6.869	1.564
44	7.950	6.713	6.080	1.989	1.030	1.244	2.022	1.224	0.108
45	5.212	3.563	5.005	0.689	0.483	0.669	0.895	0.665	0.046
46	12.891	11.777	8.932	5.558	2.584	2.875	5.260	2.844	0.398
47	24.926	21.090	22.734	9.915	14.654	15.321	19.652	15.279	5.424
48	8.946	6.977	8.075	2.268	1.298	1.555	2.541	1.527	0.157
49	14.786	10.742	14.206	1.633	2.875	3.216	6.868	3.132	0.407
50	6.715	5.085	5.948	1.913	0.712	0.843	1.420	0.839	0.066
51	15.827	13.957	14.042	6.937	5.487	5.906	7.992	5.870	1.249

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2	6.419	4.551	6.134	0.624	0.618	0.839	1.316	0.813	0.058
3	8.062	6.217	6.768	2.455	1.126	1.368	2.042	1.365	0.137
4	17.188	10.658	16.238	2.250	3.236	4.445	9.425	4.430	0.696
5	7.303	4.996	6.301	1.470	0.688	0.925	1.676	0.910	0.072
6	4.605	2.692	4.603	0.037	0.296	0.466	0.713	0.462	0.023
7	4.605	3.619	3.564	1.963	0.355	0.438	0.677	0.430	0.023
8	4.653	2.599	4.537	0.354	0.303	0.480	0.698	0.475	0.025
9	13.326	11.629	11.342	5.799	3.546	3.816	5.596	3.800	0.658
10	7.105	4.947	6.019	0.113	0.678	0.891	1.586	0.882	0.061
11	4.777	2.888	4.516	0.482	0.282	0.439	0.727	0.433	0.023
12	18.334	17.219	14.463	8.226	5.638	6.064	10.560	5.978	1.232
13	11.513	9.974	11.050	4.580	2.241	2.481	4.240	2.396	0.285
14	6.880	5.489	6.061	2.068	0.829	0.999	1.492	0.993	0.086
15	4.149	2.840	3.778	0.926	0.297	0.384	0.541	0.382	0.021
16	11.234	7.779	10.623	2.600	2.129	2.279	3.965	2.254	0.282
17	6.535	5.085	5.126	0.262	0.507	0.706	1.400	0.685	0.041
18	6.195	3.881	6.006	0.616	0.577	0.840	1.210	0.829	0.061
19	4.282	2.759	3.841	0.151	0.216	0.331	0.590	0.325	0.013
20	5.968	3.703	5.938	1.423	0.517	0.678	1.119	0.668	0.043
21	4.773	4.310	4.200	2.368	0.467	0.513	0.771	0.506	0.031
22	9.479	6.686	9.469	2.116	1.305	1.446	2.823	1.429	0.139
23	4.362	2.739	4.165	0.197	0.326	0.447	0.600	0.445	0.025
24	7.928	6.831	6.578	2.903	1.256	1.465	2.026	1.456	0.154
25	2.798	1.593	2.792	0.014	0.105	0.170	0.266	0.167	0.005
26	6.330	3.703	6.047	0.954	0.580	0.806	1.259	0.803	0.058
27	7.668	6.509	6.943	1.249	0.852	1.054	1.873	0.999	0.070
28	8.038	5.767	7.357	1.708	0.972	1.152	2.030	1.143	0.103
29	13.384	9.880	12.864	3.835	3.174	3.751	5.854	3.690	0.603
30	4.583	3.361	4.077	0.084	0.364	0.502	0.704	0.498	0.030
31	13.573	12.129	7.940	6.398	2.411	2.619	5.788	2.564	0.328
32	6.253	4.782	5.560	2.596	0.679	0.785	1.232	0.782	0.060
33	6.774	5.738	4.776	1.687	0.752	0.882	1.467	0.876	0.070
34	19.580	14.862	19.183	7.524	7.554	7.889	12.044	7.851	1.917
35	10.702	7.977	8.927	2.139	2.019	2.495	3.606	2.481	0.325
36	6.698	4.629	5.540	0.489	0.576	0.764	1.410	0.757	0.055
37	6.354	4.692	5.177	1.312	0.626	0.795	1.289	0.776	0.053
38	6.204	3.207	6.016	0.114	0.413	0.706	1.215	0.694	0.044
39	14.376	13.009	10.934	6.325	2.638	2.994	6.492	2.830	0.343
40	6.016	4.460	5.142	0.926	0.678	0.873	1.149	0.866	0.071
41	5.832	3.890	5.511	0.286	0.536	0.691	1.071	0.684	0.046
42	14.708	12.119	12.964	4.615	3.419	3.829	6.796	3.791	0.609
43	5.100	3.825	4.479	0.525	0.452	0.611	0.840	0.603	0.038
44	10.529	8.923	7.517	2.011	1.266	1.421	3.483	1.355	0.113
45	6.886	3.607	6.764	0.185	0.510	0.851	1.490	0.837	0.060
46	4.974	3.155	4.670	0.739	0.312	0.487	0.792	0.479	0.026
47	6.182	5.235	3.884	2.072	0.422	0.503	1.203	0.487	0.025
48	8.405	5.927	8.296	2.748	1.255	1.408	2.270	1.385	0.133
49	15.254	10.492	15.251	1.120	3.825	4.559	7.665	4.507	0.804
50	7.735	5.096	7.199	1.289	0.956	1.265	1.925	1.236	0.115
51	11.062	9.776	9.388	5.048	2.352	2.598	3.900	2.577	0.353
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2	9.022	8.308	5.532	5.605	1.258	1.403	2.566	1.369	0.125
3	32.342	25.628	30.344	9.085	21.842	22.485	32.901	22.541	9.061
4	3.400	2.107	3.340	0.103	0.171	0.249	0.382	0.247	0.010
5	5.047	4.006	3.660	0.257	0.368	0.480	0.802	0.479	0.028
6	3.134	1.819	3.062	0.002	0.128	0.204	0.325	0.203	0.007
7	13.558	11.007	11.469	5.880	3.372	4.048	5.907	3.950	0.645
8	8.282	6.772	7.749	2.957	1.357	1.578	2.227	1.567	0.170
9	5.390	3.909	3.582	0.036	0.363	0.503	0.917	0.497	0.029
10	5.401	3.552	5.038	1.301	0.435	0.613	0.917	0.611	0.042
11	3.966	2.604	3.799	0.123	0.269	0.369	0.506	0.368	0.019
12	5.633	4.386	4.464	0.942	0.531	0.621	1.001	0.614	0.039
13	3.149	1.664	3.147	0.170	0.102	0.155	0.311	0.153	0.005
14	3.784	2.577	3.258	0.475	0.191	0.258	0.454	0.256	0.011
15	7.951	6.459	5.903	0.045	0.885	1.210	2.142	1.167	0.093
16	6.817	4.506	6.387	1.055	0.691	0.886	1.462	0.880	0.067
17	7.784	6.322	6.895	2.712	1.231	1.415	1.903	1.412	0.152
18	12.441	7.739	12.162	1.572	2.313	2.941	4.898	2.904	0.402
19	16.422	12.513	15.861	2.894	4.492	4.998	8.482	4.966	0.797
20	27.009	21.425	25.069	8.693	14.959	16.042	22.918	16.010	5.763
21	8.947	7.350	6.990	2.234	1.135	1.351	2.515	1.341	0.128
22	13.291	8.491	13.104	0.615	2.474	3.251	5.883	3.166	0.379
23	5.671	2.993	5.671	0.100	0.283	0.495	1.011	0.489	0.019
24	8.214	5.554	7.968	1.932	1.237	1.574	2.124	1.572	0.170
25	5.584	4.790	4.319	2.528	0.481	0.539	0.980	0.527	0.031
26	9.725	6.554	9.274	1.314	1.459	1.953	2.971	1.944	0.238
27	16.284	12.471	15.055	0.726	3.620	4.000	8.331	3.963	0.645
28	3.707	2.472	3.379	0.531	0.221	0.311	0.445	0.309	0.014
29	16.159	11.384	16.159	4.627	3.858	4.256	8.203	4.029	0.506
30	4.053	2.688	3.620	0.707	0.258	0.349	0.516	0.347	0.016
31	3.744	1.985	3.743	0.076	0.186	0.285	0.442	0.282	0.011
32	6.956	5.626	4.803	1.591	0.669	0.821	1.525	0.808	0.058
33	7.936	6.362	7.128	3.081	1.178	1.318	2.163	1.302	0.120
34	9.195	6.126	7.318	1.738	1.708	1.836	2.661	1.858	0.209
35	17.009	8.810	16.189	0.942	2.437	3.849	9.088	3.752	0.562
36	9.263	7.602	7.208	3.536	1.222	1.383	2.696	1.338	0.114
37	10.514	8.759	7.409	3.082	1.494	1.771	3.482	1.712	0.151
38	10.231	8.838	7.094	2.851	1.488	1.803	3.372	1.739	0.166
39	6.100	4.339	5.591	0.679	0.516	0.732	1.220	0.722	0.048
40	17.012	13.949	16.935	6.552	6.058	6.416	9.100	6.386	1.433
41	18.621	14.380	14.373	6.548	4.829	5.408	10.893	5.328	0.999
42	9.774	6.785	8.878	1.968	1.741	2.204	3.001	2.190	0.285
43	10.375	7.553	9.325	3.307	1.779	2.280	3.443	2.262	0.286
44	11.542	9.849	7.908	4.661	2.103	2.433	4.190	2.390	0.308
45	8.757	6.907	8.753	2.415	1.552	1.848	2.420	1.841	0.224
46	6.793	4.234	6.753	0.367	0.597	0.920	1.502	0.910	0.068
47	6.195	5.019	5.753	2.072	0.634	0.738	1.213	0.721	0.049
48	2.123	1.222	2.050	0.099	0.062	0.091	0.144	0.089	0.002
49	7.276	4.568	7.267	1.827	0.795	0.957	1.663	0.935	0.073
50	2.744	1.425	2.563	0.133	0.078	0.128	0.237	0.123	0.003
51	10.853	8.721	9.956	2.319	2.269	2.569	3.723	2.547	0.342
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2	6.386	4.271	6.267	1.450	0.622	0.798	1.282	0.779	0.052
3	7.385	6.025	5.712	3.287	0.847	0.981	1.714	0.961	0.077
4	6.224	4.693	5.826	1.532	0.584	0.710	1.218	0.686	0.040
5	2.739	1.458	2.699	0.000	0.079	0.137	0.248	0.129	0.003
6	6.758	5.613	6.202	3.057	0.747	0.850	1.552	0.826	0.060
7	8.335	5.295	8.154	0.578	0.472	0.673	2.182	0.626	0.032
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9	24.223	19.791	22.453	9.808	12.666	13.149	18.524	13.126	4.170
10	9.429	7.753	9.246	3.668	1.763	2.018	2.881	1.991	0.233
11	7.279	5.501	6.496	1.296	0.962	1.180	1.701	1.156	0.093
12	4.951	3.068	4.238	0.721	0.311	0.403	0.770	0.396	0.018
13	3.677	3.075	2.630	1.197	0.197	0.240	0.431	0.230	0.008
14	3.184	1.674	2.913	0.185	0.096	0.166	0.322	0.159	0.004
15	4.432	3.209	4.075	1.200	0.283	0.349	0.626	0.346	0.016
16	8.784	7.818	6.956	3.946	1.370	1.477	2.435	1.460	0.148
17	13.905	9.021	13.148	0.801	2.857	3.336	6.331	3.136	0.362
18	7.117	5.697	7.117	1.111	0.959	1.100	1.716	1.067	0.083
19	4.398	3.418	3.652	1.122	0.260	0.319	0.609	0.314	0.014
20	4.263	2.616	3.714	0.022	0.236	0.323	0.576	0.316	0.014
21	3.378	1.853	3.377	0.224	0.119	0.210	0.389	0.196	0.005
22	5.130	2.891	4.336	0.308	0.177	0.292	0.827	0.275	0.008
23	5.027	3.392	4.348	1.368	0.315	0.392	0.795	0.385	0.019
24	2.603	1.519	2.548	0.128	0.096	0.144	0.214	0.138	0.004
25	8.733	7.733	5.173	2.236	1.000	1.104	2.399	1.082	0.087
26	6.282	4.788	4.997	1.219	0.529	0.634	1.242	0.623	0.038
27	6.960	6.297	6.263	3.045	0.617	0.691	1.556	0.649	0.035
28	6.109	4.679	5.536	1.914	0.602	0.685	1.173	0.680	0.047
29	8.258	5.056	7.901	0.962	0.957	1.190	2.143	1.166	0.099
30	21.893	19.479	15.008	5.305	5.825	6.171	15.090	6.046	1.094
31	7.690	6.527	5.130	2.092	0.820	0.984	1.861	0.906	0.058
32	4.236	3.327	2.935	1.359	0.267	0.320	0.564	0.310	0.014
33	7.909	6.999	6.604	1.846	1.191	1.329	1.991	1.306	0.123
34	5.815	3.677	4.000	0.846	0.324	0.434	1.062	0.406	0.019
35	7.097	4.213	6.014	0.103	0.332	0.541	1.582	0.515	0.023
36	2.628	1.504	2.617	0.126	0.075	0.129	0.227	0.120	0.003
37	6.801	6.385	4.171	3.307	0.723	0.806	1.476	0.797	0.058
38	5.605	3.754	5.144	1.846	0.487	0.608	0.987	0.597	0.037
39	6.085	4.188	5.097	1.013	0.566	0.707	1.164	0.693	0.046
40	10.066	6.868	9.700	2.978	1.972	2.370	3.227	2.338	0.291
41	11.565	10.869	9.066	5.115	2.694	2.806	4.206	2.801	0.417
42	10.003	8.861	9.695	3.555	2.151	2.310	3.143	2.295	0.306
43	6.948	6.210	4.669	2.279	0.766	0.840	1.517	0.825	0.061
44	8.098	6.481	7.268	3.584	1.033	1.168	2.064	1.144	0.093
45	15.923	12.736	11.639	3.653	3.319	3.922	7.966	3.711	0.511
46	9.220	8.728	6.525	5.970	1.325	1.489	2.729	1.424	0.127
47	8.947	7.049	8.891	2.469	1.606	1.828	2.595	1.814	0.208
48	3.410	2.529	3.319	1.196	0.188	0.222	0.369	0.217	0.008
49	6.977	5.759	5.449	1.556	0.777	0.934	1.530	0.903	0.066
50	1.627	0.900	1.540	0.310	0.031	0.050	0.090	0.047	0.001
51	1.571	0.846	1.511	0.124	0.026	0.044	0.080	0.041	0.001
52	4.670	3.829	3.715	0.862	0.374	0.442	0.707	0.433	0.023
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2	2.495	1.472	2.180	0.087	0.072	0.103	0.196	0.100	0.002
3	2.449	1.457	2.325	0.046	0.086	0.131	0.194	0.125	0.003
4	9.599	6.040	9.240	1.954	1.225	1.478	2.895	1.465	0.128
5	7.998	6.644	5.913	3.660	1.019	1.183	2.072	1.148	0.100
6	7.328	5.848	5.773	2.070	0.814	0.905	1.687	0.887	0.066
7	6.486	5.072	6.312	0.846	0.639	0.755	1.334	0.750	0.052
8	7.722	6.054	7.580	2.357	1.147	1.296	1.910	1.270	0.117
9	4.784	3.869	4.102	1.291	0.329	0.390	0.719	0.383	0.019
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11	15.603	11.496	14.341	7.003	4.024	4.638	7.675	4.569	0.809
12	5.647	3.274	5.306	0.026	0.355	0.466	1.003	0.451	0.021
13	4.724	3.696	4.160	1.815	0.429	0.518	0.707	0.510	0.030
14	6.943	5.844	5.841	1.209	0.657	0.807	1.560	0.764	0.049
15	11.331	8.473	9.336	2.050	1.711	1.957	4.035	1.938	0.218
16	3.405	1.788	3.124	0.171	0.121	0.195	0.369	0.189	0.005
17	3.375	1.970	3.356	0.117	0.146	0.221	0.377	0.215	0.007
18	2.674	2.099	2.427	0.125	0.119	0.164	0.251	0.160	0.005
19	6.651	5.678	4.727	3.075	0.642	0.716	1.397	0.705	0.049
20	4.557	3.452	4.551	1.438	0.388	0.466	0.672	0.457	0.025
21	6.241	5.711	6.021	2.024	0.837	0.928	1.273	0.922	0.073
22	4.200	3.054	3.431	0.180	0.273	0.358	0.574	0.350	0.016
23	4.277	3.071	4.011	1.379	0.341	0.433	0.576	0.427	0.023
24	7.789	6.371	6.026	2.151	0.819	0.987	1.906	0.932	0.060
25	2.779	2.123	2.323	0.573	0.137	0.172	0.243	0.171	0.006
26	3.590	2.777	3.414	1.580	0.240	0.286	0.408	0.278	0.012
27	6.957	6.079	6.471	2.907	0.713	0.780	1.524	0.750	0.048
28	5.784	5.145	4.269	1.733	0.498	0.560	1.051	0.547	0.030
29	5.795	4.770	4.652	1.961	0.401	0.530	1.068	0.476	0.021
30	5.333	3.786	4.835	0.986	0.424	0.507	0.893	0.498	0.028
31	7.607	6.500	4.457	3.691	0.723	0.793	1.818	0.773	0.053
32	4.095	3.019	3.578	1.043	0.276	0.374	0.556	0.364	0.017
33	5.900	5.509	4.218	3.215	0.545	0.570	1.098	0.557	0.031
34	5.574	3.949	5.005	1.532	0.505	0.630	0.977	0.624	0.041
35	5.053	3.735	4.455	1.533	0.398	0.461	0.803	0.454	0.025
36	9.075	6.193	9.068	2.564	1.532	1.753	2.802	1.731	0.191
37	7.748	7.232	7.453	3.980	1.306	1.395	1.963	1.378	0.139
38	7.203	5.799	5.440	1.852	0.826	0.957	1.631	0.925	0.070
39	15.720	12.308	14.026	4.352	4.479	5.063	7.782	5.036	0.977
40	5.186	4.052	3.267	1.796	0.280	0.347	0.845	0.322	0.012
41	5.388	2.932	4.739	0.773	0.335	0.421	0.912	0.407	0.018
42	6.487	5.148	5.922	1.965	0.654	0.765	1.340	0.742	0.050
43	5.446	3.837	5.297	1.539	0.461	0.549	0.932	0.537	0.031
44	4.406	3.846	4.243	1.228	0.391	0.445	0.653	0.440	0.025
45	5.714	4.684	5.562	1.815	0.544	0.612	1.026	0.588	0.034
46	5.047	4.191	3.070	1.619	0.276	0.311	0.801	0.289	0.012
47	7.755	6.941	4.725	4.013	0.823	0.909	1.891	0.893	0.066
48	2.901	1.778	2.668	0.019	0.107	0.158	0.278	0.150	0.004
49	6.661	5.753	4.657	1.227	0.646	0.769	1.394	0.738	0.048
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	ml	ml	mm	mm	mm	mm	cm ²	cm ²	-
5	0.091	0.172	2.903	3.885	13.086	3.537	0.116	0.089	1.479
6	0.372	0.943	2.992	5.434	17.029	3.417	0.145	0.128	1.520
7	0.071	0.204	3.276	4.862	14.831	3.926	0.146	0.125	1.239
8	0.105	0.262	2.412	3.903	13.317	3.147	0.105	0.074	1.460
9	0.087	0.217	2.835	4.497	15.471	3.260	0.126	0.100	1.260
10	0.076	0.134	4.243	5.252	19.040	4.336	0.206	0.175	0.543
11	4.299	7.404	7.102	11.374	37.990	7.833	0.744	0.634	1.721
12	0.080	0.160	2.937	5.732	18.940	3.767	0.178	0.132	0.733
13	0.062	0.108	3.700	5.163	19.585	4.624	0.226	0.150	0.735
14	0.062	0.145	3.135	3.555	11.360	3.390	0.096	0.088	1.421
15	0.219	0.337	4.061	6.687	22.302	4.713	0.263	0.213	1.015
16	0.211	0.747	2.896	4.022	12.395	3.169	0.098	0.091	1.892
17	0.343	0.775	4.591	6.207	19.420	4.961	0.241	0.224	1.314
18	0.064	0.205	3.911	6.350	21.036	4.791	0.252	0.195	0.400
19	0.028	0.058	3.525	4.157	13.267	3.968	0.132	0.115	0.769
20	0.567	1.327	4.216	6.408	19.835	4.605	0.228	0.212	1.496
21	0.006	0.014	1.920	2.875	8.841	2.356	0.052	0.043	0.654
22	0.765	1.591	5.778	6.676	22.660	5.667	0.321	0.303	1.837
23	0.018	0.028	2.370	2.886	9.061	2.653	0.060	0.054	0.967
24	0.045	0.096	2.781	3.684	11.481	3.120	0.090	0.080	1.230
25	0.110	0.260	3.374	4.360	13.771	3.700	0.127	0.116	1.284
26	0.085	0.144	4.129	4.939	15.345	4.263	0.164	0.160	1.048
27	0.535	1.061	5.283	6.859	21.247	5.494	0.292	0.285	1.541
28	0.116	0.316	4.399	6.782	20.002	4.982	0.249	0.234	0.732
29	0.349	0.459	5.692	6.345	21.843	5.642	0.308	0.284	1.246
30	0.144	0.334	5.051	7.400	24.248	5.730	0.347	0.294	0.621
31	0.027	0.067	3.554	4.752	15.381	4.143	0.159	0.133	0.612
32	1.148	1.661	6.103	13.945	53.525	9.693	1.297	0.668	0.608
33	0.096	0.244	3.241	5.421	18.057	4.145	0.187	0.138	0.776
34	0.131	0.322	4.742	5.937	19.016	4.669	0.222	0.221	0.774
35	0.140	0.592	3.148	5.233	16.748	4.119	0.172	0.129	1.047
36	0.640	2.049	6.067	6.812	24.497	5.741	0.352	0.325	1.876
37	0.065	0.121	3.929	4.537	15.469	3.986	0.154	0.140	0.899
38	0.057	0.156	2.964	5.044	16.782	3.982	0.167	0.117	0.622
39	0.049	0.161	2.859	4.073	13.567	3.522	0.119	0.091	1.249
40	0.015	0.026	2.338	3.094	9.103	3.028	0.069	0.057	0.878
41	0.065	0.154	3.388	4.395	14.337	3.683	0.132	0.117	1.134
42	0.150	0.300	4.221	5.874	20.243	4.553	0.230	0.195	0.773
43	1.618	2.628	7.460	14.252	45.129	8.355	0.943	0.835	0.665
44	0.118	0.270	3.389	5.919	16.909	4.575	0.193	0.158	1.049
45	0.048	0.080	4.100	4.888	16.858	4.339	0.183	0.157	0.692
46	0.413	1.134	4.955	5.832	21.532	4.829	0.260	0.227	2.005
47	5.489	8.192	4.856	13.272	38.744	6.453	0.625	0.506	1.563
48	0.166	0.381	4.146	5.861	19.226	4.767	0.229	0.191	0.946
49	0.471	1.692	4.251	6.311	19.493	5.268	0.257	0.211	1.331
50	0.068	0.159	3.330	4.548	14.206	3.568	0.127	0.119	0.943
51	1.284	2.125	5.828	7.791	26.972	5.678	0.383	0.357	1.769

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2	0.065	0.142	2.869	6.280	18.787	4.153	0.195	0.141	0.685
3	0.140	0.274	5.099	5.722	19.742	4.850	0.239	0.229	1.030
4	0.723	2.721	9.411	15.328	45.262	10.554	1.194	1.133	0.448
5	0.076	0.204	3.921	5.390	19.347	4.578	0.221	0.166	0.782
6	0.025	0.057	4.072	4.605	15.924	4.153	0.165	0.147	0.524
7	0.025	0.052	2.544	3.498	10.509	2.840	0.075	0.070	1.001
8	0.027	0.055	3.973	4.537	15.822	4.355	0.172	0.142	0.506
9	0.671	1.245	5.067	6.060	20.235	5.028	0.254	0.241	1.844
10	0.067	0.188	4.039	6.019	18.197	4.473	0.203	0.191	0.770
11	0.024	0.058	3.349	4.139	15.221	3.971	0.151	0.109	0.532
12	1.284	3.227	3.904	8.491	26.453	5.140	0.340	0.260	2.001
13	0.334	0.821	3.698	5.097	15.808	3.937	0.156	0.148	1.489
14	0.088	0.171	3.652	5.028	14.943	4.393	0.164	0.144	1.004
15	0.021	0.037	2.695	3.182	10.976	3.122	0.086	0.067	0.874
16	0.296	0.742	3.682	4.035	12.878	3.887	0.125	0.117	1.693
17	0.047	0.156	3.958	5.126	15.600	4.569	0.178	0.159	0.948
18	0.065	0.125	3.926	6.009	20.114	5.003	0.252	0.185	0.554
19	0.015	0.043	3.044	3.841	13.047	3.343	0.109	0.092	0.545
20	0.048	0.111	3.747	4.646	14.887	4.055	0.151	0.137	0.609
21	0.032	0.064	1.743	2.212	6.685	2.312	0.039	0.030	1.934
22	0.146	0.446	3.494	4.013	13.901	3.573	0.124	0.110	1.223
23	0.026	0.044	3.340	4.165	13.007	3.667	0.119	0.109	0.616
24	0.158	0.271	3.373	5.696	18.626	4.310	0.201	0.151	1.161
25	0.006	0.013	2.149	2.798	9.586	2.605	0.062	0.047	0.549
26	0.059	0.133	4.544	5.666	18.559	4.809	0.223	0.202	0.554
27	0.088	0.241	3.240	5.327	15.348	3.834	0.147	0.136	0.751
28	0.106	0.272	3.982	5.445	15.999	4.286	0.171	0.170	0.895
29	0.635	1.332	5.655	8.968	30.914	6.682	0.516	0.398	0.953
30	0.031	0.056	3.242	4.090	14.393	3.732	0.134	0.104	0.775
31	0.352	1.309	4.023	4.674	15.332	4.004	0.153	0.148	2.325
32	0.062	0.129	3.028	3.756	12.271	3.335	0.102	0.089	1.209
33	0.072	0.167	3.273	4.162	13.626	3.661	0.125	0.107	1.327
34	1.971	3.931	5.400	6.936	23.221	5.117	0.297	0.294	1.995
35	0.349	0.644	6.668	7.542	25.103	7.353	0.461	0.395	1.030
36	0.057	0.157	2.954	5.757	18.913	3.839	0.182	0.134	0.634
37	0.060	0.138	3.374	4.303	14.245	4.211	0.150	0.114	0.937
38	0.048	0.126	4.114	6.204	23.009	4.885	0.281	0.200	0.431
39	0.410	1.556	4.088	5.305	16.784	4.591	0.193	0.170	2.214
40	0.073	0.116	2.687	5.335	20.340	3.712	0.189	0.113	0.513
41	0.049	0.104	2.559	5.530	16.327	3.620	0.148	0.111	0.666
42	0.647	1.666	5.581	7.501	23.891	6.226	0.372	0.329	1.329
43	0.041	0.072	3.421	4.484	14.463	4.178	0.151	0.120	0.841
44	0.133	0.611	2.123	4.861	12.221	2.913	0.089	0.081	1.572
45	0.064	0.171	4.645	6.823	21.514	6.082	0.327	0.249	0.355
46	0.029	0.066	3.453	4.611	16.463	4.059	0.167	0.125	0.494
47	0.028	0.124	2.466	2.877	9.725	2.697	0.066	0.056	1.584
48	0.144	0.322	2.931	4.907	13.849	3.745	0.130	0.113	1.014
49	0.831	1.995	3.693	15.254	44.240	6.164	0.682	0.442	0.666
50	0.123	0.251	3.660	5.911	21.822	5.129	0.280	0.170	0.849
51	0.370	0.724	4.471	5.481	18.185	4.966	0.226	0.193	1.679
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2	0.138	0.387	3.088	3.831	12.450	3.565	0.111	0.093	2.122
3	9.561	17.746	2.961	18.027	50.338	5.556	0.699	0.419	1.193
4	0.010	0.022	2.536	3.340	10.417	2.938	0.077	0.067	0.611
5	0.028	0.068	2.961	3.628	12.388	3.587	0.111	0.084	1.019
6	0.007	0.017	2.669	3.062	9.724	3.065	0.075	0.064	0.485
7	0.709	1.350	6.233	9.921	32.559	7.095	0.578	0.486	1.059
8	0.177	0.312	3.682	5.598	18.267	4.597	0.210	0.162	1.131
9	0.030	0.083	3.109	3.713	13.372	4.008	0.134	0.091	0.945
10	0.043	0.083	2.949	4.596	16.118	4.349	0.175	0.106	0.652
11	0.019	0.034	3.058	3.824	11.763	3.366	0.099	0.092	0.673
12	0.041	0.094	2.402	3.999	11.654	2.840	0.083	0.075	0.993
13	0.005	0.016	1.871	3.149	9.064	2.252	0.051	0.046	0.473
14	0.011	0.029	2.480	2.749	9.781	2.680	0.066	0.054	0.838
15	0.105	0.295	5.164	6.092	19.890	5.675	0.282	0.247	0.940
16	0.071	0.166	3.647	5.591	18.794	4.024	0.189	0.160	0.718
17	0.154	0.247	3.845	5.198	17.087	4.221	0.180	0.157	1.182
18	0.433	1.019	7.600	9.255	32.052	7.377	0.591	0.552	0.759
19	0.946	2.323	5.854	9.288	29.079	6.525	0.474	0.427	1.117
20	5.822	10.316	10.249	12.646	43.430	9.687	1.052	1.018	1.517
21	0.133	0.375	4.577	4.981	16.951	4.848	0.205	0.179	1.257
22	0.457	1.342	6.603	9.821	38.845	7.126	0.692	0.509	0.530
23	0.021	0.096	4.180	5.671	18.176	4.536	0.206	0.186	0.300
24	0.173	0.291	5.563	7.294	22.990	5.826	0.335	0.319	0.738
25	0.033	0.091	1.425	2.956	8.692	2.091	0.045	0.033	1.531
26	0.242	0.482	6.692	7.545	27.655	7.023	0.486	0.397	0.804
27	0.673	2.261	4.714	7.341	25.595	5.352	0.342	0.272	0.918
28	0.014	0.028	3.033	3.304	11.382	3.083	0.088	0.079	0.715
29	0.705	2.209	3.936	5.479	16.917	4.038	0.171	0.169	1.545
30	0.017	0.035	2.888	3.555	11.320	3.126	0.088	0.081	0.700
31	0.012	0.028	2.723	3.744	12.259	3.122	0.096	0.080	0.511
32	0.062	0.177	3.927	4.189	14.081	3.967	0.140	0.129	1.205
33	0.129	0.299	3.261	4.724	14.375	3.444	0.124	0.121	1.255
34	0.223	0.408	1.690	6.942	22.424	2.675	0.150	0.092	0.807
35	0.604	2.576	9.516	16.051	57.167	9.204	1.315	1.200	0.288
36	0.133	0.416	3.427	4.118	13.379	3.487	0.117	0.111	1.722
37	0.190	0.611	4.209	5.875	18.330	4.775	0.219	0.194	1.392
38	0.200	0.582	4.580	5.781	20.002	5.026	0.251	0.208	1.487
39	0.052	0.127	4.276	4.986	17.482	4.697	0.205	0.167	0.779
40	1.463	2.581	5.536	7.179	23.516	5.577	0.328	0.312	1.939
41	1.064	3.380	4.917	12.472	34.457	5.794	0.499	0.482	1.010
42	0.294	0.489	4.505	8.378	31.391	5.719	0.449	0.296	0.719
43	0.301	0.601	6.063	8.092	28.011	6.899	0.483	0.385	0.865
44	0.323	0.806	3.486	7.314	23.602	4.859	0.287	0.200	1.297
45	0.227	0.354	3.933	6.501	22.813	5.068	0.289	0.201	0.960
46	0.072	0.173	4.796	6.793	21.520	5.804	0.312	0.256	0.533
47	0.054	0.126	2.981	3.763	11.219	3.091	0.087	0.088	1.153
48	0.002	0.005	1.667	2.050	6.305	1.717	0.027	0.027	0.561
49	0.080	0.202	3.798	4.688	14.879	3.770	0.140	0.140	0.865
50	0.003	0.011	2.058	2.646	8.188	2.184	0.045	0.043	0.390
51	0.364	0.676	4.880	7.274	20.777	5.344	0.278	0.279	1.165
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2	0.059	0.136	3.633	5.216	16.163	3.879	0.157	0.149	0.784
3	0.083	0.211	3.466	3.933	13.148	3.467	0.114	0.107	1.281
4	0.049	0.126	3.027	4.428	12.646	3.207	0.101	0.105	1.023
5	0.004	0.012	2.254	2.739	9.026	2.224	0.050	0.048	0.413
6	0.066	0.182	2.509	4.164	11.013	2.871	0.079	0.082	1.172
7	0.040	0.303	3.046	6.031	16.366	3.781	0.155	0.144	0.385
8	4.307	7.497	4.943	11.565	29.411	6.256	0.460	0.449	1.617
9	0.251	0.460	3.312	6.808	19.810	4.592	0.227	0.177	0.979
10	0.109	0.209	4.469	5.198	17.058	4.553	0.194	0.182	1.006
11	0.020	0.064	2.612	4.202	11.337	3.013	0.085	0.086	0.710
12	0.010	0.027	1.673	2.354	6.665	1.998	0.033	0.031	1.238
13	0.005	0.017	2.558	3.184	9.667	2.606	0.063	0.064	0.377
14	0.017	0.047	2.537	3.163	9.173	2.730	0.063	0.063	0.845
15	0.156	0.357	3.105	3.630	11.718	3.059	0.090	0.089	1.984
16	0.496	1.498	3.688	7.971	23.076	4.837	0.279	0.231	1.062
17	0.097	0.211	3.514	3.858	12.669	3.425	0.108	0.106	1.402
18	0.015	0.045	2.234	2.843	9.386	2.324	0.055	0.050	0.937
19	0.015	0.041	3.000	3.715	10.778	2.970	0.080	0.088	0.565
20	0.007	0.023	2.662	3.378	11.376	2.694	0.077	0.071	0.423
21	0.010	0.071	2.885	4.088	12.580	3.113	0.098	0.093	0.312
22	0.020	0.067	2.674	3.641	10.202	2.743	0.070	0.076	0.774
23	0.005	0.009	1.941	2.438	8.082	2.096	0.042	0.037	0.530
24	0.094	0.349	2.932	3.509	10.841	3.047	0.083	0.081	2.044
25	0.042	0.130	2.598	4.490	11.942	3.133	0.094	0.092	0.946
26	0.044	0.182	1.604	2.311	6.687	1.877	0.031	0.029	2.104
27	0.049	0.119	2.818	3.448	10.414	2.988	0.078	0.076	1.158
28	0.112	0.295	4.647	5.228	18.128	4.607	0.209	0.191	0.834
29	1.181	5.512	3.626	7.662	19.509	4.543	0.222	0.218	2.164
30	0.078	0.239	2.966	3.629	11.960	2.882	0.086	0.085	1.665
31	0.016	0.040	2.054	2.604	8.405	2.090	0.044	0.042	1.193
32	0.133	0.264	3.526	4.008	13.454	3.419	0.115	0.111	1.572
33	0.023	0.103	2.488	4.181	11.759	2.758	0.081	0.082	0.733
34	0.028	0.187	3.376	6.094	16.842	4.360	0.184	0.162	0.395
35	0.003	0.010	2.058	2.628	8.482	2.109	0.045	0.042	0.422
36	0.060	0.169	2.876	3.210	9.865	3.022	0.075	0.072	1.979
37	0.041	0.092	2.534	4.791	13.958	3.151	0.110	0.095	0.683
38	0.051	0.118	3.367	4.437	14.181	3.586	0.127	0.117	0.909
39	0.323	0.545	4.747	9.608	24.939	5.860	0.365	0.358	0.651
40	0.424	0.811	2.828	4.463	12.938	3.306	0.107	0.099	2.356
41	0.315	0.524	3.432	4.980	14.519	3.980	0.144	0.134	1.701
42	0.066	0.176	2.482	3.060	9.082	2.609	0.059	0.060	1.963
43	0.108	0.279	2.829	4.298	13.230	3.376	0.112	0.095	1.206
44	0.639	2.114	4.957	9.395	25.968	6.032	0.392	0.366	1.109
45	0.148	0.424	3.121	3.948	11.926	3.295	0.098	0.097	2.209
46	0.221	0.393	3.803	6.053	18.164	4.583	0.208	0.181	1.031
47	0.009	0.021	1.782	2.158	6.541	1.799	0.029	0.030	0.933
48	0.077	0.178	3.345	4.520	13.440	3.752	0.126	0.119	1.234
49	0.001	0.003	1.249	1.627	4.931	1.263	0.016	0.016	0.420
50	0.001	0.002	1.171	1.571	5.218	1.191	0.016	0.014	0.365
51	0.025	0.056	2.550	2.828	9.049	2.602	0.059	0.057	1.291
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2	0.003	0.008	1.614	2.232	6.529	1.706	0.028	0.028	0.544
3	0.004	0.008	2.024	2.328	7.829	1.956	0.038	0.037	0.595
4	0.152	0.463	3.752	6.083	20.202	4.746	0.240	0.179	0.764
5	0.110	0.280	3.307	5.198	14.592	3.553	0.130	0.135	1.248
6	0.074	0.206	2.337	3.921	10.721	2.726	0.073	0.072	1.265
7	0.054	0.145	3.253	4.288	12.309	3.606	0.111	0.110	0.924
8	0.130	0.248	3.443	4.427	13.709	3.601	0.123	0.120	1.325
9	0.020	0.057	2.337	2.977	8.842	2.448	0.054	0.055	1.207
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11	0.875	1.999	5.504	11.272	31.139	6.996	0.545	0.487	0.882
12	0.025	0.094	2.229	5.284	13.469	2.867	0.097	0.093	0.481
13	0.033	0.056	2.807	3.647	10.997	2.972	0.082	0.080	0.984
14	0.058	0.183	3.309	4.297	13.094	3.291	0.108	0.112	1.192
15	0.230	0.762	4.694	6.020	17.946	5.054	0.227	0.222	1.171
16	0.006	0.021	2.550	3.222	9.787	2.806	0.069	0.065	0.377
17	0.008	0.022	2.539	3.357	10.019	2.758	0.069	0.067	0.526
18	0.006	0.012	1.792	2.444	7.653	2.150	0.041	0.034	0.834
19	0.051	0.155	2.582	3.108	9.392	2.699	0.063	0.063	1.671
20	0.027	0.052	2.791	3.230	9.826	2.820	0.069	0.071	1.005
21	0.078	0.135	3.086	3.614	10.669	3.209	0.086	0.088	1.562
22	0.018	0.041	2.968	3.431	10.338	2.993	0.077	0.080	0.871
23	0.025	0.041	2.996	3.439	10.693	3.209	0.086	0.081	0.826
24	0.080	0.247	3.390	4.303	13.330	3.390	0.113	0.115	1.321
25	0.006	0.011	1.980	2.183	6.667	2.038	0.034	0.034	0.957
26	0.013	0.024	1.860	2.600	7.731	1.939	0.037	0.038	0.960
27	0.057	0.177	1.771	2.520	7.349	2.020	0.037	0.035	1.909
28	0.034	0.101	2.142	2.834	8.480	2.306	0.049	0.048	1.758
29	0.030	0.104	2.525	3.927	10.784	2.783	0.075	0.078	0.972
30	0.031	0.079	2.552	3.426	10.614	2.776	0.074	0.069	0.998
31	0.058	0.230	2.391	2.810	8.625	2.316	0.050	0.053	1.969
32	0.019	0.039	3.067	3.601	11.501	3.064	0.088	0.087	0.793
33	0.036	0.108	0.981	1.591	4.414	1.106	0.012	0.012	2.888
34	0.043	0.091	3.448	4.293	13.109	3.606	0.118	0.116	0.848
35	0.027	0.068	2.188	3.205	9.355	2.372	0.055	0.055	1.086
36	0.204	0.441	4.669	5.375	16.745	4.748	0.199	0.197	1.128
37	0.145	0.259	2.815	3.184	10.027	2.889	0.072	0.070	2.243
38	0.079	0.196	3.412	3.903	11.686	3.419	0.100	0.105	1.424
39	1.014	2.041	6.801	10.575	28.975	7.694	0.557	0.565	1.066
40	0.016	0.073	1.988	2.577	7.813	2.160	0.042	0.040	1.274
41	0.022	0.082	2.507	3.337	10.511	2.750	0.072	0.066	0.695
42	0.056	0.146	3.141	3.432	11.178	3.152	0.088	0.085	1.217
43	0.034	0.085	2.409	3.774	10.852	2.821	0.077	0.071	0.845
44	0.026	0.050	2.316	2.781	8.572	2.264	0.049	0.051	1.334
45	0.040	0.098	2.113	2.553	7.909	2.222	0.044	0.042	1.627
46	0.014	0.067	1.016	1.949	4.922	1.111	0.014	0.016	1.743
47	0.071	0.245	2.801	3.116	10.051	2.771	0.070	0.069	2.029
48	0.005	0.014	1.964	2.682	8.337	2.070	0.043	0.041	0.565
49	0.056	0.155	3.187	3.553	11.772	3.139	0.092	0.089	1.483
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eAR	BF	BL	NSI	AVSV	AASA	UI	EI	MAA			mm ⁻¹
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5	1.625	1.471	0.153	0.270	0.485	0.671	0.079	0.240	0.318		
6	2.417	2.012	0.364	0.370	0.285	0.545	0.277	0.271	0.254		
7	1.534	1.000	0.052	0.311	0.311	0.529	0.101	0.282	0.322		
8	1.811	1.836	0.626	0.278	0.370	0.567	0.077	0.255	0.302		
9	1.739	1.358	0.340	0.270	0.390	0.580	0.023	0.264	0.325		
10	0.657	1.101	0.202	0.249	0.549	0.709	0.034	0.237	0.322		
11	2.499	2.064	0.491	0.257	0.555	0.721	0.045	0.234	0.090		
12	1.115	1.117	0.351	0.254	0.478	0.650	0.043	0.240	0.324		
13	0.821	1.004	0.019	0.258	0.555	0.723	0.037	0.247	0.308		
14	1.490	1.649	0.475	0.279	0.407	0.605	0.046	0.267	0.354		
15	1.441	1.113	0.499	0.236	0.639	0.770	0.018	0.231	0.239		
16	2.401	2.536	0.414	0.304	0.261	0.465	0.077	0.284	0.259		
17	1.644	1.768	0.543	0.249	0.431	0.603	0.027	0.240	0.216		
18	0.531	1.148	0.113	0.299	0.285	0.491	0.079	0.275	0.356		
19	0.805	1.000	0.010	0.291	0.460	0.667	0.039	0.276	0.401		
20	2.082	1.729	0.453	0.261	0.396	0.579	0.073	0.245	0.185		
21	0.798	1.000	0.031	0.289	0.441	0.647	0.037	0.277	0.666		
22	2.164	1.847	0.528	0.267	0.459	0.644	0.047	0.251	0.163		
23	1.052	1.172	0.466	0.239	0.628	0.766	0.017	0.233	0.524		
24	1.452	1.214	0.464	0.260	0.454	0.633	0.029	0.251	0.389		
25	1.513	1.531	0.674	0.275	0.390	0.584	0.074	0.252	0.292		
26	1.214	1.180	0.285	0.266	0.562	0.737	0.054	0.248	0.315		
27	1.924	1.583	0.324	0.243	0.494	0.655	0.022	0.235	0.179		
28	0.997	1.153	0.390	0.278	0.354	0.550	0.034	0.266	0.283		
29	1.402	1.454	0.443	0.226	0.748	0.845	0.016	0.220	0.200		
30	0.802	0.986	0.424	0.286	0.396	0.600	0.079	0.259	0.239		
31	0.701	0.998	0.026	0.297	0.377	0.589	0.080	0.272	0.357		
32	0.874	0.993	0.153	0.232	0.680	0.799	0.016	0.226	0.132		
33	1.016	1.204	0.520	0.299	0.349	0.561	0.112	0.264	0.321		
34	0.985	1.417	0.453	0.271	0.385	0.577	0.053	0.253	0.303		
35	1.330	1.958	0.536	0.354	0.188	0.404	0.204	0.300	0.317		
36	2.226	1.674	0.290	0.322	0.275	0.496	0.119	0.276	0.176		
37	1.023	1.178	0.492	0.254	0.522	0.690	0.024	0.245	0.337		
38	0.787	1.281	0.383	0.279	0.344	0.540	0.066	0.257	0.354		
39	1.444	1.163	0.261	0.307	0.277	0.486	0.099	0.278	0.371		
40	0.897	1.049	0.432	0.258	0.539	0.709	0.039	0.243	0.499		
41	1.353	1.145	0.347	0.266	0.404	0.591	0.042	0.253	0.325		
42	0.998	1.361	0.313	0.263	0.473	0.654	0.055	0.246	0.271		
43	1.134	1.112	0.234	0.247	0.595	0.746	0.033	0.231	0.128		
44	1.358	1.027	0.320	0.288	0.400	0.605	0.087	0.256	0.284		
45	0.780	1.024	0.204	0.259	0.578	0.743	0.032	0.248	0.335		
46	2.421	1.532	0.475	0.270	0.351	0.541	0.036	0.259	0.193		
47	3.215	1.713	0.478	0.224	0.662	0.777	0.012	0.220	0.088		
48	1.163	1.378	0.409	0.268	0.413	0.601	0.055	0.254	0.274		
49	1.594	2.251	0.194	0.327	0.241	0.456	0.136	0.277	0.212		
50	1.202	1.308	0.446	0.255	0.413	0.591	0.032	0.242	0.336		
51	2.428	1.802	0.503	0.242	0.588	0.734	0.027	0.232	0.135		
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2	1.036	0.977	0.145	0.297	0.405	0.618	0.109	0.264	0.331
3	1.215	1.183	0.417	0.254	0.499	0.669	0.022	0.244	0.258
4	0.651	1.059	0.327	0.319	0.256	0.470	0.037	0.304	0.154
5	0.920	1.169	0.349	0.271	0.352	0.543	0.052	0.257	0.345
6	0.581	1.000	0.015	0.318	0.415	0.647	0.050	0.301	0.368
7	1.233	1.019	0.561	0.280	0.437	0.635	0.069	0.258	0.435
8	0.527	1.000	0.154	0.309	0.456	0.680	0.067	0.284	0.343
9	2.223	1.872	0.519	0.236	0.528	0.679	0.019	0.229	0.169
10	1.037	1.000	0.024	0.329	0.323	0.556	0.099	0.287	0.313
11	0.555	1.091	0.219	0.279	0.399	0.596	0.047	0.265	0.413
12	3.305	1.703	0.484	0.262	0.382	0.566	0.041	0.252	0.142
13	1.927	2.168	0.604	0.306	0.347	0.565	0.145	0.256	0.232
14	1.149	1.205	0.410	0.246	0.503	0.666	0.026	0.237	0.314
15	0.890	1.187	0.333	0.238	0.559	0.706	0.019	0.231	0.494
16	1.757	2.633	0.381	0.268	0.380	0.569	0.049	0.251	0.223
17	1.063	1.000	0.054	0.332	0.264	0.489	0.126	0.292	0.373
18	0.666	0.999	0.185	0.282	0.488	0.685	0.059	0.262	0.302
19	0.626	1.000	0.072	0.336	0.313	0.550	0.102	0.301	0.437
20	0.698	1.278	0.503	0.299	0.383	0.597	0.104	0.257	0.391
21	1.850	1.899	0.554	0.259	0.479	0.656	0.059	0.239	0.432
22	1.374	2.359	0.431	0.279	0.312	0.506	0.047	0.264	0.285
23	0.700	1.000	0.077	0.267	0.568	0.742	0.027	0.255	0.443
24	1.534	1.155	0.439	0.242	0.569	0.719	0.027	0.233	0.261
25	0.590	0.998	0.009	0.309	0.405	0.630	0.084	0.281	0.578
26	0.653	1.067	0.304	0.284	0.437	0.638	0.025	0.274	0.355
27	1.043	1.303	0.312	0.347	0.290	0.533	0.202	0.281	0.330
28	1.137	1.351	0.350	0.262	0.379	0.563	0.031	0.253	0.321
29	1.279	1.434	0.449	0.258	0.453	0.630	0.051	0.244	0.176
30	0.850	0.997	0.026	0.264	0.531	0.708	0.044	0.248	0.397
31	2.714	1.699	0.589	0.288	0.251	0.443	0.067	0.270	0.220
32	1.361	1.480	0.572	0.244	0.470	0.635	0.018	0.238	0.367
33	1.509	1.147	0.305	0.255	0.420	0.597	0.025	0.247	0.326
34	2.705	2.766	0.544	0.245	0.488	0.652	0.027	0.235	0.119
35	1.056	1.184	0.275	0.268	0.505	0.688	0.068	0.237	0.167
36	0.951	0.962	0.134	0.271	0.346	0.537	0.041	0.258	0.334
37	0.957	1.203	0.325	0.298	0.388	0.602	0.103	0.263	0.331
38	0.547	0.970	0.043	0.307	0.353	0.572	0.072	0.283	0.258
39	2.558	2.061	0.539	0.335	0.221	0.436	0.163	0.293	0.213
40	0.738	0.964	0.338	0.238	0.616	0.754	0.029	0.228	0.320
41	1.018	0.996	0.078	0.276	0.444	0.639	0.063	0.252	0.293
42	1.601	1.728	0.463	0.272	0.366	0.558	0.059	0.250	0.157
43	0.902	0.999	0.139	0.280	0.526	0.718	0.069	0.254	0.354
44	2.623	1.546	0.263	0.339	0.185	0.389	0.152	0.296	0.310
45	0.398	0.991	0.076	0.300	0.349	0.562	0.070	0.277	0.298
46	0.561	1.013	0.325	0.291	0.396	0.605	0.081	0.264	0.374
47	1.690	1.350	0.455	0.324	0.203	0.405	0.088	0.304	0.462
48	1.328	1.691	0.552	0.279	0.413	0.610	0.078	0.251	0.273
49	1.649	1.000	0.110	0.263	0.403	0.588	0.033	0.255	0.148
50	0.979	1.218	0.257	0.267	0.457	0.642	0.070	0.248	0.296
51	1.853	1.713	0.549	0.256	0.488	0.661	0.045	0.239	0.181
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2	2.281	1.444	0.689	0.298	0.324	0.534	0.091	0.270	0.297
3	3.872	1.683	0.422	0.260	0.511	0.685	0.052	0.231	0.073
4	0.694	1.000	0.050	0.295	0.436	0.647	0.057	0.271	0.532
5	1.031	1.009	0.069	0.257	0.417	0.597	0.009	0.255	0.456
6	0.485	1.000	0.001	0.301	0.407	0.623	0.018	0.296	0.593
7	1.480	1.156	0.560	0.275	0.478	0.669	0.091	0.246	0.152
8	1.377	1.384	0.467	0.247	0.545	0.704	0.039	0.232	0.241
9	0.875	0.965	0.010	0.278	0.346	0.542	0.053	0.260	0.393
10	0.689	1.096	0.434	0.238	0.511	0.666	0.017	0.232	0.406
11	0.765	0.994	0.048	0.262	0.556	0.727	0.021	0.253	0.494
12	1.398	1.116	0.237	0.278	0.416	0.613	0.051	0.261	0.401
13	0.661	0.999	0.114	0.313	0.276	0.490	0.059	0.295	0.631
14	0.860	1.185	0.206	0.270	0.375	0.565	0.042	0.255	0.565
15	1.009	0.969	0.008	0.325	0.315	0.545	0.115	0.294	0.283
16	0.998	1.142	0.263	0.277	0.406	0.602	0.047	0.259	0.353
17	1.456	1.326	0.441	0.227	0.614	0.742	0.012	0.222	0.274
18	0.952	1.314	0.224	0.280	0.395	0.593	0.070	0.253	0.198
19	1.590	1.708	0.279	0.336	0.343	0.586	0.158	0.260	0.163
20	1.980	1.982	0.453	0.229	0.559	0.699	0.010	0.226	0.088
21	1.291	1.403	0.357	0.271	0.343	0.533	0.037	0.258	0.286
22	0.730	1.334	0.118	0.365	0.283	0.538	0.170	0.299	0.230
23	0.375	1.000	0.059	0.449	0.195	0.484	0.115	0.409	0.320
24	0.924	1.092	0.359	0.251	0.584	0.740	0.016	0.244	0.268
25	2.164	1.461	0.559	0.277	0.342	0.538	0.060	0.263	0.453
26	0.864	1.229	0.217	0.241	0.495	0.654	0.016	0.236	0.243
27	1.259	2.051	0.108	0.277	0.285	0.476	0.041	0.263	0.182
28	0.767	1.023	0.225	0.293	0.487	0.695	0.054	0.271	0.483
29	2.097	2.949	0.546	0.395	0.229	0.491	0.282	0.285	0.215
30	0.796	1.018	0.284	0.285	0.471	0.672	0.044	0.267	0.482
31	0.613	1.000	0.040	0.335	0.390	0.637	0.134	0.277	0.535
32	1.273	1.147	0.315	0.288	0.328	0.530	0.064	0.268	0.354
33	1.722	1.509	0.519	0.283	0.401	0.602	0.072	0.256	0.303
34	2.094	1.054	0.310	0.272	0.512	0.698	0.064	0.230	0.254
35	0.503	1.009	0.204	0.303	0.218	0.413	0.069	0.288	0.174
36	2.034	1.750	0.499	0.327	0.273	0.496	0.148	0.275	0.304
37	1.712	1.261	0.377	0.364	0.247	0.492	0.205	0.283	0.281
38	1.711	1.227	0.332	0.334	0.285	0.516	0.172	0.271	0.255
39	0.827	1.121	0.175	0.298	0.379	0.592	0.071	0.272	0.346
40	2.496	2.359	0.471	0.236	0.555	0.702	0.021	0.229	0.137
41	2.173	1.152	0.520	0.280	0.296	0.489	0.061	0.260	0.138
42	1.053	1.060	0.327	0.241	0.584	0.730	0.029	0.230	0.197
43	1.015	1.152	0.472	0.264	0.475	0.657	0.052	0.243	0.184
44	1.953	1.081	0.491	0.267	0.382	0.570	0.046	0.258	0.206
45	1.232	1.346	0.387	0.231	0.633	0.761	0.013	0.227	0.245
46	0.624	0.994	0.101	0.300	0.390	0.606	0.056	0.281	0.278
47	1.404	1.529	0.477	0.289	0.388	0.594	0.095	0.258	0.401
48	0.669	1.000	0.086	0.317	0.389	0.619	0.083	0.295	0.974
49	1.076	1.550	0.450	0.282	0.363	0.562	0.090	0.253	0.328
50	0.472	0.969	0.129	0.365	0.268	0.520	0.154	0.315	0.791
51	1.586	1.369	0.274	0.262	0.507	0.684	0.060	0.238	0.198
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2	1.054	1.201	0.355	0.310	0.384	0.608	0.117	0.267	0.349
3	1.453	1.452	0.652	0.279	0.363	0.561	0.078	0.254	0.339
4	1.412	1.316	0.338	0.345	0.316	0.563	0.180	0.278	0.418
5	0.509	0.985	0.000	0.415	0.237	0.520	0.241	0.341	0.717
6	1.700	1.489	0.626	0.290	0.329	0.532	0.091	0.265	0.359
7	0.615	1.352	0.249	0.387	0.104	0.287	0.215	0.329	0.418
8	2.990	1.941	0.524	0.242	0.556	0.709	0.032	0.227	0.092
9	1.452	1.358	0.550	0.269	0.507	0.691	0.070	0.243	0.237
10	1.149	1.250	0.248	0.317	0.447	0.680	0.142	0.259	0.296
11	0.990	1.009	0.242	0.339	0.281	0.514	0.113	0.296	0.459
12	1.459	1.117	0.411	0.319	0.310	0.533	0.146	0.276	0.646
13	0.461	0.915	0.154	0.420	0.217	0.495	0.213	0.349	0.588
14	0.979	1.289	0.449	0.293	0.344	0.552	0.055	0.274	0.566
15	2.355	1.916	0.548	0.264	0.415	0.599	0.051	0.247	0.269
16	1.750	1.650	0.095	0.378	0.242	0.495	0.270	0.279	0.226
17	1.580	1.845	0.205	0.313	0.394	0.622	0.141	0.263	0.347
18	1.146	1.285	0.421	0.284	0.318	0.516	0.080	0.254	0.594
19	0.706	1.000	0.010	0.303	0.334	0.548	0.075	0.282	0.538
20	0.530	1.000	0.157	0.402	0.233	0.503	0.195	0.355	0.507
21	0.410	1.061	0.241	0.443	0.113	0.333	0.239	0.370	0.537
22	1.027	1.194	0.485	0.299	0.280	0.485	0.078	0.273	0.501
23	0.617	1.045	0.099	0.340	0.394	0.647	0.200	0.262	0.841
24	2.354	1.474	0.312	0.305	0.248	0.451	0.079	0.280	0.315
25	1.355	1.113	0.287	0.305	0.291	0.501	0.098	0.269	0.398
26	2.590	2.710	0.626	0.371	0.190	0.417	0.218	0.305	0.462
27	1.336	1.605	0.479	0.265	0.392	0.579	0.050	0.246	0.397
28	0.946	1.511	0.221	0.295	0.336	0.544	0.118	0.249	0.289
29	3.649	1.959	0.320	0.326	0.199	0.401	0.074	0.305	0.151
30	2.097	1.414	0.346	0.366	0.243	0.487	0.261	0.285	0.355
31	1.486	1.127	0.438	0.271	0.360	0.551	0.091	0.247	0.546
32	1.842	1.648	0.293	0.274	0.465	0.656	0.076	0.247	0.279
33	1.112	0.957	0.276	0.323	0.186	0.382	0.159	0.290	0.471
34	0.552	0.987	0.043	0.396	0.123	0.326	0.180	0.344	0.392
35	0.526	0.996	0.113	0.357	0.279	0.527	0.180	0.317	0.764
36	2.102	1.299	0.521	0.280	0.343	0.540	0.042	0.268	0.364
37	1.039	1.074	0.564	0.284	0.403	0.605	0.100	0.246	0.419
38	1.125	1.149	0.251	0.288	0.390	0.595	0.102	0.251	0.378
39	1.068	1.010	0.476	0.279	0.533	0.725	0.101	0.237	0.207
40	3.180	2.032	0.487	0.236	0.514	0.666	0.017	0.229	0.207
41	2.128	1.947	0.420	0.240	0.584	0.730	0.029	0.230	0.211
42	2.303	1.525	0.379	0.275	0.350	0.544	0.072	0.252	0.354
43	1.536	1.691	0.692	0.313	0.333	0.554	0.138	0.256	0.331
44	1.728	1.239	0.351	0.339	0.242	0.466	0.201	0.274	0.189
45	2.647	1.653	0.685	0.319	0.299	0.522	0.142	0.279	0.284
46	1.362	1.469	0.396	0.257	0.529	0.699	0.059	0.233	0.244
47	1.119	1.538	0.595	0.288	0.384	0.589	0.086	0.261	0.685
48	1.487	1.206	0.279	0.306	0.371	0.590	0.138	0.259	0.331
49	0.542	0.946	0.453	0.346	0.283	0.523	0.186	0.289	1.245
50	0.481	0.962	0.216	0.379	0.260	0.520	0.222	0.310	1.290
51	1.403	1.314	0.236	0.291	0.404	0.612	0.096	0.258	0.498
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2	0.711	0.977	0.072	0.350	0.270	0.510	0.175	0.286	0.960
3	0.708	0.998	0.033	0.322	0.406	0.642	0.142	0.283	0.778
4	0.980	1.519	0.420	0.333	0.277	0.506	0.154	0.261	0.273
5	1.826	1.137	0.564	0.281	0.356	0.554	0.090	0.257	0.286
6	1.820	1.472	0.417	0.290	0.323	0.526	0.097	0.255	0.339
7	1.099	1.472	0.213	0.286	0.359	0.562	0.041	0.272	0.360
8	1.629	1.712	0.402	0.277	0.472	0.665	0.101	0.240	0.288
9	1.468	1.378	0.359	0.288	0.330	0.533	0.071	0.266	0.513
10	1.421	1.272	0.704	0.270	0.405	0.595	0.075	0.243	0.158
11	0.887	1.004	0.010	0.354	0.222	0.450	0.172	0.290	0.503
12	1.207	1.141	0.506	0.268	0.543	0.721	0.073	0.241	0.427
13	1.556	1.359	0.236	0.324	0.270	0.490	0.155	0.284	0.360
14	1.395	1.551	0.291	0.282	0.286	0.480	0.051	0.264	0.222
15	0.432	0.970	0.141	0.391	0.247	0.513	0.180	0.323	0.548
16	0.640	1.000	0.066	0.355	0.317	0.572	0.129	0.310	0.553
17	0.948	0.993	0.061	0.298	0.422	0.637	0.094	0.267	0.685
18	1.924	1.521	0.592	0.274	0.314	0.505	0.048	0.261	0.385
19	1.151	1.409	0.443	0.276	0.489	0.680	0.078	0.251	0.443
20	1.759	1.666	0.358	0.272	0.542	0.725	0.062	0.245	0.330
21	0.999	1.000	0.060	0.308	0.387	0.610	0.109	0.270	0.463
22	0.886	1.166	0.485	0.265	0.569	0.741	0.067	0.240	0.439
23	1.677	1.400	0.378	0.369	0.242	0.489	0.251	0.278	0.358
24	1.025	1.064	0.274	0.260	0.532	0.704	0.026	0.252	0.717
25	1.287	1.313	0.633	0.284	0.481	0.681	0.112	0.248	0.603
26	2.382	2.568	0.604	0.321	0.273	0.492	0.156	0.268	0.404
27	2.160	1.506	0.348	0.320	0.298	0.521	0.102	0.286	0.439
28	1.372	1.184	0.514	0.395	0.198	0.446	0.325	0.294	0.524
29	1.231	1.411	0.288	0.294	0.349	0.557	0.099	0.256	0.453
30	2.389	1.586	0.667	0.295	0.232	0.425	0.075	0.276	0.374
31	0.932	0.994	0.365	0.305	0.434	0.655	0.102	0.272	0.483
32	4.155	2.651	0.700	0.325	0.284	0.507	0.137	0.272	0.473
33	1.009	1.166	0.421	0.266	0.454	0.639	0.044	0.252	0.377
34	1.468	1.390	0.440	0.274	0.372	0.565	0.063	0.254	0.475
35	1.277	1.687	0.423	0.265	0.432	0.618	0.063	0.242	0.231
36	2.472	2.341	0.557	0.254	0.537	0.702	0.046	0.239	0.274
37	1.625	1.394	0.333	0.295	0.358	0.568	0.111	0.263	0.329
38	1.466	1.326	0.386	0.250	0.478	0.647	0.037	0.235	0.142
39	1.520	1.268	0.547	0.363	0.169	0.381	0.221	0.303	0.600
40	0.843	1.420	0.333	0.352	0.220	0.447	0.171	0.290	0.536
41	1.325	1.726	0.471	0.302	0.340	0.554	0.113	0.265	0.381
42	1.130	1.404	0.483	0.289	0.371	0.576	0.088	0.261	0.405
43	1.639	1.526	0.331	0.261	0.497	0.674	0.048	0.244	0.474
44	1.870	2.178	0.437	0.320	0.344	0.573	0.168	0.262	0.442
45	3.059	1.575	0.476	0.309	0.176	0.361	0.142	0.289	0.651
46	2.282	1.516	0.635	0.300	0.269	0.472	0.077	0.275	0.360
47	0.732	0.995	0.012	0.324	0.313	0.541	0.148	0.286	0.680
48	1.679	1.311	0.233	0.310	0.313	0.530	0.136	0.269	0.383
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	absMAA	MSD	HMC	MLN	GAA	absGAA	GSD	HGC	GLN
	mm ⁻¹	mm ⁻¹	%	-	mm ⁻²	mm ⁻²	mm ⁻²	%	-
5	0.370	0.303	27.483	0.329	0.069	0.227	0.376	170.270	2.699
6	0.328	0.307	99.650	0.491	0.034	0.179	0.308	561.209	5.898
7	0.382	0.330	39.608	0.316	0.048	0.220	0.383	193.206	2.283
8	0.343	0.255	35.989	0.317	0.050	0.192	0.287	202.369	2.361
9	0.337	0.247	25.724	0.306	0.081	0.152	0.244	111.783	1.818
10	0.348	0.234	10.601	0.264	0.090	0.155	0.217	56.300	1.293
11	0.140	0.155	68.740	0.506	0.006	0.030	0.072	337.335	7.205
12	0.379	0.315	27.518	0.311	0.080	0.199	0.306	125.715	1.876
13	0.325	0.237	-4.035	0.233	0.076	0.159	0.256	38.871	1.205
14	0.376	0.331	22.618	0.325	0.092	0.203	0.412	115.984	2.393
15	0.248	0.178	7.167	0.294	0.047	0.083	0.136	54.474	1.768
16	0.294	0.242	65.689	0.374	0.041	0.130	0.235	310.560	3.334
17	0.232	0.170	32.321	0.326	0.042	0.071	0.102	131.248	1.942
18	0.380	0.249	39.230	0.262	0.102	0.203	0.260	172.089	1.276
19	0.404	0.211	-2.756	0.215	0.132	0.193	0.229	12.202	0.746
20	0.215	0.197	46.687	0.382	0.024	0.082	0.158	281.687	4.003
21	0.671	0.414	-0.486	0.222	0.361	0.563	0.758	23.583	0.845
22	0.199	0.192	44.389	0.398	0.020	0.063	0.127	232.352	4.009
23	0.543	0.286	2.134	0.252	0.241	0.363	0.400	28.454	1.043
24	0.399	0.190	13.360	0.256	0.120	0.191	0.207	54.113	1.056
25	0.307	0.212	21.546	0.290	0.053	0.152	0.204	138.982	1.721
26	0.340	0.239	10.459	0.284	0.081	0.165	0.226	74.818	1.560
27	0.203	0.158	28.289	0.329	0.028	0.056	0.096	122.201	2.377
28	0.315	0.227	33.131	0.287	0.073	0.131	0.186	133.613	1.570
29	0.216	0.119	3.469	0.271	0.036	0.056	0.064	27.970	1.247
30	0.271	0.231	16.426	0.271	0.038	0.130	0.217	140.469	1.842
31	0.382	0.264	-3.851	0.197	0.096	0.246	0.282	55.765	0.735
32	0.140	0.088	2.641	0.257	0.016	0.025	0.033	36.799	1.203
33	0.387	0.372	50.037	0.365	0.077	0.284	0.468	327.761	3.296
34	0.333	0.246	41.619	0.324	0.085	0.154	0.209	177.817	1.951
35	0.354	0.270	84.214	0.364	0.055	0.217	0.303	487.876	2.950
36	0.237	0.244	86.955	0.450	0.019	0.087	0.200	441.938	5.629
37	0.371	0.235	13.847	0.266	0.100	0.161	0.201	51.703	1.185
38	0.439	0.399	46.462	0.326	0.087	0.306	0.492	240.832	2.349
39	0.407	0.281	37.388	0.281	0.076	0.231	0.343	163.135	1.613
40	0.570	0.384	4.723	0.241	0.184	0.475	0.580	60.221	1.122
41	0.362	0.272	20.362	0.280	0.081	0.167	0.275	85.294	1.573
42	0.308	0.246	27.931	0.317	0.060	0.144	0.226	147.719	2.208
43	0.164	0.148	40.176	0.378	0.015	0.033	0.059	142.546	2.862
44	0.343	0.312	37.421	0.341	0.048	0.213	0.351	242.425	2.908
45	0.387	0.269	3.259	0.237	0.098	0.204	0.253	45.488	1.042
46	0.226	0.209	46.111	0.364	0.027	0.073	0.137	206.103	2.868
47	0.096	0.068	19.469	0.339	0.007	0.012	0.020	92.486	2.471
48	0.289	0.212	30.106	0.314	0.061	0.121	0.182	145.513	1.983
49	0.281	0.269	107.395	0.461	0.030	0.133	0.249	629.400	5.743
50	0.393	0.319	32.247	0.311	0.093	0.194	0.294	119.328	1.750
51	0.165	0.153	31.289	0.381	0.015	0.037	0.066	136.383	2.960

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2	0.350	0.247	13.398	0.258	0.070	0.203	0.269	112.222	1.370
3	0.287	0.208	15.684	0.280	0.052	0.102	0.226	66.441	2.078
4	0.182	0.175	57.716	0.334	0.022	0.042	0.081	218.754	2.151
5	0.356	0.234	30.075	0.275	0.096	0.198	0.247	164.159	1.450
6	0.388	0.259	-7.566	0.195	0.122	0.195	0.277	10.566	0.715
7	0.460	0.300	6.766	0.251	0.122	0.315	0.390	69.545	1.155
8	0.407	0.329	-3.969	0.208	0.118	0.246	0.302	36.806	0.780
9	0.203	0.182	35.467	0.372	0.023	0.063	0.105	179.517	3.037
10	0.419	0.407	48.732	0.337	0.078	0.257	0.381	224.679	2.102
11	0.473	0.333	13.718	0.224	0.139	0.309	0.393	78.607	0.935
12	0.161	0.146	47.887	0.385	0.015	0.043	0.081	264.046	3.689
13	0.278	0.232	61.744	0.390	0.035	0.115	0.193	289.460	3.489
14	0.343	0.232	18.223	0.283	0.082	0.158	0.233	88.126	1.628
15	0.516	0.267	7.079	0.243	0.221	0.329	0.340	41.759	0.958
16	0.275	0.261	54.542	0.398	0.039	0.108	0.207	242.212	3.573
17	0.402	0.312	34.161	0.275	0.096	0.248	0.417	176.386	1.726
18	0.327	0.269	1.580	0.244	0.071	0.179	0.283	72.216	1.339
19	0.523	0.441	13.316	0.229	0.147	0.443	0.626	107.707	1.104
20	0.491	0.422	46.646	0.329	0.120	0.372	0.524	231.396	2.211
21	0.484	0.309	19.917	0.289	0.080	0.373	0.597	129.208	2.242
22	0.318	0.236	50.879	0.336	0.061	0.135	0.240	202.896	2.567
23	0.463	0.263	1.081	0.234	0.180	0.269	0.319	28.479	0.951
24	0.298	0.229	19.650	0.310	0.057	0.120	0.208	94.046	2.157
25	0.601	0.450	-12.547	0.189	0.274	0.589	0.757	24.710	0.673
26	0.368	0.232	16.362	0.257	0.120	0.161	0.209	60.852	1.110
27	0.385	0.324	48.503	0.340	0.063	0.256	0.413	281.276	2.831
28	0.340	0.253	36.700	0.321	0.085	0.162	0.290	161.584	2.334
29	0.205	0.197	40.081	0.374	0.025	0.068	0.150	216.724	3.849
30	0.437	0.302	3.354	0.240	0.136	0.240	0.328	34.409	1.029
31	0.234	0.160	59.080	0.336	0.034	0.082	0.108	276.784	2.173
32	0.374	0.216	17.165	0.279	0.114	0.175	0.261	71.811	1.539
33	0.356	0.235	21.604	0.277	0.073	0.173	0.277	101.693	1.713
34	0.163	0.184	59.477	0.479	0.013	0.047	0.138	347.994	8.316
35	0.268	0.333	43.610	0.421	0.021	0.093	0.193	166.645	3.114
36	0.398	0.341	33.368	0.288	0.094	0.204	0.327	128.610	1.558
37	0.415	0.393	32.874	0.323	0.084	0.229	0.342	134.917	1.756
38	0.320	0.293	-0.625	0.200	0.038	0.168	0.269	62.166	0.895
39	0.255	0.212	83.131	0.388	0.023	0.103	0.163	433.185	3.457
40	0.379	0.308	14.760	0.291	0.088	0.207	0.331	89.730	1.849
41	0.395	0.322	15.166	0.254	0.043	0.241	0.361	105.098	1.550
42	0.201	0.181	48.023	0.352	0.012	0.064	0.109	248.305	2.981
43	0.392	0.291	1.273	0.245	0.094	0.233	0.293	55.595	1.109
44	0.368	0.321	93.888	0.400	0.051	0.203	0.379	462.490	3.849
45	0.350	0.276	20.654	0.231	0.081	0.163	0.223	93.445	0.961
46	0.428	0.351	7.344	0.228	0.100	0.274	0.369	72.784	0.947
47	0.478	0.292	47.932	0.282	0.105	0.283	0.429	171.297	1.482
48	0.348	0.308	47.938	0.367	0.054	0.186	0.289	236.237	2.935
49	0.167	0.145	30.251	0.322	0.010	0.043	0.078	162.837	2.388
50	0.343	0.294	34.369	0.325	0.075	0.203	0.309	211.068	2.415
51	0.234	0.207	30.349	0.335	0.016	0.074	0.146	129.073	2.742
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2	0.310	0.203	40.308	0.321	0.062	0.127	0.156	158.831	1.680
3	0.134	0.159	116.852	0.652	0.004	0.032	0.070	729.119	12.129
4	0.582	0.368	1.515	0.213	0.245	0.414	0.448	25.923	0.694
5	0.456	0.212	15.229	0.243	0.171	0.207	0.272	32.309	0.940
6	0.596	0.330	-4.095	0.194	0.295	0.427	0.550	10.610	0.637
7	0.198	0.195	35.769	0.362	0.010	0.071	0.132	235.187	3.551
8	0.287	0.219	20.911	0.302	0.047	0.113	0.167	100.239	1.872
9	0.442	0.314	19.405	0.241	0.102	0.267	0.354	94.929	1.064
10	0.422	0.250	13.919	0.250	0.164	0.215	0.238	56.828	1.001
11	0.523	0.306	4.891	0.240	0.221	0.313	0.342	26.158	0.871
12	0.462	0.355	30.353	0.311	0.127	0.265	0.410	111.064	1.816
13	0.694	0.535	9.189	0.210	0.239	0.801	1.159	98.527	0.957
14	0.632	0.437	20.122	0.248	0.262	0.507	0.657	83.067	1.073
15	0.287	0.214	18.435	0.266	0.052	0.111	0.229	88.334	1.656
16	0.384	0.290	31.078	0.302	0.114	0.181	0.260	109.950	1.561
17	0.289	0.180	12.421	0.289	0.069	0.095	0.137	43.848	1.499
18	0.240	0.200	49.804	0.341	0.036	0.079	0.118	206.468	2.274
19	0.240	0.234	97.060	0.481	0.018	0.087	0.128	487.833	4.638
20	0.095	0.071	28.605	0.350	0.007	0.012	0.023	123.417	2.849
21	0.302	0.200	35.247	0.296	0.068	0.112	0.147	124.830	1.462
22	0.324	0.338	121.985	0.512	0.040	0.148	0.249	593.122	4.969
23	0.334	0.280	-5.348	0.180	0.085	0.189	0.332	52.250	0.772
24	0.271	0.137	11.424	0.266	0.071	0.080	0.092	34.642	1.143
25	0.472	0.278	31.700	0.294	0.131	0.275	0.419	114.179	1.681
26	0.246	0.119	19.664	0.260	0.058	0.064	0.064	51.720	1.000
27	0.233	0.223	89.689	0.436	0.028	0.080	0.135	433.125	3.965
28	0.534	0.370	0.416	0.228	0.195	0.369	0.501	30.857	0.949
29	0.312	0.312	151.925	0.593	0.026	0.159	0.256	935.858	7.911
30	0.526	0.357	6.666	0.243	0.197	0.375	0.483	54.078	1.073
31	0.559	0.295	4.862	0.210	0.250	0.355	0.369	25.014	0.660
32	0.363	0.233	26.305	0.276	0.093	0.198	0.265	140.458	1.494
33	0.359	0.305	48.969	0.371	0.077	0.185	0.285	219.141	2.764
34	0.335	0.338	54.332	0.440	0.050	0.171	0.468	262.402	6.402
35	0.199	0.168	69.450	0.300	0.016	0.056	0.091	303.266	1.787
36	0.363	0.302	68.165	0.377	0.052	0.219	0.295	369.005	2.910
37	0.349	0.311	83.616	0.408	0.044	0.209	0.311	478.957	3.737
38	0.334	0.316	73.015	0.394	0.042	0.195	0.284	424.433	3.396
39	0.377	0.293	17.496	0.259	0.093	0.191	0.292	85.111	1.259
40	0.154	0.123	31.337	0.360	0.016	0.033	0.058	137.452	2.922
41	0.155	0.120	44.422	0.320	0.010	0.037	0.061	224.235	2.390
42	0.227	0.165	11.027	0.270	0.029	0.076	0.109	80.816	1.565
43	0.255	0.255	33.511	0.334	0.026	0.107	0.171	194.240	2.452
44	0.209	0.129	20.799	0.280	0.026	0.060	0.102	100.045	1.762
45	0.253	0.159	10.847	0.290	0.056	0.080	0.103	53.801	1.446
46	0.317	0.254	9.439	0.232	0.058	0.141	0.240	68.197	1.174
47	0.436	0.318	35.395	0.324	0.115	0.280	0.420	170.562	2.199
48	0.974	0.334	4.159	0.204	0.852	0.945	0.784	8.047	0.571
49	0.372	0.298	35.316	0.314	0.074	0.231	0.414	206.100	2.662
50	0.791	0.300	8.528	0.188	0.627	0.663	0.529	24.912	0.511
51	0.225	0.170	22.277	0.313	0.034	0.068	0.114	101.540	2.151
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2	0.395	0.337	26.292	0.304	0.106	0.215	0.343	119.503	1.779
3	0.345	0.208	27.427	0.291	0.095	0.150	0.229	104.142	1.671
4	0.481	0.370	49.783	0.340	0.141	0.339	0.471	228.326	2.284
5	0.717	0.172	0.717	0.165	0.476	0.494	0.292	-2.452	0.350
6	0.360	0.183	26.541	0.277	0.083	0.154	0.221	89.651	1.407
7	0.420	0.192	75.210	0.252	0.135	0.181	0.207	215.113	0.927
8	0.114	0.110	38.262	0.407	0.008	0.019	0.049	180.146	5.047
9	0.242	0.132	15.827	0.287	0.046	0.076	0.105	73.711	1.611
10	0.363	0.333	33.399	0.348	0.076	0.189	0.303	155.409	2.388
11	0.545	0.457	35.031	0.288	0.193	0.368	0.588	125.531	1.531
12	0.664	0.437	23.027	0.275	0.240	0.730	0.921	150.513	1.489
13	0.589	0.286	-5.813	0.161	0.347	0.429	0.381	9.752	0.395
14	0.568	0.184	26.758	0.252	0.283	0.309	0.258	53.829	0.861
15	0.297	0.218	30.931	0.323	0.053	0.124	0.194	140.585	2.194
16	0.290	0.329	105.626	0.537	0.032	0.148	0.425	646.131	9.678
17	0.393	0.341	45.084	0.379	0.096	0.269	0.401	266.984	3.148
18	0.594	0.180	30.718	0.252	0.316	0.331	0.285	60.140	0.880
19	0.569	0.351	21.800	0.248	0.239	0.421	1.604	92.936	3.043
20	0.523	0.311	-7.988	0.163	0.232	0.306	0.414	-5.200	0.449
21	0.543	0.371	39.201	0.218	0.241	0.362	0.570	137.911	0.872
22	0.546	0.364	37.232	0.277	0.195	0.408	0.621	157.810	1.634
23	0.873	0.447	13.886	0.235	0.691	0.832	0.948	41.574	0.896
24	0.341	0.238	48.851	0.314	0.055	0.157	0.237	200.304	1.940
25	0.440	0.311	38.254	0.292	0.125	0.259	0.359	156.080	1.601
26	0.524	0.447	84.399	0.402	0.138	0.440	0.790	445.200	3.938
27	0.431	0.279	31.785	0.299	0.136	0.222	0.294	107.420	1.554
28	0.362	0.304	49.502	0.326	0.067	0.191	0.295	224.935	2.304
29	0.165	0.136	80.958	0.391	0.015	0.035	0.074	323.417	3.489
30	0.391	0.288	50.280	0.329	0.069	0.237	0.307	251.364	2.052
31	0.551	0.257	16.638	0.248	0.216	0.402	0.423	80.139	1.007
32	0.322	0.285	28.080	0.346	0.058	0.168	0.298	165.452	2.882
33	0.482	0.297	40.044	0.252	0.141	0.354	0.464	199.146	1.251
34	0.407	0.307	44.513	0.228	0.099	0.252	0.444	217.488	1.200
35	0.767	0.275	3.142	0.177	0.594	0.632	0.378	14.077	0.420
36	0.364	0.139	24.614	0.263	0.095	0.133	0.144	56.210	0.992
37	0.425	0.219	19.227	0.263	0.137	0.223	0.314	75.266	1.328
38	0.403	0.274	22.733	0.279	0.113	0.232	0.333	114.462	1.583
39	0.264	0.252	33.935	0.365	0.031	0.116	0.252	198.855	3.979
40	0.223	0.159	28.928	0.341	0.039	0.065	0.143	118.067	3.175
41	0.256	0.244	28.024	0.377	0.031	0.105	0.236	163.323	4.077
42	0.381	0.243	32.272	0.299	0.085	0.197	0.259	138.150	1.661
43	0.385	0.313	55.871	0.369	0.082	0.234	0.360	283.973	3.034
44	0.241	0.245	92.100	0.448	0.020	0.098	0.167	521.985	4.429
45	0.308	0.213	43.675	0.325	0.043	0.134	0.208	190.504	2.243
46	0.276	0.227	25.543	0.336	0.051	0.108	0.209	122.525	2.754
47	0.703	0.413	20.526	0.276	0.370	0.689	0.789	102.406	1.304
48	0.387	0.315	34.960	0.321	0.076	0.237	0.340	188.784	2.155
49	1.246	0.507	5.409	0.190	1.456	1.771	1.521	26.783	0.528
50	1.290	0.436	2.759	0.174	1.617	1.792	1.226	13.602	0.418
51	0.520	0.377	23.268	0.304	0.197	0.380	0.577	113.641	1.815
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2	0.978	0.554	22.089	0.237	0.888	1.297	1.236	102.055	0.872
3	0.793	0.359	-1.413	0.201	0.561	0.741	0.666	14.568	0.599
4	0.371	0.370	78.107	0.406	0.058	0.229	0.371	427.990	3.659
5	0.320	0.265	29.756	0.313	0.050	0.157	0.273	158.021	2.246
6	0.414	0.326	51.809	0.338	0.073	0.248	0.370	232.553	2.444
7	0.395	0.282	28.826	0.291	0.104	0.216	0.310	129.108	1.660
8	0.349	0.308	36.082	0.359	0.061	0.192	0.311	192.483	2.890
9	0.566	0.434	35.500	0.307	0.218	0.438	0.681	150.907	1.871
10	0.201	0.237	57.108	0.454	0.011	0.091	0.499	454.480	15.975
11	0.572	0.377	61.654	0.298	0.184	0.483	0.553	285.505	1.644
12	0.450	0.243	6.697	0.256	0.150	0.274	0.309	54.358	1.170
13	0.423	0.363	49.203	0.329	0.083	0.279	0.447	246.705	2.375
14	0.270	0.257	52.916	0.353	0.041	0.090	0.158	189.102	2.229
15	0.677	0.576	15.981	0.220	0.295	0.543	0.734	59.595	0.760
16	0.615	0.430	6.457	0.213	0.291	0.469	0.609	40.678	0.786
17	0.717	0.438	1.433	0.223	0.383	0.619	0.769	23.782	0.812
18	0.394	0.224	31.241	0.284	0.101	0.197	0.275	118.561	1.495
19	0.501	0.363	15.854	0.284	0.148	0.372	0.510	98.952	1.638
20	0.416	0.481	32.256	0.425	-0.035	0.396	3.326	301.410	22.151
21	0.517	0.364	10.600	0.245	0.156	0.394	0.477	79.837	1.090
22	0.474	0.330	1.492	0.255	0.155	0.349	0.439	60.040	1.264
23	0.443	0.394	72.470	0.383	0.091	0.325	0.686	393.159	4.508
24	0.717	0.244	-0.307	0.223	0.459	0.548	0.439	5.803	0.691
25	0.631	0.386	13.614	0.279	0.315	0.503	0.598	63.297	1.292
26	0.436	0.294	51.879	0.336	0.092	0.240	0.339	190.884	1.993
27	0.492	0.408	42.402	0.337	0.126	0.340	0.542	184.095	2.209
28	0.552	0.458	60.888	0.351	0.111	0.581	0.852	393.852	2.740
29	0.518	0.409	38.234	0.316	0.150	0.401	0.663	185.284	2.293
30	0.418	0.324	58.963	0.335	0.073	0.282	0.490	307.733	2.848
31	0.529	0.450	11.413	0.276	0.194	0.421	0.745	86.600	1.692
32	0.609	0.623	80.026	0.459	0.130	0.591	1.244	415.731	5.422
33	0.409	0.258	14.050	0.259	0.115	0.203	0.303	57.781	1.302
34	0.498	0.281	25.777	0.277	0.205	0.274	0.301	75.337	1.155
35	0.297	0.299	40.100	0.372	0.042	0.133	0.260	195.973	3.215
36	0.297	0.221	17.446	0.320	0.050	0.129	0.218	100.845	2.327
37	0.380	0.315	37.038	0.330	0.069	0.253	0.385	228.068	2.567
38	0.171	0.152	34.278	0.350	0.015	0.043	0.100	163.667	3.608
39	0.611	0.415	58.447	0.307	0.181	0.614	0.818	313.327	1.864
40	0.594	0.462	60.049	0.326	0.204	0.578	0.816	319.459	2.242
41	0.424	0.366	38.583	0.340	0.107	0.296	0.508	215.801	2.702
42	0.486	0.372	32.390	0.297	0.110	0.312	0.450	131.456	1.699
43	0.513	0.295	16.990	0.278	0.186	0.333	0.424	73.202	1.443
44	0.511	0.407	46.090	0.352	0.083	0.447	0.953	264.583	4.138
45	0.653	0.286	64.988	0.297	0.187	0.566	0.711	260.920	1.612
46	0.397	0.269	54.190	0.324	0.089	0.203	0.300	205.775	2.049
47	0.742	0.476	10.353	0.216	0.421	0.637	0.722	40.798	0.712
48	0.478	0.451	59.272	0.379	0.099	0.390	0.685	332.115	3.557
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Geometric uncertainty in intracranial aneurysm rupture status discrimination: a two-site retrospective study.

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Abstract

Objectives: Assessing the risk associated with unruptured intracranial aneurysms (IA) is essential in clinical decision making. Several geometric risk parameters have been proposed for this purpose. However, performance of these parameters has been inconsistent. This study evaluates the performance and robustness of geometric risk parameters on two datasets and compare it to the uncertainty inherent in assessing these parameters and quantifies inter-parameter correlations.

Methods: Two datasets containing 244 IA geometries from 178 patients were retrospectively analyzed. IAs were stratified by anatomical region, based on the PHASES score locations. 37 geometric risk parameters representing four groups (size, neck, non-dimensional, and curvature parameters) were assessed. Analysis included standardized absolute differences (SAD) between ruptured and unruptured IAs, ratios of SAD to median relative uncertainty (MRU) associated with the parameters, and inter-parameter correlation.

Results: The ratio of SAD to MRU was lower for higher-dimensional size parameters (i.e., areas and volumes) than for one-dimensional size parameters. Non-dimensional size parameters performed comparatively well with regard to SAD and MRU. SAD was higher in the posterior anatomical region. Correlation of parameters was strongest within parameter (sub)groups and between size and curvature parameters, while anatomical region did not strongly affect correlation patterns.

Conclusion: Non-dimensional parameters and few parameters from other groups were comparatively robust, suggesting that they might generalize better to other datasets. The data on discriminative performance and inter-parameter correlations presented in this study may aid in developing and choosing robust geometric risk parameters for use in rupture risk models.

Strengths and limitations of this study

- This study provides location-specific estimates of the discriminative ability of a large set of geometric risk parameters for IA rupture risk assessment, while also considering uncertainty.
- The analysis was performed on two independent datasets to assess robustness of the findings.
- Even though the relative uncertainty in acquisition of each geometric risk parameter was evaluated based on more than 20 individual segmentations performed during the Multiple Aneurysms Anatomy Challenge, this evaluation was only performed on five aneurysms in total.

Introduction

A relevant part of the general population harbors one or more unruptured intracranial aneurysms (IAs), with the overall prevalence estimated around 3% [1]. While most IAs do not rupture [2], the question of whether and when to treat them remains relevant due to the poor prognosis of ruptured IAs [3, 4] as well as the risk of intervention [3, 5]. Current American Heart Association/American Stroke Association guidelines list several modifiable and non-modifiable risk factors for IA growth and/or rupture, including IA location, growth rate, morphology, smoking status, alcohol consumption, hypertension, age, sex, previous IA, and family history [6]. Attempts have been made to develop scoring systems to quantify rupture risk, growth risk, and/or support treatment decisions, these include the PHASES score by Greving et al. [7], the UIATS by Etminan et al. [8] and the ELAPSS score by Backes et al. [9]. All three of these scores are based on clinically available data and all include geometric rupture risk parameters: IA size in case of the PHASES score [7], surface irregularity, size ratio, as well as aspect ratio in case of the UIATS [8], and IA size as well as surface irregularity for the ELAPSS score [9]. While these metrics were designed to support clinical decision making, performance on clinical data has been mixed [10-12] and improvements, particularly for patients harboring multiple IAs, are desired by clinicians [13].

The aim of this paper is to assess the ability of a broad number of proposed geometric risk parameters to differentiate between unruptured and ruptured IAs while also comparing their discriminative ability relative to the uncertainty encountered in determining them. Any acquisition of patient-specific IA geometries and subsequent use of these geometries to derive geometric risk parameters is affected by a number of uncertainty-introducing factors. Starting with the medical imaging acquisition itself, which is followed by image data pre-processing, segmentation, geometry reconstruction including post-processing (e.g., smoothing, checking of topology), and finally calculation of the geometric risk parameters. All these processing steps are associated with some errors, resulting in uncertainty, which negatively affects the ability of parameters to discriminate IA rupture status. Discrimination of rupture status on an individual IA level is, however, necessary if these parameters are to support the clinical decision-making process, including any decisions regarding treatment modalities. Previous studies found high variability in the uncertainty of different geometric risk parameters as well as differences in their ability to differentiate between ruptured and unruptured IAs [14-16]. Furthermore, for geometric risk parameters with multiple alternative definitions, the specific implementation can affect the discriminative performance of the parameter itself and any derived parameters, as demonstrated by Lauric et al. for parameters incorporating IA and neck size [17].

The current study was performed to facilitate optimal selection of geometric rupture risk parameters by identifying geometric parameters, which are good discriminators while also exhibiting low uncertainty. The analysis is performed on two datasets processed by different research groups and is differentiated by

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3 anatomical region, in order to assess how the predictive suitability of the geometric risk parameters is
4 affected by geometry processing as well as anatomical location. Additionally, correlation of the geometric
5 risk parameters with each other is assessed.
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Methods

Medical imaging data

IA geometries were retrospectively reconstructed and segmented from 3D rotational angiography data acquired for routine clinical indications. Data was collected consecutively. The inclusion criteria of the datasets were imaging modality and the corresponding acquisition resolution. Cases with considerable segmentation artifacts such as close vessels that appear to be merged or holes in the segmented lumen were rejected from the analysis. 142 IAs were acquired in the Helios Klinikum Berlin-Buch (Berlin, Germany), 38 in KRH Klinikum Nordstadt (Hanover, Germany), 23 in the University Medical Center Schleswig-Holstein (UKSH) (Kiel, Germany), and 41 in the University Hospital Magdeburg (Magdeburg, Germany). Processing of the imaging data, including segmentation, was performed at two sites: Berlin, which processed 142 IAs from Helios Klinikum Berlin-Buch (dataset 1), and Magdeburg, which processed 102 IAs from KRH Klinikum Nordstadt, UKSH, and University Hospital Magdeburg (dataset 2). Overall, 244 IAs from 178 patients were included, from which geometric risk parameters were subsequently calculated. Based on the PHASES score [7], aneurysm location was classified into four anatomical regions: internal carotid artery (ICA), middle cerebral artery (MCA), anterior region (all vessels anterior of the ICA/MCA), and posterior region (all vessels posterior of the ICA/MCA). The distribution of the individual IA locations and their assignment to the four anatomical regions are shown in Table 1.

Table 1: Frequency and rupture status of individual IA locations by dataset. ACA: anterior cerebral artery, AComA: anterior communicating artery, AChA: anterior choroidal artery, ICA: internal carotid artery, MCA: middle cerebral artery, PComA: posterior communicating artery, PCA: posterior cerebral artery, SCA: superior cerebellar artery, BA: basilar artery, PICA: posterior inferior cerebellar artery, VA: vertebral artery.

Anatomical region	Vessel	Dataset 1 unruptured	Dataset 1 ruptured	Dataset 2 unruptured	Dataset 2 ruptured
Anterior	ACA	3	1	2	2
	AComA	10	22	11	5
ICA	AChA	0	1	1	2
	ICA	29	8	19	4
MCA	MCA	28	10	31	8
Posterior	PComA	8	10	2	4
	PCA	0	1	0	0
	SCA	0	0	1	1
	BA	4	3	3	4
	PICA	0	4	1	0
	VA	0	0	0	1

Geometric risk parameters

Historically, several geometric parameters for IA rupture risk assessment have been proposed. In order to have access to information on parameter uncertainty, the parameters chosen for this study were limited to a subset of the parameters reported in Goubergrits et al. [14], a parameter uncertainty study performed on segmentation data obtained during the Multiple Aneurysms AnaTomy Challenge (MATCH) 2018 [18]. The major outcome of this study was the median relative uncertainty (MRU) of geometric parameters. Briefly, five aneurysms were segmented and reconstructed by 26 international research groups, which participated in the MATCH challenge. These segmentations were used to calculate the median and the 68.3% range between the 84.13th and the 15.87th percentile for each of the five aneurysms. The uncertainty range was selected with respect to the range of \pm one standard deviation for normally distributed data reported in other studies. The uncertainty was defined as the uncertainty range divided by the median value and calculated for each geometric parameter. Finally, the average of all five aneurysms was calculated to define the MRU. For a detailed description of the parameters and the rationale for choosing the parameters, the interested reader is referred to Goubergrits et al. [14]. Briefly, most of the proposed geometric parameters describe aneurysm and/or aneurysmal neck size or shape, or irregularity. These parameters were previously proposed as predictors for rupture risk. Table 2 lists the geometric parameters, their abbreviations and MRU values.

Table 2: List of the investigated geometric parameters, their descriptions, and median relative uncertainties (MRU). Note that terminology and implementation in the references might differ subtly. Derived and modified from tables 1-5 from Goubergrits et al. [14], used under Creative Commons Attribution License (CC BY 4.0). The CC BY 4.0 license text is available at <https://creativecommons.org/licenses/by/4.0/>.

Parameter group	Parameter name, unit [exemplary reference]	Parameter abbreviation	Short description	MRU
Size	Height, mm [19]	H	Maximum perpendicular distance from the neck plane to the aneurysm surface	0.140
	Maximum dimension, mm [20]	L_{\max}	Maximum distance between two points on the aneurysm surface	0.157
	Maximum height, mm [15]	H_{\max}	Maximum distance between the centroid of the neck and the aneurysm surface	0.123
	Maximum diameter, mm [17]	D_{\max}	Maximum neck plane-parallel distance between two points on the aneurysm surface	0.169
	Bulge height, mm [19]	H_b	Distance between the neck plane and the maximum diameter	0.373
	Surface area, mm ² [15]	A	Surface area of the aneurysm	0.215

	Convex hull surface area, mm ² [15]	A_{CH}	Surface area of the aneurysm's convex hull	0.277
	Minimal bounding sphere surface area, mm ² [21]	A_{MBS}	Surface area of the aneurysm's minimal bounding sphere	0.305
	Closed surface area, mm ²	A_{closed}	Surface area of the neck-closed aneurysm	0.283
	Volume, mm ³ [15]	V	Volume of the neck-closed aneurysm	0.392
	Convex hull volume, mm ³ [15]	V_{CH}	Volume of the aneurysm's convex hull	0.399
	Minimal bounding sphere volume, mm ³ [21]	V_{MBS}	Volume of the aneurysm's minimal bounding sphere	0.451
Neck	Minimum neck diameter, mm [17]	$D_{neck,min}$	Minimum distance between two opposite points on the neck perimeter	0.306
	Maximum neck diameter, mm [22]	$D_{neck,max}$	Maximum distance between two points on the neck perimeter	0.348
	Neck perimeter, mm [19]	P_{neck}	Perimeter of the aneurysm neck	0.374
	Equivalent neck diameter, mm [19]	$D_{neck,equiv}$	Hydraulic diameter of the aneurysm neck	0.276
	Neck area, mm ² [19]	A_{neck}	Area of the aneurysm neck	0.593
	Elliptical neck area, mm ²	$A_{neck,elliptical}$	Neck area calculated as the product of the minimum and maximum neck diameter	0.650
Non-dimensional	Aspect ratio [22]	AR	Ratio of height to maximum neck diameter	0.293
	Equivalent aspect ratio [19]	eAR	Ratio of height to equivalent neck diameter	0.326
	Bottleneck factor [19]	BF	Ratio of maximum diameter to maximum neck diameter	0.201
	Bulge location [19]	BL	Ratio of bulge height to height	0.301
	Nonsphericity index [15]	NSI	Normalized ratio of volume to surface area relative to a hemisphere	0.108
	Aneurysm volume to bounding sphere volume [21]	AVSV	Ratio of volume to minimal bounding sphere volume	0.173
	Aneurysm surface area to bounding sphere area [21]	AASA	Ratio of surface area to minimal bounding sphere surface area	0.095

	Undulation index [15]	UI	1 minus the ratio of volume to convex hull volume	0.709
	Ellipticity index [15]	EI	Normalized ratio of convex hull volume to convex hull surface area relative to a hemisphere	0.051
Curvature	Mean of mean curvature, mm ⁻¹ [19]	MAA	Surface average of local mean curvature	0.136
	Mean of absolute mean curvature, mm ⁻¹	absMAA	Surface average of the magnitude of the local mean curvature	0.133
	Standard deviation of mean curvature, mm ⁻¹	MSD	Standard deviation of the local mean curvature	1.011
	High mean curvature, % [21]	HMC	Relative increase of the mean of absolute mean curvature over the mean curvature of the minimal bounding sphere	0.396
	L2-norm of mean curvature [19]	MLN	Scale invariant measure of surface irregularity, uses mean curvature	0.150
	Mean of Gaussian curvature, mm ⁻² [19]	GAA	Surface average of local Gaussian curvature	0.344
	Mean of absolute Gaussian curvature, mm ⁻²	absGAA	Surface average of the magnitude of the local Gaussian curvature	0.485
	Standard deviation of Gaussian curvature, mm ⁻²	GSD	Standard deviation of the local Gaussian curvature	1.798
	High Gaussian curvature, % [21]	HGC	Relative increase of the mean of absolute Gaussian curvature over the Gaussian curvature of the minimal bounding sphere	0.822
L2-norm of Gaussian curvature [19]	GLN	Scale invariant measure of surface irregularity, uses Gaussian curvature	0.545	

Since the diameter of the parent vessel was not available for all IAs studied, size ratio could not be calculated and was excluded. Furthermore, UI and CR as well as NSI and NPR are directly related through $CR = 1 - UI$ and $IPR = \frac{\sqrt[3]{18\pi}}{1 - NSI}$, respectively. CR and IPR were therefore not included in the analysis, in order to avoid redundancy. Geometric risk parameters were calculated from the IA geometries using MATLAB (version R2017b, MathWorks, Natick, USA), Python (version 3.7.1, Python Software Foundation, Delaware, USA), and ZIBAmira (version 2015.28, Zuse Institute Berlin, Germany). The individual parameter values, IA location, and rupture status for each IA in this study, as well as the exact

values of the inter-parameter correlation coefficients are provided as supplemental material 1 and 2 respectively.

Statistical analysis

Since most of the geometric risk parameters were non-normally distributed, as assessed by Q-Q plots and Shapiro-Wilk tests, the median was used to quantify central tendency and the interquartile range was used to quantify dispersion. Correlations were quantified using Pearson's r with correlations $|r| \geq 0.75$ referred to as strong, while those with $0.75 > |r| \geq 0.25$ and $|r| < 0.25$ referred to as moderate and weak, respectively. Statistical analysis was performed using SPSS (version 28.0.0.0, IBM, Armonk, USA) and MATLAB.

The discriminative ability of the individual parameters was assessed by standardizing the absolute difference between the medians of the ruptured and unruptured IAs with the weighted arithmetic mean of the IQRs of the two groups. This measure of effect size will be referred to as the standardized absolute group difference (SAD). Furthermore, the ratio of the SAD to the relative uncertainty, a measure of the uncertainty associated with parameter calculation, from Goubergrits et al. [14] was calculated for all parameters and will be referred to as the group difference-uncertainty ratio (DUR). The equations for SAD and DUR are thus $SAD = \frac{(n_r + n_u) \cdot |m_r - m_u|}{n_r IQR_r + n_u IQR_u}$ and $DUR = \frac{SAD}{MRU}$, where n_i , m_i , and IQR_i are the sample sizes, median values, and interquartile ranges of the ruptured (subscript r) and unruptured (subscript u) samples, while MRU is the median relative uncertainty from Goubergrits et al. [14], which is also listed in Table 2. SAD and DUR may take any value ≥ 0 with higher values indicating stronger discriminative ability and a better ratio of discriminative ability to uncertainty, respectively. SAD and DUR values of zero would indicate no discriminative ability and the worst possible ratio of discriminative ability to uncertainty, respectively. Additionally, the correlation coefficients between the parameters were calculated. Analysis of SAD and DUR as well as the correlation coefficients was performed individually for each anatomical region and each dataset.

Patient and public involvement

Due to the purely retrospective manner of this study, no involvement of patients or the general public was considered.

Results

Figure 1 shows SAD for all geometric risk parameters by anatomical region and dataset. Considering both datasets, the following parameters achieved the comparatively highest SAD for each anatomical region: curvature (HMC, MLN, HGC, GLN) and non-dimensional (AR, eAR, AVSV, AASA) parameters in the anterior region, curvature (HMC, HGC) and non-dimensional (NSI, AASA, EI) parameters in the ICA, non-dimensional (AR, eAR, BL, AVSV, AASA) parameters in the MCA, and size (H, L_{\max} , A, A_{MBS}) and curvature (MSD, absGAA, GSD) parameters in the posterior region. Compared to the other anatomical regions, SAD was higher in the posterior region and more parameters exhibited relatively high SAD. Looking at all anatomical regions combined, curvature (HMC, MLN, absGAA, HGC, GLN) and non-dimensional (AR, eAR, AVSV, AASA) parameters as well as one neck ($D_{\text{neck,min}}$) and one size (H_b) parameter show comparatively high SAD in both datasets. Furthermore, the differences between the two datasets become less pronounced when combining all anatomical regions. Moreover, this combined evaluation resulted in SAD being higher for the size parameters in site 2 compared to site 1. Here, it is worthwhile to note that the SAD of this combined assessment is not the average of the SAD of all four region-specific evaluations. Thus, pooling for some parameters can result in the absolute difference between the ruptured and unruptured groups to be close to zero, which results in SAD values close to zero as observed for the one-dimensional size parameters of the site 1 dataset.

Figure 2 shows DUR for all geometric risk parameters by anatomical region and dataset. Considering both datasets, the following parameters achieved the comparatively highest DUR for each anatomical region: non-dimensional (AASA, EI) and one curvature (MLN) parameter in the anterior region, non-dimensional (EI, AASA, NSI) parameters in the ICA, non-dimensional (AASA, EI) parameters in the MCA, and size parameters (H, L_{\max} , H_{\max} , A), curvature (MAA, absMAA), and one non-dimensional (EI) parameter in the posterior region. Similar to SAD, DUR in the posterior region was overall higher and more parameters exhibited relatively high DUR, compared to the other anatomical regions. Looking at all anatomical regions combined, non-dimensional (NSI, AVSV, AASA, EI) and curvature (absMAA, MLN) parameters show comparatively high DUR in both datasets. As for SAD, the differences between the two datasets are less pronounced when looking at all anatomical regions combined.

Figures 3 and 4 show correlation coefficients between the geometric risk parameters by anatomical region for both datasets. The following general features are present in most data correlation plots: The size parameters (H, L_{\max} , H_{\max} , D_{\max} , H_b , A, A_{CH} , A_{MBS} , A_{closed} , V, V_{CH} , V_{MBS}) are generally strongly correlated with each other. Similarly, the neck parameters ($D_{\text{neck,min}}$, $D_{\text{neck,max}}$, P_{neck} , $D_{\text{neck,equiv}}$, A_{neck} , $A_{\text{neck,elliptical}}$) are also generally strongly correlated with each other.

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3 Within the non-dimensional parameter group, there are two distinct subgroups in most plots: one formed by
4 AR, eAR, BF, and BL and one formed by NSI, AVSV, AASA, UI, and EI. Within the latter subgroup,
5 several of the correlations are negative but their magnitude is overall moderate to strong. The curvature
6 parameters also form two subgroups, one formed by dimensional curvature parameters (MAA, absMAA,
7 MDS, GAA, absGAA, GSD) and one by non-dimensional curvature parameters (HMC, MLN, HGC, GLN).
8 With regard to correlations between parameter groups, there is generally moderate to strong correlation
9 between the size and neck parameters. Additionally, the size and neck parameters are generally moderately
10 correlated with the curvature parameters, the direction of the correlation being positive for the non-
11 dimensional curvature parameters and negative for the dimensional curvature parameters.
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Discussion

Previous research has assessed the impact of uncertainty on geometric risk parameters in a limited fashion. Ma et al. examined the influence of random noise on the calculation of 14 geometric risk parameters, finding curvature parameters more susceptible to random noise than size, neck, and non-dimensional parameters [19]. Others have examined the influence of imaging modality [23] and CT angiography reconstruction kernel [24] on geometric risk parameters. Regarding image acquisition, Ramachandran et al. have examined the influence of imaging modality [23], while O'Meara et al. [24] and Berg et al. [25] have focused on the reconstruction kernel's effect on geometric and hemodynamic risk parameters, respectively. The current study as well as the earlier uncertainty study based on the MATCH challenge were both based on 3D rotational angiography imaging, which is the routine imaging modality in both centers involved in this study. Other sensitivity and uncertainty aspects of computational fluid dynamics approaches to IAs have been explored, e.g., by Cebral et al. [26], Sarrami-Foroushani et al. [27], and Schneiders et al. [28]. To the authors' knowledge there is, however, no comprehensive publication relating discriminative performance and uncertainty of geometric risk parameters, while also providing detailed data on their correlation with each other.

Looking at the parameter groups examined in this study, the following findings can be made: the size and neck parameters measuring areas (A , A_{CH} , A_{MBS} , A_{closed} , A_{neck} , $A_{neck,elliptical}$) and volumes (V , V_{CH} , V_{MBS}) generally do not achieve high DUR, despite having SAD similar to the size and neck parameters measuring length (H , L_{max} , H_{max} , D_{max} , H_b , $D_{neck,min}$, $D_{neck,max}$, P_{neck} , $D_{neck,equiv}$). The cause is the higher uncertainty encountered in determining the higher-dimensional parameters when compared to the one-dimensional parameters [14]. This suggests that higher-dimensional size parameters tend to be less robust and thus less suitable for use in practical risk models than one-dimensional size parameters. Like Lauric et al. [17], there are instances of noticeable differences in the discriminative performance of parameters capturing the same aspect of IA geometry, e.g., for the neck size parameters. The non-dimensional parameters exhibit comparatively high SAD and DUR, except for BL and UI, which exhibit lower discriminative ability and/or higher uncertainty in their calculation. The curvature parameters show substantial variability in SAD and DUR depending on the anatomical region and the parameter, with MLN performing comparatively well overall. It is notable that the posterior region tends to exhibit higher SAD and DUR than the other regions, indicating more pronounced geometric differences between ruptured and unruptured IAs in this region. Regarding the differences in SAD and DUR between datasets 1 and 2, it is likely that differences in the patient collectives, subsample sizes, and reconstruction techniques are the main causes. The latter could in the future be tackled by machine learning-based segmentation methods, which can reduce operator-induced uncertainty. Examples of such methods have previously been presented, e.g., in the context of the CADA challenge [29].

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3 Regarding the correlation patterns, there is substantial similarity between all analyzed anatomical regions
4 and datasets. Parameters tend to be most strongly correlated with other parameters from the same parameter
5 group, except for the non-dimensional and curvature parameters, which form two subgroups each. This is
6 reasonable, given that the parameters within each parameter group capture similar aspects of IA geometry.
7 For the size and neck parameter groups this is obvious, since they both capture aspects of IA and neck size,
8 respectively. The two distinct correlation subgroups within the non-dimensional parameter group are likely
9 caused by the underlying parameter subgroups capturing different aspects of aneurysm shape. While the
10 parameters of the first subgroup (AR, eAR, BF, BL) are simply ratios of one-dimensional size parameters,
11 the second subgroup (NSI, AVSV, AASA, UI, EI) is formed by parameters relating aneurysm area and/or
12 volume to geometric reference objects, e.g., the minimal bounding sphere or convex hull. The negative
13 correlation between AVSV and AASA with the other parameters from the second subgroup is due to the
14 parameter definitions, which cause AVSV and AASA to increase with increasing sphericity, while the other
15 parameters tend to decrease with increasing sphericity. The curvature parameters also form two subgroups,
16 with the first subgroup consisting of the dimensional parameters quantifying the mean or dispersion of IA
17 surface curvature (MAA, absMAA, MSD, GAA, absGAA, GSD) and the second subgroup consisting of
18 non-dimensional, scale invariant curvature parameters (HMC, MLN, HGC, GLN). Since the former
19 parameters intrinsically decrease with IA size, while the latter parameters increase with IA size, the negative
20 correlation of the two subgroups with each other makes sense. It should be noted that the positive correlation
21 of the non-dimensional curvature parameters with IA size is not an intrinsic property of the non-dimensional
22 parameters themselves, since they are designed to be scale invariant. It rather indicates that curvature and
23 irregularities of the IA surface increase in larger IAs.
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26 For a geometric risk parameter to be a good candidate for rupture risk prediction, it should generally have a
27 high SAD, in order to be able to differentiate between ruptured and unruptured IAs. Additionally, DUR
28 should be high, indicating low sensitivity of the parameter to the imaging, segmentation, and calculation
29 workflow, by which it is calculated. This is desirable because it allows models including such parameters
30 to generalize well to other datasets. Finally, when choosing a set of parameters, data from the correlation
31 analysis can be used to identify parameters that are not strongly correlated. Neyazi et al. have previously
32 used this method to derive a two-parameter rupture status prediction model from a set of 49 geometric and
33 hemodynamic rupture risk parameters, identifying AR and the maximal relative residence time as the most
34 suitable model parameters [13]. Other attempts to identify suitable rupture status prediction models based
35 on geometric risk parameters have been attempted, e.g., Dhar et al. [15] and Zhang et al. [30], but results
36 have generally been inconsistent. Possible reasons for the discrepant findings regarding optimal parameter
37 choice are the sample sizes used and the uncertainty inherent in the workflow by which the parameters are
38 calculated. This may lead to the selection of less robust parameters that perform well on a given dataset but
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3 generalize less well to others. Based on the results of this study and considering SAD, DUR, as well as the
4 correlation between geometric risk parameters, examples of more robust parameter choices could look as
5 follows:
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- 8 • H_{\max} , $D_{\text{neck},\min}$, AR, AASA, and MLN for the anterior region.
- 9 • L_{\max} , P_{neck} , AR, AASA, and HGC for the ICA.
- 10 • D_{\max} , $D_{\text{neck},\min}$, eAR, AASA, and HMC for the MCA.
- 11 • L_{\max} , $D_{\text{neck},\min}$, BL, EI, and absMAA for the posterior region.
- 12 • H_b , $D_{\text{neck},\min}$, AR, AASA, and MLN if looking at all anatomical regions combined.

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17 Overall, while individual size, neck, and curvature parameters achieved good discriminative performance
18 and robustness, the non-dimensional parameters tended to perform well as a group. This suggests that non-
19 dimensional geometric risk parameters can provide comparatively good discriminative performance, while
20 the nondimensionalization itself mitigates some of the uncertainty introduced through the workflow by
21 which the parameters are calculated [14]. Neither did we attempt to develop a novel aneurysm rupture risk
22 prediction model, nor did we test earlier published models [16, 31]. We decided against this analysis due to
23 the large variety of published proposed risk models. Testing them as well as the propagation of the
24 parameter's uncertainty towards assessment of rupture risk should be tested in a separate study. Finally,
25 elaborated models will also require further information such as hypertension status, earlier SAH as well as
26 hemodynamic parameters, which were unavailable within this study.
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34 Limitations

35 IAs were grouped by anatomical region because IA location is an important determinant of rupture risk, as
36 demonstrated by its weight in current risk scores [7-9]. However, by analyzing the datasets by anatomical
37 region, some subsamples become quite small. Small sample size might affect the accuracy of the median
38 and interquartile range estimates derived from these groups. This limitation is, however, partially mitigated
39 by also analyzing all anatomical regions combined and using two datasets, in order to get a more
40 comprehensive picture of the risk parameters' performance. The major focus of the study was the analysis
41 of the performance and robustness of 37 geometric risk parameters. Thus, not all findings of this study could
42 be assessed in depth. For example, we decided for grouping of aneurysms by anatomical regions as
43 recommended by clinical scores, such as such as PHASES score [7]. While we observed differences in both
44 SAD and DUR based on the aneurysms' location within the circulation, the underlying mechanisms for
45 these differences cannot be assessed by the available data. However, Tykocki & Kostkiewicz found
46 significant differences between some geometric parameters (parent artery size, size ratio and aspect ratio)
47 of aneurysms for the anterior and the posterior regions [32]. They associated the difference in these
48 parameters to different impacts on the intra-aneurysmal hemodynamics such as vortex formation and wall
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3 shear stress. Why these geometric parameters might result in different hemodynamic conditions and rupture
4 risks must be investigated in a dedicated study. This is especially important as this study's findings
5 demonstrated differences in the SAD not only between locations and the cohorts, but also when all aneurysm
6 locations were evaluated together.
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10 Furthermore, the underlying motivation for the chosen geometric parameters to be used for risk prediction.
11 All parameters were chosen as they were discussed in existing literature as potential risk parameters. The
12 investigated parameters as well as their respective references are summarized in the table 2. Respectively,
13 most of rupture risk models used in frames of the MATCH challenge [18] included both geometric and
14 hemodynamic parameters.
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18 Another potential limitation are the uncertainty values from Goubergrits et al. [14], which were used to
19 calculate DUR. These values were calculated on a sample containing MCA and posterior region IAs [14].
20 While it does not seem particularly probable, it is possible that IA location and size might affect the
21 uncertainty inherent in calculating the geometric risk parameters in a relevant manner, which in turn could
22 influence DUR results. Respectively the generalization of MRU values from the uncertainty study [14]
23 should be considered with caution, especially as those values were calculated only based on five aneurysms.
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25 A more fundamental limitations is the focus on geometric risk parameters. These parameters serve as proxies
26 for the pathophysiological processes leading to IA rupture through the latter's influence on the geometry of
27 the IA surface. Due to their nature, geometric risk parameters cannot directly capture the hemodynamic,
28 mechanical, or biochemical aspects of IA rupture. Nevertheless, they are among the most intensely
29 researched types of IA rupture risk parameters, due to the comparative ease with which they can be
30 calculated from clinical data.
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34 Note that the list of parameters investigated in this study is not exhaustive. More proposed geometric
35 parameters can be found in recent literature [33]. The parameters investigated here are limited to a set of
36 parameters investigated earlier in frames of the uncertainty study [14]. Second, these parameters were
37 constrained to parameters, which can be calculated automatically. Furthermore, we excluded parameters
38 such as Writhe-based indices or indices based on Zernike moments due to high sensitivity of these parameter
39 to the reconstruction process (e.g., surface smoothing algorithms). However, some of the novel parameters
40 (e.g. conicity index [33]) can be calculated based on parameters provided in this study.
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44 Finally, the calculation of geometric parameters including the ostium plane depends on a sufficient reference
45 plane selection. Recently, Berg et al. quantified the potential effect of neck curve variations on
46 hemodynamic predictions [34]. These findings could be transferred to the cases included in this study in
47 future work.
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Conclusion

Based on datasets from two research groups, the present study provides location-specific estimates of the discriminative ability of a large set of geometric risk parameters for IA rupture risk assessment, while also considering uncertainty. Additionally, correlation patterns between the parameters are identified. The presented data is potentially useful in evaluating geometric risk parameters for use in rupture risk models or when choosing input parameters for machine learning approaches to rupture risk prediction. It may also be helpful when designing future geometric risk parameters for clinical use.

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Conflict of interest statement

The authors declare that there is no conflict of interest.

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Data Availability Statement

All individual parameter values as well as the correlation coefficients are made available as supplemental material.

- supplemental material 1: individual parameter values, IA location, and rupture status for each IA
- supplemental material 2: exact values of the inter-parameter correlation coefficients

Ethical approval statements

In this study, patient-specific 3D reconstructions of intracranial aneurysms based on routine information were evaluated retrospectively. Use of retrospective data was approved by the local ethics committees (Ethikkommission der Charité - Universitätsmedizin Berlin: EA2/222/19; Ethikkommission der Med. Hochschule Hannover: NOVA Nr. 68/20).

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Author contributions

All roles according to CRediT (contributor roles taxonomy). Conceptualization: LG, JS, FH, JB, and PB. Methodology: FH, JS, and LG. Resources: AS, IES, OB, NL, SS, and PB. Investigation: JB, FH, and JS. Formal Analysis: FH. Funding acquisition: LG, PB, and SS. Supervision: LG. Writing – original draft: FH, LG, and JB. Writing – review & editing: PB, SS, AS, IES, OB, NL, and JS.

References

1. Vlak, M.H., A. Algra, R. Brandenburg, and G.J. Rinkel, *Prevalence of unruptured intracranial aneurysms, with emphasis on sex, age, comorbidity, country, and time period: a systematic review and meta-analysis*. *Lancet Neurol*, 2011. **10**(7): p. 626-36.
2. Brown, R.D., Jr. and J.P. Broderick, *Unruptured intracranial aneurysms: epidemiology, natural history, management options, and familial screening*. *Lancet Neurol*, 2014. **13**(4): p. 393-404.
3. Wiebers, D.O., J.P. Whisnant, J. Huston, 3rd, I. Meissner, R.D. Brown, Jr., D.G. Piepgras, G.S. Forbes, K. Thielen, D. Nichols, W.M. O'Fallon, J. Peacock, L. Jaeger, N.F. Kassell, G.L. Kongable-Beckman, J.C. Torner, and I. International Study of Unruptured Intracranial Aneurysms, *Unruptured intracranial aneurysms: natural history, clinical outcome, and risks of surgical and endovascular treatment*. *Lancet*, 2003. **362**(9378): p. 103-10.
4. Rackauskaite, D., E. Svanborg, E. Andersson, K. Lowhagen, L. Csajbok, and B. Nellgard, *Prospective study: Long-term outcome at 12-15 years after aneurysmal subarachnoid hemorrhage*. *Acta Neurol Scand*, 2018. **138**(5): p. 400-407.
5. Pontes, F.G.B., E.M. da Silva, J.C. Baptista-Silva, and V. Vasconcelos, *Treatments for unruptured intracranial aneurysms*. *Cochrane Database Syst Rev*, 2021. **5**: p. CD013312.
6. Thompson, B.G., et al., *Guidelines for the Management of Patients With Unruptured Intracranial Aneurysms: A Guideline for Healthcare Professionals From the American Heart Association/American Stroke Association*. *Stroke*, 2015. **46**(8): p. 2368-400.
7. Greving, J.P., M.J. Wermer, R.D. Brown, Jr., A. Morita, S. Juvela, M. Yonekura, T. Ishibashi, J.C. Torner, T. Nakayama, G.J. Rinkel, and A. Algra, *Development of the PHASES score for prediction of risk of rupture of intracranial aneurysms: a pooled analysis of six prospective cohort studies*. *Lancet Neurol*, 2014. **13**(1): p. 59-66.
8. Etminan, N., et al., *The unruptured intracranial aneurysm treatment score: a multidisciplinary consensus*. *Neurology*, 2015. **85**(10): p. 881-9.
9. Backes, D., et al., *ELAPSS score for prediction of risk of growth of unruptured intracranial aneurysms*. *Neurology*, 2017. **88**(17): p. 1600-1606.
10. Juvela, S., *PHASES score and treatment scoring with cigarette smoking in the long-term prediction of rupturing of unruptured intracranial aneurysms*. *J Neurosurg*, 2022. **136**(1): p. 156-162.
11. Molenberg, R., M.W. Aalbers, A. Mazuri, G.J. Luijckx, J.D.M. Metzemaekers, R.J.M. Groen, M. Uyttenboogaart, and J.M.C. van Dijk, *The Unruptured Intracranial Aneurysm Treatment Score as a predictor of aneurysm growth or rupture*. *Eur J Neurol*, 2021. **28**(3): p. 837-843.
12. Hernandez-Duran, S., D. Mielke, V. Rohde, and V. Malinova, *Is the unruptured intracranial aneurysm treatment score (UIATS) sensitive enough to detect aneurysms at risk of rupture?* *Neurosurg Rev*, 2021. **44**(2): p. 987-993.
13. Neyazi, B., V.M. Swiatek, M. Skalej, O. Beuing, K.P. Stein, J. Hattingen, B. Preim, P. Berg, S. Saalfeld, and I.E. Sandalcioglu, *Rupture risk assessment for multiple intracranial aneurysms: why there is no need for dozens of clinical, morphological and hemodynamic parameters*. *Ther Adv Neurol Disord*, 2020. **13**: p. 1756286420966159.
14. Goubergrits, L., F. Hellmeier, J. Bruening, A. Spuler, H.C. Hege, S. Voss, G. Janiga, S. Saalfeld, O. Beuing, and P. Berg, *Multiple Aneurysms AnaTomy CHallenge 2018 (MATCH): uncertainty quantification of geometric rupture risk parameters*. *Biomed Eng Online*, 2019. **18**(1): p. 35.
15. Dhar, S., M. Tremmel, J. Mocco, M. Kim, J. Yamamoto, A.H. Siddiqui, L.N. Hopkins, and H. Meng, *Morphology parameters for intracranial aneurysm rupture risk assessment*. *Neurosurgery*, 2008. **63**(2): p. 185-96; discussion 196-7.
16. Detmer, F.J., B.J. Chung, F. Mut, M. Slawski, F. Hamzei-Sichani, C. Putman, C. Jimenez, and J.R. Czebral, *Development and internal validation of an aneurysm rupture probability model based on patient characteristics and aneurysm location, morphology, and hemodynamics*. *Int J Comput Assist Radiol Surg*, 2018. **13**(11): p. 1767-1779.

17. Lauric, A., M.I. Baharoglu, and A.M. Malek, *Ruptured status discrimination performance of aspect ratio, height/width, and bottleneck factor is highly dependent on aneurysm sizing methodology*. Neurosurgery, 2012. **71**(1): p. 38-45.
18. Berg, P., et al., *Multiple Aneurysms AnaTomy CHallenge 2018 (MATCH): Phase I: Segmentation*. Cardiovasc Eng Technol, 2018. **9**(4): p. 565-581.
19. Ma, B., R.E. Harbaugh, and M.L. Raghavan, *Three-dimensional geometrical characterization of cerebral aneurysms*. Ann Biomed Eng, 2004. **32**(2): p. 264-73.
20. Lauric, A., E.L. Miller, M.I. Baharoglu, and A.M. Malek, *3D shape analysis of intracranial aneurysms using the writhe number as a discriminant for rupture*. Ann Biomed Eng, 2011. **39**(5): p. 1457-69.
21. Chien, A., J. Sayre, and F. Vinuela, *Comparative morphological analysis of the geometry of ruptured and unruptured aneurysms*. Neurosurgery, 2011. **69**(2): p. 349-56.
22. Ujiie, H., Y. Tamano, K. Sasaki, and T. Hori, *Is the aspect ratio a reliable index for predicting the rupture of a saccular aneurysm?* Neurosurgery, 2001. **48**(3): p. 495-502; discussion 502-3.
23. Ramachandran, M., R. Retarekar, R.E. Harbaugh, D. Hasan, B. Policeni, R. Rosenwasser, C. Ogilvy, and M.L. Raghavan, *Sensitivity of Quantified Intracranial Aneurysm Geometry to Imaging Modality*. Cardiovasc Eng Technol, 2013. **4**(1): p. 75-86.
24. O'Meara, B., J.P. Rahal, A. Lauric, and A.M. Malek, *Benefit of a sharp computed tomography angiography reconstruction kernel for improved characterization of intracranial aneurysms*. Neurosurgery, 2014. **10 Suppl 1**: p. 97-105; discussion 105.
25. Berg, P., S. Saalfeld, S. Voss, T. Redel, B. Preim, G. Janiga, and O. Beuing, *Does the DSA reconstruction kernel affect hemodynamic predictions in intracranial aneurysms? An analysis of geometry and blood flow variations*. J Neurointerv Surg, 2018. **10**(3): p. 290-296.
26. Cebal, J.R., M.A. Castro, S. Appanaboyina, C.M. Putman, D. Millan, and A.F. Frangi, *Efficient pipeline for image-based patient-specific analysis of cerebral aneurysm hemodynamics: technique and sensitivity*. IEEE Trans Med Imaging, 2005. **24**(4): p. 457-67.
27. Sarrami-Foroushani, A., T. Lassila, and A.F. Frangi, *Virtual endovascular treatment of intracranial aneurysms: models and uncertainty*. Wiley Interdiscip Rev Syst Biol Med, 2017. **9**(4).
28. Schneiders, J.J., H.A. Marquering, L. Antiga, R. van den Berg, E. VanBavel, and C.B. Majoie, *Intracranial aneurysm neck size overestimation with 3D rotational angiography: the impact on intra-aneurysmal hemodynamics simulated with computational fluid dynamics*. AJNR Am J Neuroradiol, 2013. **34**(1): p. 121-8.
29. Ivantsits, M., et al., *Detection and analysis of cerebral aneurysms based on X-ray rotational angiography - the CADA 2020 challenge*. Med Image Anal, 2021. **77**: p. 102333.
30. Zheng, Y., F. Xu, J. Ren, Q. Xu, Y. Liu, Y. Tian, and B. Leng, *Assessment of intracranial aneurysm rupture based on morphology parameters and anatomical locations*. J Neurointerv Surg, 2016. **8**(12): p. 1240-1246.
31. Lall, R.R., C.S. Eddleman, B.R. Bendok, and H.H. Batjer, *Unruptured intracranial aneurysms and the assessment of rupture risk based on anatomical and morphological factors: sifting through the sands of data*. Neurosurg Focus, 2009. **26**(5): p. E2.
32. Tykocki, T. and B. Kostkiewicz, *Aneurysms of the anterior and posterior cerebral circulation: comparison of the morphometric features*. Acta Neurochir (Wien), 2014. **156**(9): p. 1647-54.
33. Juchler, N., S. Schilling, P. Bijlenga, V. Kurtcuoglu, and S. Hirsch, *Shape Trumps Size: Image-Based Morphological Analysis Reveals That the 3D Shape Discriminates Intracranial Aneurysm Disease Status Better Than Aneurysm Size*. Front Neurol, 2022. **13**: p. 809391.
34. Berg, P., B. Behrendt, S. Voss, O. Beuing, B. Neyazi, I.E. Sandalcioglu, B. Preim, and S. Saalfeld, *VICTORIA: Virtual neck Curve and True Ostium Reconstruction of Intracranial Aneurysms*. Cardiovasc Eng Technol, 2021. **12**(4): p. 454-465.

Figures

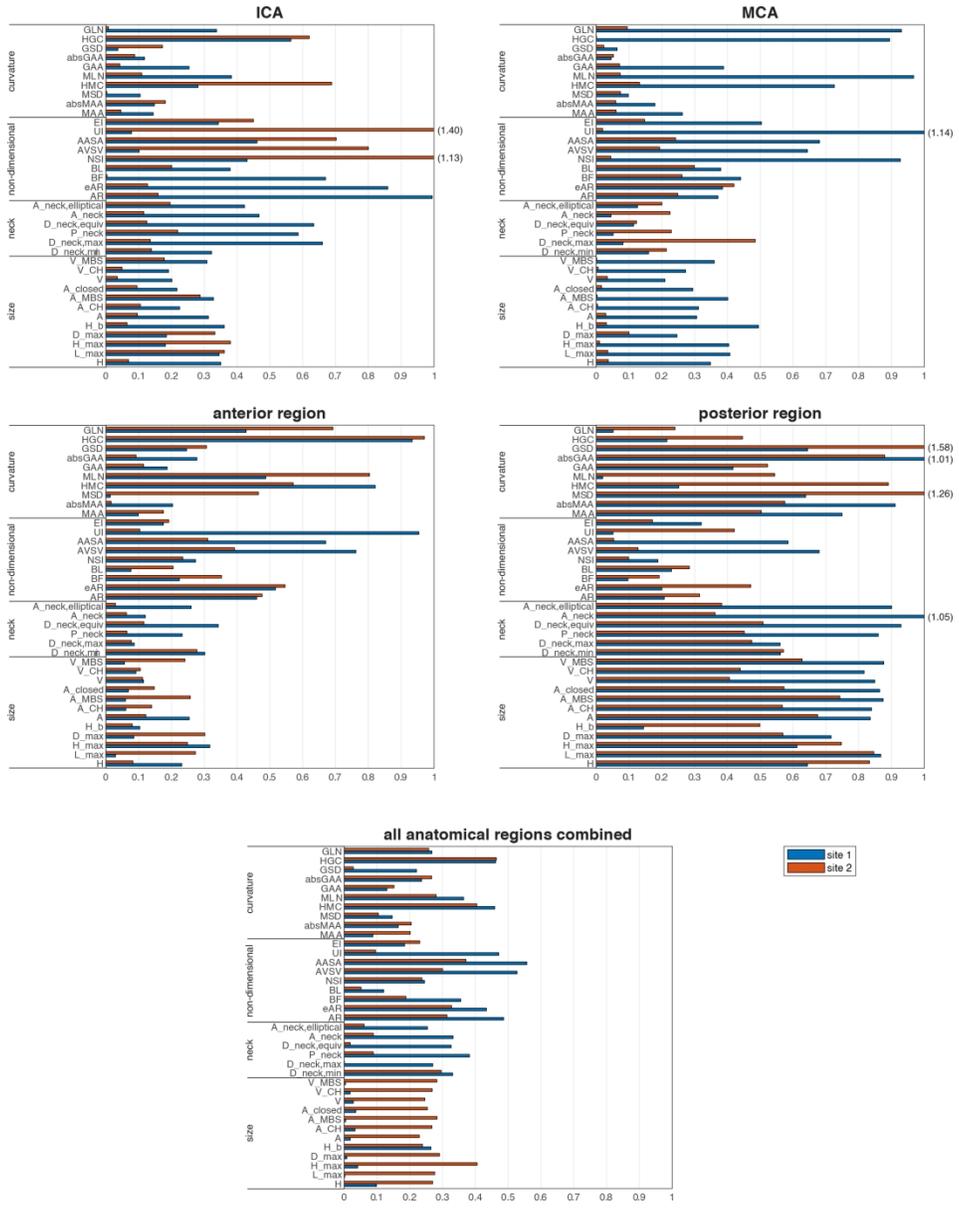
Figure 1: Standardized absolute group difference (SAD) for each anatomical region and dataset.

Figure 2: Group difference-uncertainty ratio (DUR) for each anatomical region and dataset.

Figure 3: Pearson's r for correlation between geometric risk parameters by anatomical region for dataset 1.

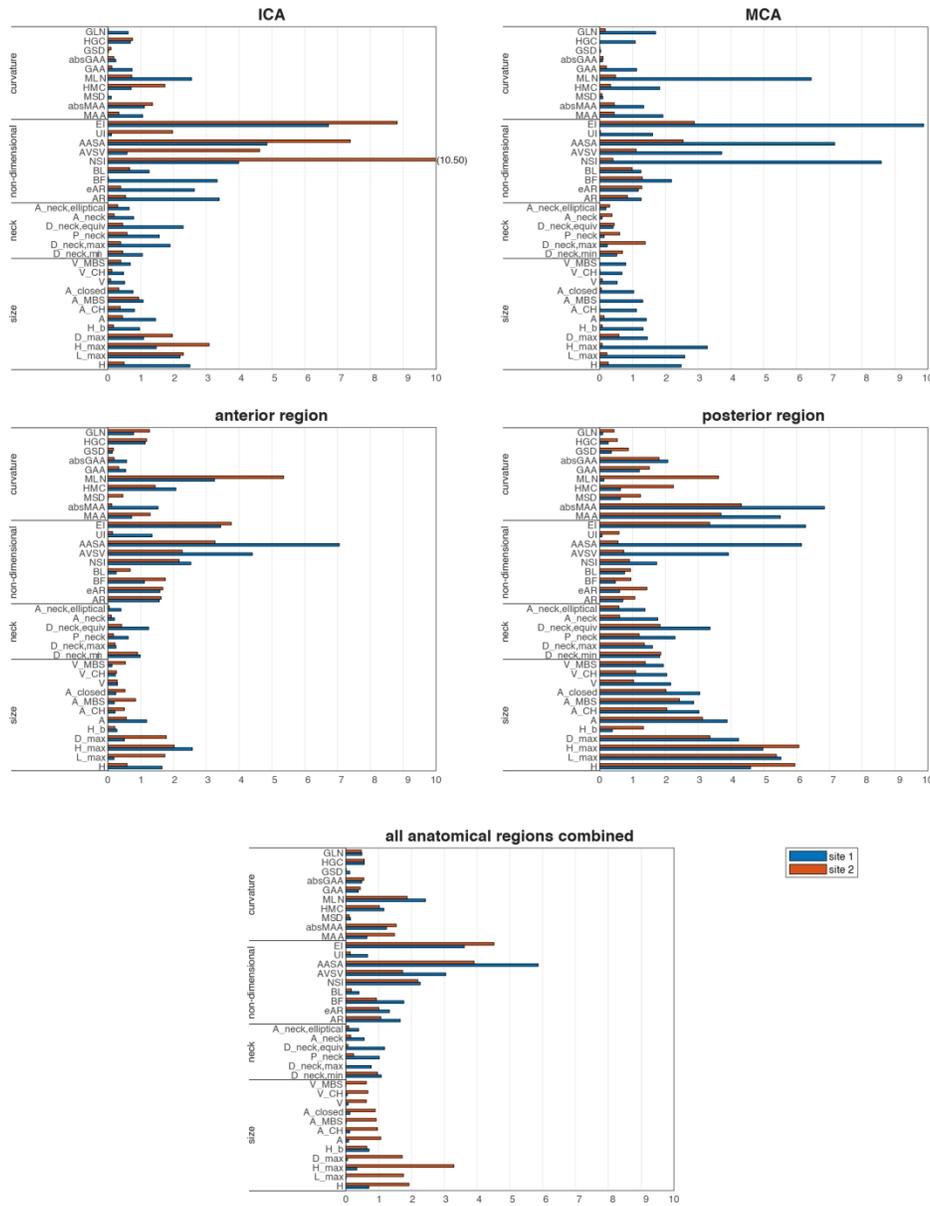
Figure 4: Pearson's r for correlation between geometric risk parameters by anatomical region for dataset 2.

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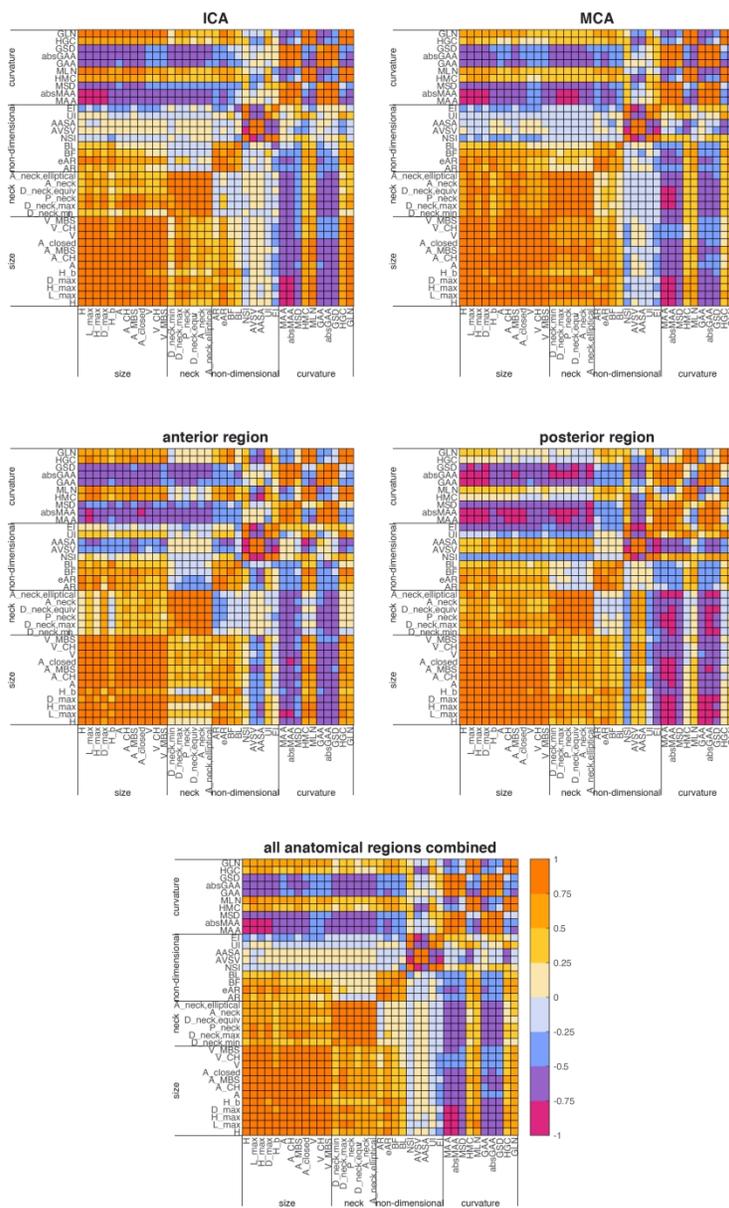


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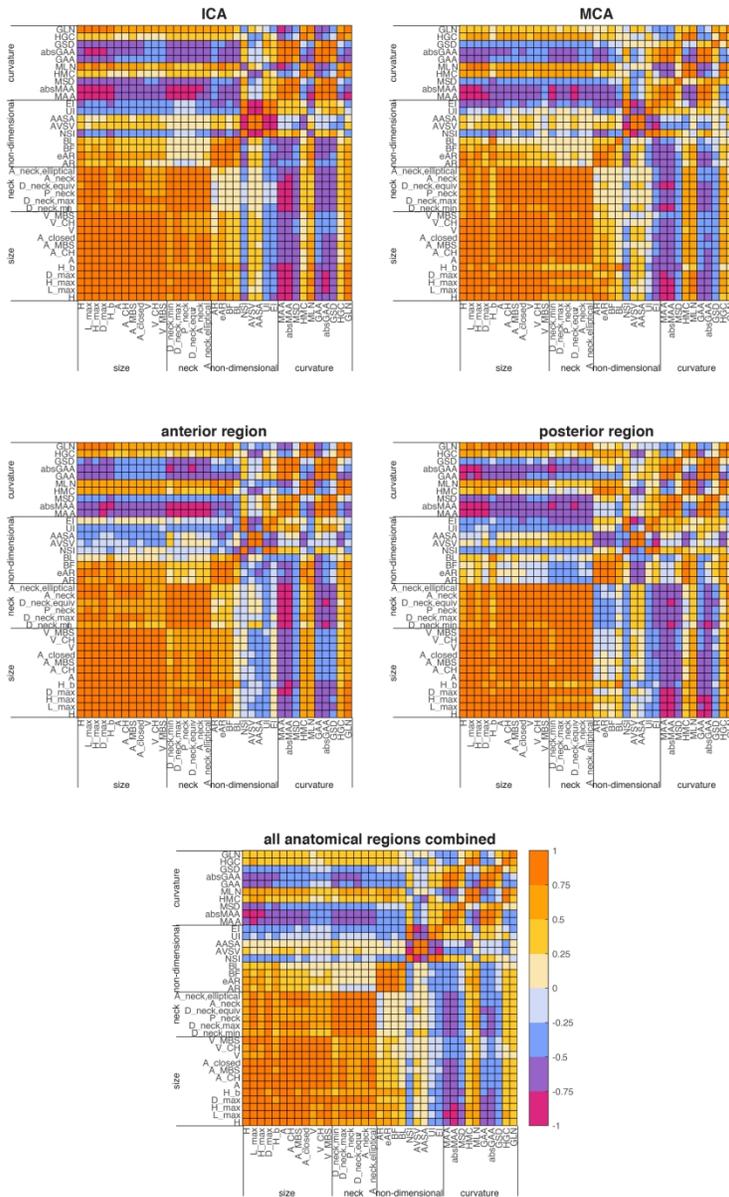
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	Pearson's r	H	L_max	H_max	D_max	H_b	A	A_CH
3	H	1.000	0.872	0.968	0.610	0.836	0.867	0.830
4	L_max	0.872	1.000	0.950	0.884	0.648	0.962	0.960
5	H_max	0.968	0.950	1.000	0.728	0.783	0.922	0.894
6	D_max	0.610	0.884	0.728	1.000	0.349	0.873	0.900
7	H_b	0.836	0.648	0.783	0.349	1.000	0.653	0.605
8	A	0.867	0.962	0.922	0.873	0.653	1.000	0.993
9	A_CH	0.830	0.960	0.894	0.900	0.605	0.993	1.000
10	A_MBS	0.835	0.973	0.919	0.863	0.596	0.967	0.957
11	A_closed	0.827	0.957	0.890	0.899	0.606	0.992	1.000
12	V	0.779	0.917	0.842	0.869	0.565	0.980	0.988
13	V_CH	0.778	0.924	0.846	0.880	0.548	0.982	0.988
14	V_MBS	0.769	0.918	0.857	0.822	0.522	0.934	0.919
15	D_neck,mir	0.220	0.402	0.246	0.535	0.125	0.415	0.484
16	D_neck,ma	0.153	0.466	0.248	0.642	-0.049	0.426	0.520
17	P_neck	0.059	0.376	0.158	0.554	-0.075	0.353	0.454
18	D_neck,eqt	0.159	0.428	0.224	0.609	-0.014	0.417	0.508
19	A_neck	0.089	0.392	0.170	0.583	-0.064	0.390	0.491
20	A_neck,elli	0.179	0.448	0.240	0.630	0.028	0.450	0.541
21	AR	0.867	0.582	0.784	0.236	0.849	0.579	0.503
22	eAR	0.879	0.639	0.819	0.304	0.801	0.608	0.536
23	BF	0.701	0.727	0.749	0.684	0.595	0.735	0.682
24	BL	0.627	0.461	0.580	0.273	0.884	0.464	0.423
25	NSI	0.173	0.275	0.235	0.216	-0.021	0.142	0.129
26	AVSV	-0.393	-0.491	-0.481	-0.331	-0.275	-0.315	-0.287
27	AASA	-0.455	-0.558	-0.551	-0.378	-0.337	-0.380	-0.350
28	UI	0.405	0.494	0.463	0.437	0.137	0.365	0.356
29	EI	0.012	0.091	0.067	0.013	-0.075	-0.034	-0.050
30	MAA	-0.661	-0.763	-0.698	-0.727	-0.481	-0.702	-0.740
31	absMAA	-0.692	-0.755	-0.711	-0.701	-0.547	-0.710	-0.747
32	MSD	-0.504	-0.453	-0.465	-0.370	-0.517	-0.489	-0.513
33	HMC	0.672	0.801	0.776	0.698	0.434	0.706	0.672
34	MLN	0.727	0.775	0.790	0.706	0.500	0.745	0.704
35	GAA	-0.627	-0.693	-0.655	-0.632	-0.443	-0.590	-0.621
36	absGAA	-0.647	-0.688	-0.659	-0.626	-0.534	-0.639	-0.672
37	GSD	-0.547	-0.567	-0.541	-0.507	-0.511	-0.550	-0.584
38	HGC	0.618	0.783	0.727	0.735	0.322	0.710	0.685
39	GLN	0.614	0.729	0.698	0.731	0.300	0.711	0.681

	A_MBS	A_closed	V	V_CH	V_MBS	D_neck,min	D_neck,max	P_neck
1								
2								
3	0.835	0.827	0.779	0.778	0.769	0.220	0.153	0.059
4	0.973	0.957	0.917	0.924	0.918	0.402	0.466	0.376
5	0.919	0.890	0.842	0.846	0.857	0.246	0.248	0.158
6	0.863	0.899	0.869	0.880	0.822	0.535	0.642	0.554
7	0.596	0.606	0.565	0.548	0.522	0.125	-0.049	-0.075
8	0.967	0.992	0.980	0.982	0.934	0.415	0.426	0.353
9	0.957	1.000	0.988	0.988	0.919	0.484	0.520	0.454
10	1.000	0.952	0.939	0.953	0.984	0.346	0.375	0.290
11	0.952	1.000	0.989	0.988	0.913	0.494	0.526	0.462
12	0.939	0.989	1.000	0.998	0.920	0.486	0.503	0.457
13	0.953	0.988	0.998	1.000	0.940	0.460	0.485	0.430
14	0.984	0.913	0.920	0.940	1.000	0.298	0.302	0.223
15	0.346	0.494	0.486	0.460	0.298	1.000	0.685	0.681
16	0.375	0.526	0.503	0.485	0.302	0.685	1.000	0.952
17	0.290	0.462	0.457	0.430	0.223	0.681	0.952	1.000
18	0.361	0.516	0.504	0.485	0.310	0.907	0.870	0.857
19	0.321	0.500	0.503	0.477	0.263	0.780	0.944	0.974
20	0.377	0.550	0.543	0.517	0.316	0.909	0.909	0.886
21	0.568	0.498	0.454	0.459	0.527	-0.127	-0.328	-0.375
22	0.610	0.529	0.473	0.480	0.553	-0.208	-0.214	-0.304
23	0.753	0.675	0.643	0.668	0.743	0.043	-0.096	-0.153
24	0.362	0.427	0.370	0.348	0.268	0.087	-0.061	-0.064
25	0.334	0.113	0.080	0.131	0.361	-0.197	-0.061	-0.176
26	-0.501	-0.273	-0.225	-0.261	-0.486	0.179	0.068	0.160
27	-0.558	-0.337	-0.288	-0.320	-0.535	0.160	0.041	0.130
28	0.494	0.340	0.273	0.321	0.477	-0.152	0.134	-0.008
29	0.166	-0.065	-0.072	-0.032	0.209	-0.227	-0.193	-0.269
30	-0.636	-0.743	-0.667	-0.654	-0.529	-0.582	-0.679	-0.648
31	-0.627	-0.752	-0.683	-0.661	-0.516	-0.646	-0.664	-0.637
32	-0.379	-0.521	-0.510	-0.474	-0.310	-0.620	-0.396	-0.402
33	0.801	0.661	0.604	0.639	0.770	-0.028	0.133	-0.011
34	0.753	0.697	0.631	0.658	0.708	-0.009	0.127	-0.014
35	-0.547	-0.622	-0.527	-0.520	-0.433	-0.446	-0.584	-0.543
36	-0.551	-0.678	-0.607	-0.582	-0.440	-0.652	-0.603	-0.580
37	-0.453	-0.592	-0.545	-0.515	-0.360	-0.695	-0.549	-0.547
38	0.811	0.672	0.627	0.670	0.805	-0.029	0.180	0.038
39	0.748	0.672	0.626	0.664	0.737	-0.038	0.158	0.024
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3	0.159	0.089	0.179	0.867	0.879	0.701	0.627	0.173
4	0.428	0.392	0.448	0.582	0.639	0.727	0.461	0.275
5	0.224	0.170	0.240	0.784	0.819	0.749	0.580	0.235
6	0.609	0.583	0.630	0.236	0.304	0.684	0.273	0.216
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8	-0.014	-0.064	0.028	0.849	0.801	0.595	0.884	-0.021
9	0.417	0.390	0.450	0.579	0.608	0.735	0.464	0.142
10	0.508	0.491	0.541	0.503	0.536	0.682	0.423	0.129
11	0.361	0.321	0.377	0.568	0.610	0.753	0.362	0.334
12	0.516	0.500	0.550	0.498	0.529	0.675	0.427	0.113
13	0.504	0.503	0.543	0.454	0.473	0.643	0.370	0.080
14	0.485	0.477	0.517	0.459	0.480	0.668	0.348	0.131
15	0.310	0.263	0.316	0.527	0.553	0.743	0.268	0.361
16	0.907	0.780	0.909	-0.127	-0.208	0.043	0.087	-0.197
17	0.870	0.944	0.909	-0.328	-0.214	-0.096	-0.061	-0.061
18	0.857	0.974	0.886	-0.375	-0.304	-0.153	-0.064	-0.176
19	1.000	0.927	0.953	-0.267	-0.298	-0.034	-0.040	-0.113
20	0.927	1.000	0.949	-0.353	-0.317	-0.119	-0.074	-0.157
21	0.953	0.949	1.000	-0.266	-0.247	-0.036	0.004	-0.155
22	-0.267	-0.353	-0.266	1.000	0.946	0.687	0.672	0.175
23	-0.298	-0.317	-0.247	0.946	1.000	0.669	0.627	0.253
24	-0.034	-0.119	-0.036	0.687	0.669	1.000	0.525	0.300
25	-0.040	-0.074	0.004	0.672	0.627	0.525	1.000	-0.267
26	-0.113	-0.157	-0.155	0.175	0.253	0.300	-0.267	1.000
27	0.141	0.175	0.161	-0.403	-0.468	-0.491	-0.075	-0.823
28	0.129	0.153	0.138	-0.450	-0.524	-0.532	-0.148	-0.751
29	0.019	-0.021	-0.047	0.320	0.427	0.442	-0.027	0.824
30	-0.219	-0.243	-0.226	0.085	0.141	0.157	-0.325	0.922
31	-0.656	-0.622	-0.632	-0.337	-0.379	-0.384	-0.446	0.044
32	-0.678	-0.632	-0.667	-0.377	-0.393	-0.371	-0.492	0.103
33	-0.516	-0.461	-0.553	-0.319	-0.252	-0.158	-0.456	0.370
34	0.017	-0.024	0.030	0.536	0.649	0.764	0.318	0.542
35	0.022	-0.028	0.035	0.591	0.685	0.804	0.463	0.314
36	-0.543	-0.499	-0.495	-0.365	-0.417	-0.365	-0.436	-0.045
37	-0.634	-0.575	-0.635	-0.368	-0.375	-0.327	-0.513	0.183
38	-0.631	-0.563	-0.640	-0.296	-0.265	-0.203	-0.488	0.303
39	0.077	0.033	0.055	0.449	0.560	0.753	0.186	0.602
40	0.064	0.022	0.042	0.453	0.551	0.779	0.234	0.427
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	AVSV	AASA	UI	EI	MAA	absMAA	MSD	HMC
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3	-0.393	-0.455	0.405	0.012	-0.661	-0.692	-0.504	0.672
4	-0.491	-0.558	0.494	0.091	-0.763	-0.755	-0.453	0.801
5	-0.481	-0.551	0.463	0.067	-0.698	-0.711	-0.465	0.776
6	-0.331	-0.378	0.437	0.013	-0.727	-0.701	-0.370	0.698
7	-0.275	-0.337	0.137	-0.075	-0.481	-0.547	-0.517	0.434
8	-0.315	-0.380	0.365	-0.034	-0.702	-0.710	-0.489	0.706
9	-0.287	-0.350	0.356	-0.050	-0.740	-0.747	-0.513	0.672
10	-0.501	-0.558	0.494	0.166	-0.636	-0.627	-0.379	0.801
11	-0.273	-0.337	0.340	-0.065	-0.743	-0.752	-0.521	0.661
12	-0.225	-0.288	0.273	-0.072	-0.667	-0.683	-0.510	0.604
13	-0.261	-0.320	0.321	-0.032	-0.654	-0.661	-0.474	0.639
14	-0.486	-0.535	0.477	0.209	-0.529	-0.516	-0.310	0.770
15	0.179	0.160	-0.152	-0.227	-0.582	-0.646	-0.620	-0.028
16	0.068	0.041	0.134	-0.193	-0.679	-0.664	-0.396	0.133
17	0.160	0.130	-0.008	-0.269	-0.648	-0.637	-0.402	-0.011
18	0.141	0.129	0.019	-0.219	-0.656	-0.678	-0.516	0.017
19	0.175	0.153	-0.021	-0.243	-0.622	-0.632	-0.461	-0.024
20	0.161	0.138	-0.047	-0.226	-0.632	-0.667	-0.553	0.030
21	-0.403	-0.450	0.320	0.085	-0.337	-0.377	-0.319	0.536
22	-0.468	-0.524	0.427	0.141	-0.379	-0.393	-0.252	0.649
23	-0.491	-0.532	0.442	0.157	-0.384	-0.371	-0.158	0.764
24	-0.075	-0.148	-0.027	-0.325	-0.446	-0.492	-0.456	0.318
25	-0.823	-0.751	0.824	0.922	0.044	0.103	0.370	0.542
26	1.000	0.988	-0.699	-0.776	0.120	0.070	-0.205	-0.736
27	0.988	1.000	-0.667	-0.702	0.177	0.129	-0.138	-0.785
28	-0.699	-0.667	1.000	0.556	-0.297	-0.203	0.211	0.706
29	-0.776	-0.702	0.556	1.000	0.257	0.273	0.377	0.341
30	0.120	0.177	-0.297	0.257	1.000	0.974	0.558	-0.424
31	0.070	0.129	-0.203	0.273	0.974	1.000	0.709	-0.339
32	-0.205	-0.138	0.211	0.377	0.558	0.709	1.000	0.032
33	-0.736	-0.785	0.706	0.341	-0.424	-0.339	0.032	1.000
34	-0.488	-0.536	0.586	0.075	-0.511	-0.427	0.009	0.912
35	0.207	0.254	-0.399	0.184	0.968	0.923	0.460	-0.446
36	0.021	0.088	-0.094	0.314	0.933	0.973	0.764	-0.290
37	-0.118	-0.050	0.060	0.393	0.798	0.880	0.904	-0.119
38	-0.689	-0.718	0.778	0.366	-0.422	-0.320	0.097	0.961
39	-0.487	-0.516	0.661	0.173	-0.452	-0.345	0.122	0.881
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	MLN	GAA	absGAA	GSD	HGC	GLN
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3	0.727	-0.627	-0.647	-0.547	0.618	0.614
4	0.775	-0.693	-0.688	-0.567	0.783	0.729
5	0.790	-0.655	-0.659	-0.541	0.727	0.698
6	0.706	-0.632	-0.626	-0.507	0.735	0.731
7	0.500	-0.443	-0.534	-0.511	0.322	0.300
8	0.745	-0.590	-0.639	-0.550	0.710	0.711
9	0.704	-0.621	-0.672	-0.584	0.685	0.681
10	0.753	-0.547	-0.551	-0.453	0.811	0.748
11	0.697	-0.622	-0.678	-0.592	0.672	0.672
12	0.631	-0.527	-0.607	-0.545	0.627	0.626
13	0.658	-0.520	-0.582	-0.515	0.670	0.664
14	0.708	-0.433	-0.440	-0.360	0.805	0.737
15	-0.009	-0.446	-0.652	-0.695	-0.029	-0.038
16	0.127	-0.584	-0.603	-0.549	0.180	0.158
17	-0.014	-0.543	-0.580	-0.547	0.038	0.024
18	0.022	-0.543	-0.634	-0.631	0.077	0.064
19	-0.028	-0.499	-0.575	-0.563	0.033	0.022
20	0.035	-0.495	-0.635	-0.640	0.055	0.042
21	0.591	-0.365	-0.368	-0.296	0.449	0.453
22	0.685	-0.417	-0.375	-0.265	0.560	0.551
23	0.804	-0.365	-0.327	-0.203	0.753	0.779
24	0.463	-0.436	-0.513	-0.488	0.186	0.234
25	0.314	-0.045	0.183	0.303	0.602	0.427
26	-0.488	0.207	0.021	-0.118	-0.689	-0.487
27	-0.536	0.254	0.088	-0.050	-0.718	-0.516
28	0.586	-0.399	-0.094	0.060	0.778	0.661
29	0.075	0.184	0.314	0.393	0.366	0.173
30	-0.511	0.968	0.933	0.798	-0.422	-0.452
31	-0.427	0.923	0.973	0.880	-0.320	-0.345
32	0.009	0.460	0.764	0.904	0.097	0.122
33	0.912	-0.446	-0.290	-0.119	0.961	0.881
34	1.000	-0.519	-0.372	-0.166	0.886	0.941
35	-0.519	1.000	0.888	0.724	-0.438	-0.459
36	-0.372	0.888	1.000	0.937	-0.231	-0.256
37	-0.166	0.724	0.937	1.000	-0.051	-0.034
38	0.886	-0.438	-0.231	-0.051	1.000	0.939
39	0.941	-0.459	-0.256	-0.034	0.939	1.000
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abbreviation	-	-	-	-	-	-	H
unit	-	-	-	-	-	1=ruptured	mm
1	1	Berlin	Berlin	AComA	anterior	1	5.748
2	2	Berlin	Berlin	PComA	posterior	0	8.261
3	3	Berlin	Berlin	PICA	posterior	1	6.023
4	4	Berlin	Berlin	AComA	anterior	1	5.698
5	5	Berlin	Berlin	ACA	anterior	0	5.667
6	6	Berlin	Berlin	MCA	MCA	0	2.849
7	7	Berlin	Berlin	ICA	ICA	0	19.575
8	8	Berlin	Berlin	MCA	MCA	0	4.199
9	9	Berlin	Berlin	MCA	MCA	0	3.795
10	10	Berlin	Berlin	AComA	anterior	1	5.051
11	11	Berlin	Berlin	MCA	MCA	0	6.789
12	12	Berlin	Berlin	ICA	ICA	1	7.610
13	13	Berlin	Berlin	MCA	MCA	0	8.157
14	14	Berlin	Berlin	AComA	anterior	1	2.542
15	15	Berlin	Berlin	PComA	posterior	1	3.196
16	16A	Berlin	Berlin	ICA	ICA	1	9.587
17	16B	Berlin	Berlin	ACA	anterior	0	1.879
18	17A	Berlin	Berlin	ICA	ICA	0	12.261
19	17B	Berlin	Berlin	ICA	ICA	0	2.791
20	17C	Berlin	Berlin	AComA	anterior	0	4.530
21	18	Berlin	Berlin	MCA	MCA	1	5.597
22	19	Berlin	Berlin	AComA	anterior	1	5.177
23	20	Berlin	Berlin	PComA	posterior	1	10.569
24	21	Berlin	Berlin	ICA	ICA	0	4.966
25	22	Berlin	Berlin	ICA	ICA	0	7.908
26	23	Berlin	Berlin	MCA	MCA	1	4.598
27	24	Berlin	Berlin	ICA	ICA	0	2.906
28	25	Berlin	Berlin	BA	posterior	0	8.473
29	26	Berlin	Berlin	MCA	MCA	1	4.210
30	27	Berlin	Berlin	AComA	anterior	1	4.597
31	28	Berlin	Berlin	MCA	MCA	1	5.480
32	29	Berlin	Berlin	ICA	ICA	0	12.780
33	30A	Berlin	Berlin	ICA	ICA	0	4.078
34	30B	Berlin	Berlin	AComA	anterior	0	3.135
35	30C	Berlin	Berlin	AComA	anterior	1	5.085
36	30D	Berlin	Berlin	MCA	MCA	0	2.715
37	30E	Berlin	Berlin	PICA	posterior	1	4.983
38	31	Berlin	Berlin	MCA	MCA	0	4.542
39	32	Berlin	Berlin	ICA	ICA	0	9.475
40	33	Berlin	Berlin	AComA	anterior	1	6.212
41	34	Berlin	Berlin	AComA	anterior	0	3.383
42	35	Berlin	Berlin	ICA	ICA	1	11.690
43	36	Berlin	Berlin	BA	posterior	0	20.748
44	37	Berlin	Berlin	AComA	anterior	1	5.543
45	38	Berlin	Berlin	AComA	anterior	0	8.400
46	39	Berlin	Berlin	ICA	ICA	1	4.290
47	40	Berlin	Berlin	PComA	posterior	1	13.786

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2	41	Berlin	Berlin	ACoMA	anterior	1	4.301
3	42	Berlin	Berlin	PCoMA	posterior	0	5.891
4	43	Berlin	Berlin	ICA	ICA	0	6.872
5	44	Berlin	Berlin	PICA	posterior	1	4.213
6	45A	Berlin	Berlin	ICA	ICA	0	2.414
7	45B	Berlin	Berlin	ICA	ICA	1	3.501
8	45C	Berlin	Berlin	ICA	ICA	0	2.297
9	46	Berlin	Berlin	BA	posterior	0	11.175
10	47	Berlin	Berlin	ICA	ICA	0	4.636
11	48	Berlin	Berlin	MCA	MCA	0	2.204
12	49	Berlin	Berlin	MCA	MCA	1	16.986
13	50	Berlin	Berlin	PCoMA	posterior	1	7.588
14	51	Berlin	Berlin	ACoMA	anterior	0	5.047
15	52	Berlin	Berlin	ACA	anterior	1	2.779
16	53	Berlin	Berlin	AChA	ICA	1	6.830
17	54	Berlin	Berlin	PCoMA	posterior	1	4.857
18	55	Berlin	Berlin	ACoMA	anterior	0	3.330
19	56	Berlin	Berlin	MCA	MCA	1	2.092
20	57A	Berlin	Berlin	ICA	ICA	0	2.831
21	57B	Berlin	Berlin	ICA	ICA	0	4.277
22	57C	Berlin	Berlin	ICA	ICA	0	4.910
23	57D	Berlin	Berlin	ACoMA	anterior	1	2.565
24	57E	Berlin	Berlin	MCA	MCA	0	6.612
25	57F	Berlin	Berlin	MCA	MCA	0	1.536
26	57G	Berlin	Berlin	MCA	MCA	0	3.139
27	58	Berlin	Berlin	PCoMA	posterior	1	3.998
28	59	Berlin	Berlin	ICA	ICA	0	4.875
29	60A	Berlin	Berlin	MCA	MCA	0	8.547
30	60B	Berlin	Berlin	MCA	MCA	0	3.172
31	61	Berlin	Berlin	ACoMA	anterior	1	10.866
32	62	Berlin	Berlin	ICA	ICA	1	4.541
33	63	Berlin	Berlin	ACoMA	anterior	1	5.524
34	64	Berlin	Berlin	ICA	ICA	1	13.839
35	65	Berlin	Berlin	ICA	ICA	0	7.768
36	66	Berlin	Berlin	ACoMA	anterior	1	3.652
37	67	Berlin	Berlin	MCA	MCA	1	4.031
38	68	Berlin	Berlin	ACoMA	anterior	1	2.672
39	69	Berlin	Berlin	ICA	ICA	0	11.746
40	70	Berlin	Berlin	ACoMA	anterior	1	2.739
41	71	Berlin	Berlin	PCoMA	posterior	0	3.684
42	72A	Berlin	Berlin	PCoMA	posterior	0	9.969
43	72B	Berlin	Berlin	ACoMA	anterior	0	3.769
44	73	Berlin	Berlin	ACoMA	anterior	1	7.640
45	74	Berlin	Berlin	ICA	ICA	0	2.422
46	75A	Berlin	Berlin	PCoMA	posterior	0	2.277
47	75B	Berlin	Berlin	BA	posterior	1	4.556
48	76	Berlin	Berlin	PCoMA	posterior	1	4.974
49	77	Berlin	Berlin	MCA	MCA	0	10.165
50	78	Berlin	Berlin	MCA	MCA	0	5.020
51	79	Berlin	Berlin	ICA	ICA	0	9.202
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2	80	Berlin	Berlin	AComA	anterior	1	8.132
3	81	Berlin	Berlin	ICA	ICA	0	21.514
4	82A	Berlin	Berlin	ICA	ICA	0	2.039
5	82B	Berlin	Berlin	MCA	MCA	0	3.698
6	82C	Berlin	Berlin	ACA	anterior	0	1.486
7	83	Berlin	Berlin	PComA	posterior	0	10.503
8	84A	Berlin	Berlin	ICA	ICA	0	6.331
9	84B	Berlin	Berlin	MCA	MCA	0	3.509
10	85	Berlin	Berlin	MCA	MCA	0	2.996
11	86	Berlin	Berlin	MCA	MCA	0	2.575
12	87	Berlin	Berlin	AComA	anterior	1	3.971
13	88A	Berlin	Berlin	MCA	MCA	0	1.489
14	88B	Berlin	Berlin	MCA	MCA	0	2.304
15	89	Berlin	Berlin	ICA	ICA	0	5.728
16	90	Berlin	Berlin	MCA	MCA	0	4.016
17	91	Berlin	Berlin	AComA	anterior	0	6.147
18	92	Berlin	Berlin	PComA	posterior	0	7.023
19	93	Berlin	Berlin	PComA	posterior	1	10.373
20	94	Berlin	Berlin	MCA	MCA	0	19.183
21	95	Berlin	Berlin	AComA	anterior	1	6.261
22	96	Berlin	Berlin	ICA	ICA	0	5.202
23	97A	Berlin	Berlin	ICA	ICA	0	1.702
24	97B	Berlin	Berlin	AComA	anterior	0	5.381
25	98	Berlin	Berlin	PICA	posterior	1	4.524
26	99	Berlin	Berlin	PComA	posterior	0	6.067
27	100A	Berlin	Berlin	MCA	MCA	1	6.738
28	100B	Berlin	Berlin	ICA	ICA	0	2.364
29	100C	Berlin	Berlin	ICA	ICA	0	8.467
30	100D	Berlin	Berlin	MCA	MCA	0	2.488
31	100E	Berlin	Berlin	MCA	MCA	0	1.914
32	101	Berlin	Berlin	PComA	posterior	1	5.048
33	102	Berlin	Berlin	AComA	anterior	1	5.931
34	103	Berlin	Berlin	PCA	posterior	1	5.602
35	104	Berlin	Berlin	MCA	MCA	0	4.629
36	105	Berlin	Berlin	ICA	ICA	1	7.092
37	106	Berlin	Berlin	MCA	MCA	1	8.177
38	107	Berlin	Berlin	PComA	posterior	1	8.598
39	108	Berlin	Berlin	AComA	anterior	1	3.886
40	109	Berlin	Berlin	BA	posterior	1	13.918
41	110	Berlin	Berlin	BA	posterior	0	12.591
42	111	Berlin	Berlin	AComA	anterior	0	6.025
43	112	Berlin	Berlin	BA	posterior	1	7.000
44	113A	Berlin	Berlin	MCA	MCA	0	9.488
45	113B	Berlin	Berlin	MCA	MCA	0	6.242
46	114	Berlin	Berlin	MCA	MCA	1	3.622
47	115A	Hanover	Magdeburg	MCA	MCA	1	4.340
48	115B	Hanover	Magdeburg	MCA	MCA	0	1.149
49	116A	Hanover	Magdeburg	AComA	anterior	1	4.055
50	116B	Hanover	Magdeburg	AComA	anterior	0	1.031
51	117A	Hanover	Magdeburg	BA	posterior	1	8.476
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2	117B	Hanover	Magdeburg	ACoMA	anterior	0	4.088
3	118A	Hanover	Magdeburg	ACoMA	anterior	0	5.039
4	118B	Hanover	Magdeburg	PCoMA	posterior	1	4.528
5	119	Hanover	Magdeburg	MCA	MCA	1	1.132
6	120A	Hanover	Magdeburg	MCA	MCA	1	4.881
7	120B	Hanover	Magdeburg	ICA	ICA	1	2.325
8	121	Hanover	Magdeburg	ICA	ICA	1	18.704
9	122	Hanover	Magdeburg	ICA	ICA	0	6.667
10	123A	Hanover	Magdeburg	PCoMA	posterior	1	5.230
11	123B	Hanover	Magdeburg	MCA	MCA	0	2.984
12	124A	Hanover	Magdeburg	ACA	anterior	1	2.914
13	124B	Hanover	Magdeburg	ACoMA	anterior	0	1.201
14	124C	Hanover	Magdeburg	ACoMA	anterior	0	2.671
15	125	Hanover	Magdeburg	ICA	ICA	0	7.204
16	126A	Hanover	Magdeburg	MCA	MCA	1	8.466
17	126B	Hanover	Magdeburg	MCA	MCA	0	5.410
18	127A	Hanover	Magdeburg	ACoMA	anterior	1	2.663
19	127B	Hanover	Magdeburg	MCA	MCA	0	2.098
20	128A	Hanover	Magdeburg	ICA	ICA	1	1.429
21	128B	Hanover	Magdeburg	ICA	ICA	0	1.275
22	129A	Hanover	Magdeburg	BA	posterior	1	2.818
23	129B	Hanover	Magdeburg	SCA	posterior	0	1.293
24	130A	Hanover	Magdeburg	MCA	MCA	1	7.171
25	130B	Hanover	Magdeburg	ACoMA	anterior	0	4.247
26	131A	Hanover	Magdeburg	BA	posterior	0	4.863
27	131B	Hanover	Magdeburg	BA	posterior	1	3.992
28	132A	Hanover	Magdeburg	PCoMA	posterior	0	4.359
29	132B	Hanover	Magdeburg	ACoMA	anterior	1	16.578
30	133A	Hanover	Magdeburg	BA	posterior	1	6.042
31	133B	Hanover	Magdeburg	ACoMA	anterior	0	3.105
32	134A	Hanover	Magdeburg	MCA	MCA	1	6.298
33	134B	Hanover	Magdeburg	MCA	MCA	0	3.067
34	135	Hanover	Magdeburg	ICA	ICA	0	2.406
35	136A	Kiel	Magdeburg	MCA	MCA	0	1.108
36	136B	Kiel	Magdeburg	MCA	MCA	0	6.352
37	137	Kiel	Magdeburg	MCA	MCA	0	3.274
38	138	Kiel	Magdeburg	MCA	MCA	0	4.033
39	139	Kiel	Magdeburg	MCA	MCA	0	6.259
40	140	Kiel	Magdeburg	MCA	MCA	0	10.513
41	141	Kiel	Magdeburg	MCA	MCA	0	8.471
42	142	Kiel	Magdeburg	MCA	MCA	0	6.008
43	143	Kiel	Magdeburg	MCA	MCA	0	5.184
44	144	Kiel	Magdeburg	MCA	MCA	0	10.421
45	145	Kiel	Magdeburg	MCA	MCA	0	8.720
46	146A	Kiel	Magdeburg	MCA	MCA	0	6.242
47	146B	Kiel	Magdeburg	ACA	anterior	0	2.012
48	147A	Kiel	Magdeburg	MCA	MCA	0	5.580
49	147B	Kiel	Magdeburg	MCA	MCA	0	0.684
50	147C	Kiel	Magdeburg	MCA	MCA	0	0.573
51	147D	Kiel	Magdeburg	ACA	anterior	0	3.651
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2	147E	Kiel	Magdeburg	AComA	anterior	0	1.213
3	147F	Kiel	Magdeburg	AComA	anterior	0	1.384
4	148	Kiel	Magdeburg	MCA	MCA	0	4.650
5	149	Kiel	Magdeburg	MCA	MCA	0	6.489
6	150	Kiel	Magdeburg	MCA	MCA	0	4.962
7	151	Kiel	Magdeburg	MCA	MCA	0	3.962
8	152	Magdeburg	Magdeburg	MCA	MCA	0	5.866
9	153	Magdeburg	Magdeburg	ACA	anterior	1	3.594
10	154	Magdeburg	Magdeburg	PComA	posterior	1	9.941
11	155A	Magdeburg	Magdeburg	AComA	anterior	1	2.543
12	155B	Magdeburg	Magdeburg	AComA	anterior	0	3.589
13	155C	Magdeburg	Magdeburg	MCA	MCA	0	5.120
14	156A	Magdeburg	Magdeburg	ICA	ICA	0	7.048
15	156B	Magdeburg	Magdeburg	ICA	ICA	0	1.214
16	156C	Magdeburg	Magdeburg	ICA	ICA	0	1.765
17	156D	Magdeburg	Magdeburg	ICA	ICA	0	2.037
18	157	Magdeburg	Magdeburg	VA	posterior	1	5.194
19	158	Magdeburg	Magdeburg	AChA	ICA	0	3.248
20	159	Magdeburg	Magdeburg	MCA	MCA	0	5.645
21	160A	Magdeburg	Magdeburg	AChA	ICA	1	2.988
22	160B	Magdeburg	Magdeburg	ICA	ICA	0	2.842
23	161A	Magdeburg	Magdeburg	ICA	ICA	1	5.684
24	161B	Magdeburg	Magdeburg	ICA	ICA	0	2.089
25	161C	Magdeburg	Magdeburg	PICA	posterior	0	2.497
26	162	Magdeburg	Magdeburg	AChA	ICA	1	4.811
27	163	Magdeburg	Magdeburg	ICA	ICA	0	4.981
28	164	Magdeburg	Magdeburg	MCA	MCA	0	3.817
29	165A	Magdeburg	Magdeburg	MCA	MCA	0	3.419
30	165B	Magdeburg	Magdeburg	PComA	posterior	0	5.533
31	165C	Magdeburg	Magdeburg	BA	posterior	0	2.856
32	165D	Magdeburg	Magdeburg	SCA	posterior	1	4.595
33	166	Magdeburg	Magdeburg	ICA	ICA	0	3.638
34	167	Magdeburg	Magdeburg	ICA	ICA	0	3.481
35	168	Magdeburg	Magdeburg	ICA	ICA	0	6.061
36	169	Magdeburg	Magdeburg	ICA	ICA	0	7.142
37	170	Magdeburg	Magdeburg	ICA	ICA	0	5.557
38	171	Magdeburg	Magdeburg	ICA	ICA	0	11.276
39	172A	Magdeburg	Magdeburg	AComA	anterior	1	3.283
40	172B	Magdeburg	Magdeburg	MCA	MCA	0	2.319
41	173A	Magdeburg	Magdeburg	MCA	MCA	1	4.176
42	173B	Magdeburg	Magdeburg	ICA	ICA	0	3.188
43	174	Magdeburg	Magdeburg	ICA	ICA	0	3.711
44	175	Magdeburg	Magdeburg	MCA	MCA	0	4.156
45	176	Magdeburg	Magdeburg	AComA	anterior	0	3.397
46	177A	Magdeburg	Magdeburg	PComA	posterior	1	6.322
47	177B	Magdeburg	Magdeburg	BA	posterior	0	1.516
48	178	Magdeburg	Magdeburg	MCA	MCA	1	5.269
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	maximum c	maximum h	maximum d	bulge height	surface area	convex hull	minimal box	closed area	volume
	L_max	H_max	D_max	H_b	A	A_CH	A_MBS	A_closed	V
	mm	mm	mm	mm	cm ²	cm ²	cm ²	cm ²	ml
5	6.629	5.790	5.713	0.877	0.887	1.018	1.495	1.003	0.083
6	11.888	8.544	10.931	3.003	2.391	2.722	4.652	2.537	0.269
7	7.306	6.133	4.862	0.313	0.742	0.914	1.677	0.888	0.064
8	7.867	6.544	7.165	3.567	1.018	1.146	1.979	1.122	0.097
9	7.336	6.315	6.104	1.929	0.888	1.022	1.749	1.014	0.085
10	6.275	4.482	5.783	0.575	0.693	0.906	1.269	0.900	0.074
11	23.888	20.508	23.475	9.621	12.495	13.243	18.371	13.239	4.106
12	6.597	4.534	6.403	1.473	0.746	0.934	1.422	0.924	0.076
13	5.837	3.939	5.183	0.070	0.568	0.802	1.099	0.795	0.060
14	6.518	5.449	5.861	2.398	0.713	0.822	1.338	0.809	0.059
15	8.495	6.902	7.441	3.391	1.540	1.813	2.341	1.803	0.215
16	11.246	9.797	10.200	3.153	1.755	1.899	3.981	1.853	0.195
17	11.394	8.611	10.972	4.429	2.218	2.475	4.079	2.459	0.334
18	7.308	4.479	7.292	0.287	0.574	0.844	1.684	0.826	0.059
19	4.672	3.411	4.157	0.033	0.354	0.489	0.729	0.486	0.027
20	13.627	11.834	11.081	4.341	3.153	3.480	5.839	3.381	0.526
21	2.875	1.899	2.875	0.057	0.126	0.180	0.276	0.178	0.006
22	14.303	12.591	12.333	6.473	3.921	4.285	6.591	4.242	0.730
23	3.763	2.874	3.382	1.302	0.281	0.342	0.445	0.341	0.018
24	5.669	4.725	4.473	2.104	0.553	0.648	1.015	0.643	0.044
25	7.910	6.289	6.673	3.770	1.024	1.175	1.970	1.151	0.101
26	6.439	5.233	5.830	1.474	0.815	0.991	1.327	0.978	0.081
27	12.632	11.229	10.859	3.425	3.001	3.307	5.029	3.293	0.523
28	8.453	6.020	7.820	1.936	0.987	1.244	2.245	1.236	0.112
29	9.521	8.035	9.229	3.504	2.125	2.439	2.878	2.433	0.344
30	8.530	5.733	7.294	1.949	1.050	1.420	2.328	1.397	0.132
31	4.793	3.005	4.741	0.075	0.310	0.479	0.797	0.470	0.025
32	14.667	10.280	13.848	1.293	4.122	5.440	6.782	5.419	1.129
33	7.677	4.990	6.526	2.190	0.873	1.094	1.890	1.060	0.085
34	8.500	5.691	8.412	2.083	1.088	1.325	2.270	1.310	0.124
35	10.420	6.548	10.246	2.938	1.204	1.480	3.411	1.377	0.112
36	15.754	13.711	11.401	3.704	3.516	3.937	7.802	3.868	0.564
37	6.137	4.508	5.343	2.007	0.663	0.820	1.184	0.817	0.063
38	6.677	3.854	6.460	1.201	0.590	0.769	1.402	0.757	0.054
39	6.751	5.481	4.736	1.330	0.577	0.716	1.432	0.696	0.045
40	3.661	2.760	3.246	1.172	0.232	0.303	0.424	0.301	0.014
41	6.655	5.163	5.034	1.727	0.691	0.832	1.391	0.823	0.062
42	8.135	5.839	7.993	1.423	1.186	1.438	2.167	1.417	0.142
43	16.986	10.740	15.845	2.213	5.926	6.882	9.209	6.869	1.564
44	7.950	6.713	6.080	1.989	1.030	1.244	2.022	1.224	0.108
45	5.212	3.563	5.005	0.689	0.483	0.669	0.895	0.665	0.046
46	12.891	11.777	8.932	5.558	2.584	2.875	5.260	2.844	0.398
47	24.926	21.090	22.734	9.915	14.654	15.321	19.652	15.279	5.424
48	8.946	6.977	8.075	2.268	1.298	1.555	2.541	1.527	0.157
49	14.786	10.742	14.206	1.633	2.875	3.216	6.868	3.132	0.407
50	6.715	5.085	5.948	1.913	0.712	0.843	1.420	0.839	0.066
51	15.827	13.957	14.042	6.937	5.487	5.906	7.992	5.870	1.249

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2	6.419	4.551	6.134	0.624	0.618	0.839	1.316	0.813	0.058
3	8.062	6.217	6.768	2.455	1.126	1.368	2.042	1.365	0.137
4	17.188	10.658	16.238	2.250	3.236	4.445	9.425	4.430	0.696
5	7.303	4.996	6.301	1.470	0.688	0.925	1.676	0.910	0.072
6	4.605	2.692	4.603	0.037	0.296	0.466	0.713	0.462	0.023
7	4.605	3.619	3.564	1.963	0.355	0.438	0.677	0.430	0.023
8	4.653	2.599	4.537	0.354	0.303	0.480	0.698	0.475	0.025
9	13.326	11.629	11.342	5.799	3.546	3.816	5.596	3.800	0.658
10	7.105	4.947	6.019	0.113	0.678	0.891	1.586	0.882	0.061
11	4.777	2.888	4.516	0.482	0.282	0.439	0.727	0.433	0.023
12	18.334	17.219	14.463	8.226	5.638	6.064	10.560	5.978	1.232
13	11.513	9.974	11.050	4.580	2.241	2.481	4.240	2.396	0.285
14	6.880	5.489	6.061	2.068	0.829	0.999	1.492	0.993	0.086
15	4.149	2.840	3.778	0.926	0.297	0.384	0.541	0.382	0.021
16	11.234	7.779	10.623	2.600	2.129	2.279	3.965	2.254	0.282
17	6.535	5.085	5.126	0.262	0.507	0.706	1.400	0.685	0.041
18	6.195	3.881	6.006	0.616	0.577	0.840	1.210	0.829	0.061
19	4.282	2.759	3.841	0.151	0.216	0.331	0.590	0.325	0.013
20	5.968	3.703	5.938	1.423	0.517	0.678	1.119	0.668	0.043
21	4.773	4.310	4.200	2.368	0.467	0.513	0.771	0.506	0.031
22	9.479	6.686	9.469	2.116	1.305	1.446	2.823	1.429	0.139
23	4.362	2.739	4.165	0.197	0.326	0.447	0.600	0.445	0.025
24	7.928	6.831	6.578	2.903	1.256	1.465	2.026	1.456	0.154
25	2.798	1.593	2.792	0.014	0.105	0.170	0.266	0.167	0.005
26	6.330	3.703	6.047	0.954	0.580	0.806	1.259	0.803	0.058
27	7.668	6.509	6.943	1.249	0.852	1.054	1.873	0.999	0.070
28	8.038	5.767	7.357	1.708	0.972	1.152	2.030	1.143	0.103
29	13.384	9.880	12.864	3.835	3.174	3.751	5.854	3.690	0.603
30	4.583	3.361	4.077	0.084	0.364	0.502	0.704	0.498	0.030
31	13.573	12.129	7.940	6.398	2.411	2.619	5.788	2.564	0.328
32	6.253	4.782	5.560	2.596	0.679	0.785	1.232	0.782	0.060
33	6.774	5.738	4.776	1.687	0.752	0.882	1.467	0.876	0.070
34	19.580	14.862	19.183	7.524	7.554	7.889	12.044	7.851	1.917
35	10.702	7.977	8.927	2.139	2.019	2.495	3.606	2.481	0.325
36	6.698	4.629	5.540	0.489	0.576	0.764	1.410	0.757	0.055
37	6.354	4.692	5.177	1.312	0.626	0.795	1.289	0.776	0.053
38	6.204	3.207	6.016	0.114	0.413	0.706	1.215	0.694	0.044
39	14.376	13.009	10.934	6.325	2.638	2.994	6.492	2.830	0.343
40	6.016	4.460	5.142	0.926	0.678	0.873	1.149	0.866	0.071
41	5.832	3.890	5.511	0.286	0.536	0.691	1.071	0.684	0.046
42	14.708	12.119	12.964	4.615	3.419	3.829	6.796	3.791	0.609
43	5.100	3.825	4.479	0.525	0.452	0.611	0.840	0.603	0.038
44	10.529	8.923	7.517	2.011	1.266	1.421	3.483	1.355	0.113
45	6.886	3.607	6.764	0.185	0.510	0.851	1.490	0.837	0.060
46	4.974	3.155	4.670	0.739	0.312	0.487	0.792	0.479	0.026
47	6.182	5.235	3.884	2.072	0.422	0.503	1.203	0.487	0.025
48	8.405	5.927	8.296	2.748	1.255	1.408	2.270	1.385	0.133
49	15.254	10.492	15.251	1.120	3.825	4.559	7.665	4.507	0.804
50	7.735	5.096	7.199	1.289	0.956	1.265	1.925	1.236	0.115
51	11.062	9.776	9.388	5.048	2.352	2.598	3.900	2.577	0.353
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2	9.022	8.308	5.532	5.605	1.258	1.403	2.566	1.369	0.125
3	32.342	25.628	30.344	9.085	21.842	22.485	32.901	22.541	9.061
4	3.400	2.107	3.340	0.103	0.171	0.249	0.382	0.247	0.010
5	5.047	4.006	3.660	0.257	0.368	0.480	0.802	0.479	0.028
6	3.134	1.819	3.062	0.002	0.128	0.204	0.325	0.203	0.007
7	13.558	11.007	11.469	5.880	3.372	4.048	5.907	3.950	0.645
8	8.282	6.772	7.749	2.957	1.357	1.578	2.227	1.567	0.170
9	5.390	3.909	3.582	0.036	0.363	0.503	0.917	0.497	0.029
10	5.401	3.552	5.038	1.301	0.435	0.613	0.917	0.611	0.042
11	3.966	2.604	3.799	0.123	0.269	0.369	0.506	0.368	0.019
12	5.633	4.386	4.464	0.942	0.531	0.621	1.001	0.614	0.039
13	3.149	1.664	3.147	0.170	0.102	0.155	0.311	0.153	0.005
14	3.784	2.577	3.258	0.475	0.191	0.258	0.454	0.256	0.011
15	7.951	6.459	5.903	0.045	0.885	1.210	2.142	1.167	0.093
16	6.817	4.506	6.387	1.055	0.691	0.886	1.462	0.880	0.067
17	7.784	6.322	6.895	2.712	1.231	1.415	1.903	1.412	0.152
18	12.441	7.739	12.162	1.572	2.313	2.941	4.898	2.904	0.402
19	16.422	12.513	15.861	2.894	4.492	4.998	8.482	4.966	0.797
20	27.009	21.425	25.069	8.693	14.959	16.042	22.918	16.010	5.763
21	8.947	7.350	6.990	2.234	1.135	1.351	2.515	1.341	0.128
22	13.291	8.491	13.104	0.615	2.474	3.251	5.883	3.166	0.379
23	5.671	2.993	5.671	0.100	0.283	0.495	1.011	0.489	0.019
24	8.214	5.554	7.968	1.932	1.237	1.574	2.124	1.572	0.170
25	5.584	4.790	4.319	2.528	0.481	0.539	0.980	0.527	0.031
26	9.725	6.554	9.274	1.314	1.459	1.953	2.971	1.944	0.238
27	16.284	12.471	15.055	0.726	3.620	4.000	8.331	3.963	0.645
28	3.707	2.472	3.379	0.531	0.221	0.311	0.445	0.309	0.014
29	16.159	11.384	16.159	4.627	3.858	4.256	8.203	4.029	0.506
30	4.053	2.688	3.620	0.707	0.258	0.349	0.516	0.347	0.016
31	3.744	1.985	3.743	0.076	0.186	0.285	0.442	0.282	0.011
32	6.956	5.626	4.803	1.591	0.669	0.821	1.525	0.808	0.058
33	7.936	6.362	7.128	3.081	1.178	1.318	2.163	1.302	0.120
34	9.195	6.126	7.318	1.738	1.708	1.836	2.661	1.858	0.209
35	17.009	8.810	16.189	0.942	2.437	3.849	9.088	3.752	0.562
36	9.263	7.602	7.208	3.536	1.222	1.383	2.696	1.338	0.114
37	10.514	8.759	7.409	3.082	1.494	1.771	3.482	1.712	0.151
38	10.231	8.838	7.094	2.851	1.488	1.803	3.372	1.739	0.166
39	6.100	4.339	5.591	0.679	0.516	0.732	1.220	0.722	0.048
40	17.012	13.949	16.935	6.552	6.058	6.416	9.100	6.386	1.433
41	18.621	14.380	14.373	6.548	4.829	5.408	10.893	5.328	0.999
42	9.774	6.785	8.878	1.968	1.741	2.204	3.001	2.190	0.285
43	10.375	7.553	9.325	3.307	1.779	2.280	3.443	2.262	0.286
44	11.542	9.849	7.908	4.661	2.103	2.433	4.190	2.390	0.308
45	8.757	6.907	8.753	2.415	1.552	1.848	2.420	1.841	0.224
46	6.793	4.234	6.753	0.367	0.597	0.920	1.502	0.910	0.068
47	6.195	5.019	5.753	2.072	0.634	0.738	1.213	0.721	0.049
48	2.123	1.222	2.050	0.099	0.062	0.091	0.144	0.089	0.002
49	7.276	4.568	7.267	1.827	0.795	0.957	1.663	0.935	0.073
50	2.744	1.425	2.563	0.133	0.078	0.128	0.237	0.123	0.003
51	10.853	8.721	9.956	2.319	2.269	2.569	3.723	2.547	0.342
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2	6.386	4.271	6.267	1.450	0.622	0.798	1.282	0.779	0.052
3	7.385	6.025	5.712	3.287	0.847	0.981	1.714	0.961	0.077
4	6.224	4.693	5.826	1.532	0.584	0.710	1.218	0.686	0.040
5	2.739	1.458	2.699	0.000	0.079	0.137	0.248	0.129	0.003
6	6.758	5.613	6.202	3.057	0.747	0.850	1.552	0.826	0.060
7	8.335	5.295	8.154	0.578	0.472	0.673	2.182	0.626	0.032
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9	24.223	19.791	22.453	9.808	12.666	13.149	18.524	13.126	4.170
10	9.429	7.753	9.246	3.668	1.763	2.018	2.881	1.991	0.233
11	7.279	5.501	6.496	1.296	0.962	1.180	1.701	1.156	0.093
12	4.951	3.068	4.238	0.721	0.311	0.403	0.770	0.396	0.018
13	3.677	3.075	2.630	1.197	0.197	0.240	0.431	0.230	0.008
14	3.184	1.674	2.913	0.185	0.096	0.166	0.322	0.159	0.004
15	4.432	3.209	4.075	1.200	0.283	0.349	0.626	0.346	0.016
16	8.784	7.818	6.956	3.946	1.370	1.477	2.435	1.460	0.148
17	13.905	9.021	13.148	0.801	2.857	3.336	6.331	3.136	0.362
18	7.117	5.697	7.117	1.111	0.959	1.100	1.716	1.067	0.083
19	4.398	3.418	3.652	1.122	0.260	0.319	0.609	0.314	0.014
20	4.263	2.616	3.714	0.022	0.236	0.323	0.576	0.316	0.014
21	3.378	1.853	3.377	0.224	0.119	0.210	0.389	0.196	0.005
22	5.130	2.891	4.336	0.308	0.177	0.292	0.827	0.275	0.008
23	5.027	3.392	4.348	1.368	0.315	0.392	0.795	0.385	0.019
24	2.603	1.519	2.548	0.128	0.096	0.144	0.214	0.138	0.004
25	8.733	7.733	5.173	2.236	1.000	1.104	2.399	1.082	0.087
26	6.282	4.788	4.997	1.219	0.529	0.634	1.242	0.623	0.038
27	6.960	6.297	6.263	3.045	0.617	0.691	1.556	0.649	0.035
28	6.109	4.679	5.536	1.914	0.602	0.685	1.173	0.680	0.047
29	8.258	5.056	7.901	0.962	0.957	1.190	2.143	1.166	0.099
30	21.893	19.479	15.008	5.305	5.825	6.171	15.090	6.046	1.094
31	7.690	6.527	5.130	2.092	0.820	0.984	1.861	0.906	0.058
32	4.236	3.327	2.935	1.359	0.267	0.320	0.564	0.310	0.014
33	7.909	6.999	6.604	1.846	1.191	1.329	1.991	1.306	0.123
34	5.815	3.677	4.000	0.846	0.324	0.434	1.062	0.406	0.019
35	7.097	4.213	6.014	0.103	0.332	0.541	1.582	0.515	0.023
36	2.628	1.504	2.617	0.126	0.075	0.129	0.227	0.120	0.003
37	6.801	6.385	4.171	3.307	0.723	0.806	1.476	0.797	0.058
38	5.605	3.754	5.144	1.846	0.487	0.608	0.987	0.597	0.037
39	6.085	4.188	5.097	1.013	0.566	0.707	1.164	0.693	0.046
40	10.066	6.868	9.700	2.978	1.972	2.370	3.227	2.338	0.291
41	11.565	10.869	9.066	5.115	2.694	2.806	4.206	2.801	0.417
42	10.003	8.861	9.695	3.555	2.151	2.310	3.143	2.295	0.306
43	6.948	6.210	4.669	2.279	0.766	0.840	1.517	0.825	0.061
44	8.098	6.481	7.268	3.584	1.033	1.168	2.064	1.144	0.093
45	15.923	12.736	11.639	3.653	3.319	3.922	7.966	3.711	0.511
46	9.220	8.728	6.525	5.970	1.325	1.489	2.729	1.424	0.127
47	8.947	7.049	8.891	2.469	1.606	1.828	2.595	1.814	0.208
48	3.410	2.529	3.319	1.196	0.188	0.222	0.369	0.217	0.008
49	6.977	5.759	5.449	1.556	0.777	0.934	1.530	0.903	0.066
50	1.627	0.900	1.540	0.310	0.031	0.050	0.090	0.047	0.001
51	1.571	0.846	1.511	0.124	0.026	0.044	0.080	0.041	0.001
52	4.670	3.829	3.715	0.862	0.374	0.442	0.707	0.433	0.023
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2	2.495	1.472	2.180	0.087	0.072	0.103	0.196	0.100	0.002
3	2.449	1.457	2.325	0.046	0.086	0.131	0.194	0.125	0.003
4	9.599	6.040	9.240	1.954	1.225	1.478	2.895	1.465	0.128
5	7.998	6.644	5.913	3.660	1.019	1.183	2.072	1.148	0.100
6	7.328	5.848	5.773	2.070	0.814	0.905	1.687	0.887	0.066
7	6.486	5.072	6.312	0.846	0.639	0.755	1.334	0.750	0.052
8	7.722	6.054	7.580	2.357	1.147	1.296	1.910	1.270	0.117
9	4.784	3.869	4.102	1.291	0.329	0.390	0.719	0.383	0.019
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11	15.603	11.496	14.341	7.003	4.024	4.638	7.675	4.569	0.809
12	5.647	3.274	5.306	0.026	0.355	0.466	1.003	0.451	0.021
13	4.724	3.696	4.160	1.815	0.429	0.518	0.707	0.510	0.030
14	6.943	5.844	5.841	1.209	0.657	0.807	1.560	0.764	0.049
15	11.331	8.473	9.336	2.050	1.711	1.957	4.035	1.938	0.218
16	3.405	1.788	3.124	0.171	0.121	0.195	0.369	0.189	0.005
17	3.375	1.970	3.356	0.117	0.146	0.221	0.377	0.215	0.007
18	2.674	2.099	2.427	0.125	0.119	0.164	0.251	0.160	0.005
19	6.651	5.678	4.727	3.075	0.642	0.716	1.397	0.705	0.049
20	4.557	3.452	4.551	1.438	0.388	0.466	0.672	0.457	0.025
21	6.241	5.711	6.021	2.024	0.837	0.928	1.273	0.922	0.073
22	4.200	3.054	3.431	0.180	0.273	0.358	0.574	0.350	0.016
23	4.277	3.071	4.011	1.379	0.341	0.433	0.576	0.427	0.023
24	7.789	6.371	6.026	2.151	0.819	0.987	1.906	0.932	0.060
25	2.779	2.123	2.323	0.573	0.137	0.172	0.243	0.171	0.006
26	3.590	2.777	3.414	1.580	0.240	0.286	0.408	0.278	0.012
27	6.957	6.079	6.471	2.907	0.713	0.780	1.524	0.750	0.048
28	5.784	5.145	4.269	1.733	0.498	0.560	1.051	0.547	0.030
29	5.795	4.770	4.652	1.961	0.401	0.530	1.068	0.476	0.021
30	5.333	3.786	4.835	0.986	0.424	0.507	0.893	0.498	0.028
31	7.607	6.500	4.457	3.691	0.723	0.793	1.818	0.773	0.053
32	4.095	3.019	3.578	1.043	0.276	0.374	0.556	0.364	0.017
33	5.900	5.509	4.218	3.215	0.545	0.570	1.098	0.557	0.031
34	5.574	3.949	5.005	1.532	0.505	0.630	0.977	0.624	0.041
35	5.053	3.735	4.455	1.533	0.398	0.461	0.803	0.454	0.025
36	9.075	6.193	9.068	2.564	1.532	1.753	2.802	1.731	0.191
37	7.748	7.232	7.453	3.980	1.306	1.395	1.963	1.378	0.139
38	7.203	5.799	5.440	1.852	0.826	0.957	1.631	0.925	0.070
39	15.720	12.308	14.026	4.352	4.479	5.063	7.782	5.036	0.977
40	5.186	4.052	3.267	1.796	0.280	0.347	0.845	0.322	0.012
41	5.388	2.932	4.739	0.773	0.335	0.421	0.912	0.407	0.018
42	6.487	5.148	5.922	1.965	0.654	0.765	1.340	0.742	0.050
43	5.446	3.837	5.297	1.539	0.461	0.549	0.932	0.537	0.031
44	4.406	3.846	4.243	1.228	0.391	0.445	0.653	0.440	0.025
45	5.714	4.684	5.562	1.815	0.544	0.612	1.026	0.588	0.034
46	5.047	4.191	3.070	1.619	0.276	0.311	0.801	0.289	0.012
47	7.755	6.941	4.725	4.013	0.823	0.909	1.891	0.893	0.066
48	2.901	1.778	2.668	0.019	0.107	0.158	0.278	0.150	0.004
49	6.661	5.753	4.657	1.227	0.646	0.769	1.394	0.738	0.048
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	convex hull	minimal bo	minimum n	maximum r	neck perim	equivalent	neck area	elliptical ne	aspect ratio
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	ml	ml	mm	mm	mm	mm	cm ²	cm ²	-
5	0.091	0.172	2.903	3.885	13.086	3.537	0.116	0.089	1.479
6	0.372	0.943	2.992	5.434	17.029	3.417	0.145	0.128	1.520
7	0.071	0.204	3.276	4.862	14.831	3.926	0.146	0.125	1.239
8	0.105	0.262	2.412	3.903	13.317	3.147	0.105	0.074	1.460
9	0.087	0.217	2.835	4.497	15.471	3.260	0.126	0.100	1.260
10	0.076	0.134	4.243	5.252	19.040	4.336	0.206	0.175	0.543
11	4.299	7.404	7.102	11.374	37.990	7.833	0.744	0.634	1.721
12	0.080	0.160	2.937	5.732	18.940	3.767	0.178	0.132	0.733
13	0.062	0.108	3.700	5.163	19.585	4.624	0.226	0.150	0.735
14	0.062	0.145	3.135	3.555	11.360	3.390	0.096	0.088	1.421
15	0.219	0.337	4.061	6.687	22.302	4.713	0.263	0.213	1.015
16	0.211	0.747	2.896	4.022	12.395	3.169	0.098	0.091	1.892
17	0.343	0.775	4.591	6.207	19.420	4.961	0.241	0.224	1.314
18	0.064	0.205	3.911	6.350	21.036	4.791	0.252	0.195	0.400
19	0.028	0.058	3.525	4.157	13.267	3.968	0.132	0.115	0.769
20	0.567	1.327	4.216	6.408	19.835	4.605	0.228	0.212	1.496
21	0.006	0.014	1.920	2.875	8.841	2.356	0.052	0.043	0.654
22	0.765	1.591	5.778	6.676	22.660	5.667	0.321	0.303	1.837
23	0.018	0.028	2.370	2.886	9.061	2.653	0.060	0.054	0.967
24	0.045	0.096	2.781	3.684	11.481	3.120	0.090	0.080	1.230
25	0.110	0.260	3.374	4.360	13.771	3.700	0.127	0.116	1.284
26	0.085	0.144	4.129	4.939	15.345	4.263	0.164	0.160	1.048
27	0.535	1.061	5.283	6.859	21.247	5.494	0.292	0.285	1.541
28	0.116	0.316	4.399	6.782	20.002	4.982	0.249	0.234	0.732
29	0.349	0.459	5.692	6.345	21.843	5.642	0.308	0.284	1.246
30	0.144	0.334	5.051	7.400	24.248	5.730	0.347	0.294	0.621
31	0.027	0.067	3.554	4.752	15.381	4.143	0.159	0.133	0.612
32	1.148	1.661	6.103	13.945	53.525	9.693	1.297	0.668	0.608
33	0.096	0.244	3.241	5.421	18.057	4.145	0.187	0.138	0.776
34	0.131	0.322	4.742	5.937	19.016	4.669	0.222	0.221	0.774
35	0.140	0.592	3.148	5.233	16.748	4.119	0.172	0.129	1.047
36	0.640	2.049	6.067	6.812	24.497	5.741	0.352	0.325	1.876
37	0.065	0.121	3.929	4.537	15.469	3.986	0.154	0.140	0.899
38	0.057	0.156	2.964	5.044	16.782	3.982	0.167	0.117	0.622
39	0.049	0.161	2.859	4.073	13.567	3.522	0.119	0.091	1.249
40	0.015	0.026	2.338	3.094	9.103	3.028	0.069	0.057	0.878
41	0.065	0.154	3.388	4.395	14.337	3.683	0.132	0.117	1.134
42	0.150	0.300	4.221	5.874	20.243	4.553	0.230	0.195	0.773
43	1.618	2.628	7.460	14.252	45.129	8.355	0.943	0.835	0.665
44	0.118	0.270	3.389	5.919	16.909	4.575	0.193	0.158	1.049
45	0.048	0.080	4.100	4.888	16.858	4.339	0.183	0.157	0.692
46	0.413	1.134	4.955	5.832	21.532	4.829	0.260	0.227	2.005
47	5.489	8.192	4.856	13.272	38.744	6.453	0.625	0.506	1.563
48	0.166	0.381	4.146	5.861	19.226	4.767	0.229	0.191	0.946
49	0.471	1.692	4.251	6.311	19.493	5.268	0.257	0.211	1.331
50	0.068	0.159	3.330	4.548	14.206	3.568	0.127	0.119	0.943
51	1.284	2.125	5.828	7.791	26.972	5.678	0.383	0.357	1.769

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2	0.065	0.142	2.869	6.280	18.787	4.153	0.195	0.141	0.685
3	0.140	0.274	5.099	5.722	19.742	4.850	0.239	0.229	1.030
4	0.723	2.721	9.411	15.328	45.262	10.554	1.194	1.133	0.448
5	0.076	0.204	3.921	5.390	19.347	4.578	0.221	0.166	0.782
6	0.025	0.057	4.072	4.605	15.924	4.153	0.165	0.147	0.524
7	0.025	0.052	2.544	3.498	10.509	2.840	0.075	0.070	1.001
8	0.027	0.055	3.973	4.537	15.822	4.355	0.172	0.142	0.506
9	0.671	1.245	5.067	6.060	20.235	5.028	0.254	0.241	1.844
10	0.067	0.188	4.039	6.019	18.197	4.473	0.203	0.191	0.770
11	0.024	0.058	3.349	4.139	15.221	3.971	0.151	0.109	0.532
12	1.284	3.227	3.904	8.491	26.453	5.140	0.340	0.260	2.001
13	0.334	0.821	3.698	5.097	15.808	3.937	0.156	0.148	1.489
14	0.088	0.171	3.652	5.028	14.943	4.393	0.164	0.144	1.004
15	0.021	0.037	2.695	3.182	10.976	3.122	0.086	0.067	0.874
16	0.296	0.742	3.682	4.035	12.878	3.887	0.125	0.117	1.693
17	0.047	0.156	3.958	5.126	15.600	4.569	0.178	0.159	0.948
18	0.065	0.125	3.926	6.009	20.114	5.003	0.252	0.185	0.554
19	0.015	0.043	3.044	3.841	13.047	3.343	0.109	0.092	0.545
20	0.048	0.111	3.747	4.646	14.887	4.055	0.151	0.137	0.609
21	0.032	0.064	1.743	2.212	6.685	2.312	0.039	0.030	1.934
22	0.146	0.446	3.494	4.013	13.901	3.573	0.124	0.110	1.223
23	0.026	0.044	3.340	4.165	13.007	3.667	0.119	0.109	0.616
24	0.158	0.271	3.373	5.696	18.626	4.310	0.201	0.151	1.161
25	0.006	0.013	2.149	2.798	9.586	2.605	0.062	0.047	0.549
26	0.059	0.133	4.544	5.666	18.559	4.809	0.223	0.202	0.554
27	0.088	0.241	3.240	5.327	15.348	3.834	0.147	0.136	0.751
28	0.106	0.272	3.982	5.445	15.999	4.286	0.171	0.170	0.895
29	0.635	1.332	5.655	8.968	30.914	6.682	0.516	0.398	0.953
30	0.031	0.056	3.242	4.090	14.393	3.732	0.134	0.104	0.775
31	0.352	1.309	4.023	4.674	15.332	4.004	0.153	0.148	2.325
32	0.062	0.129	3.028	3.756	12.271	3.335	0.102	0.089	1.209
33	0.072	0.167	3.273	4.162	13.626	3.661	0.125	0.107	1.327
34	1.971	3.931	5.400	6.936	23.221	5.117	0.297	0.294	1.995
35	0.349	0.644	6.668	7.542	25.103	7.353	0.461	0.395	1.030
36	0.057	0.157	2.954	5.757	18.913	3.839	0.182	0.134	0.634
37	0.060	0.138	3.374	4.303	14.245	4.211	0.150	0.114	0.937
38	0.048	0.126	4.114	6.204	23.009	4.885	0.281	0.200	0.431
39	0.410	1.556	4.088	5.305	16.784	4.591	0.193	0.170	2.214
40	0.073	0.116	2.687	5.335	20.340	3.712	0.189	0.113	0.513
41	0.049	0.104	2.559	5.530	16.327	3.620	0.148	0.111	0.666
42	0.647	1.666	5.581	7.501	23.891	6.226	0.372	0.329	1.329
43	0.041	0.072	3.421	4.484	14.463	4.178	0.151	0.120	0.841
44	0.133	0.611	2.123	4.861	12.221	2.913	0.089	0.081	1.572
45	0.064	0.171	4.645	6.823	21.514	6.082	0.327	0.249	0.355
46	0.029	0.066	3.453	4.611	16.463	4.059	0.167	0.125	0.494
47	0.028	0.124	2.466	2.877	9.725	2.697	0.066	0.056	1.584
48	0.144	0.322	2.931	4.907	13.849	3.745	0.130	0.113	1.014
49	0.831	1.995	3.693	15.254	44.240	6.164	0.682	0.442	0.666
50	0.123	0.251	3.660	5.911	21.822	5.129	0.280	0.170	0.849
51	0.370	0.724	4.471	5.481	18.185	4.966	0.226	0.193	1.679
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2	0.138	0.387	3.088	3.831	12.450	3.565	0.111	0.093	2.122
3	9.561	17.746	2.961	18.027	50.338	5.556	0.699	0.419	1.193
4	0.010	0.022	2.536	3.340	10.417	2.938	0.077	0.067	0.611
5	0.028	0.068	2.961	3.628	12.388	3.587	0.111	0.084	1.019
6	0.007	0.017	2.669	3.062	9.724	3.065	0.075	0.064	0.485
7	0.709	1.350	6.233	9.921	32.559	7.095	0.578	0.486	1.059
8	0.177	0.312	3.682	5.598	18.267	4.597	0.210	0.162	1.131
9	0.030	0.083	3.109	3.713	13.372	4.008	0.134	0.091	0.945
10	0.043	0.083	2.949	4.596	16.118	4.349	0.175	0.106	0.652
11	0.019	0.034	3.058	3.824	11.763	3.366	0.099	0.092	0.673
12	0.041	0.094	2.402	3.999	11.654	2.840	0.083	0.075	0.993
13	0.005	0.016	1.871	3.149	9.064	2.252	0.051	0.046	0.473
14	0.011	0.029	2.480	2.749	9.781	2.680	0.066	0.054	0.838
15	0.105	0.295	5.164	6.092	19.890	5.675	0.282	0.247	0.940
16	0.071	0.166	3.647	5.591	18.794	4.024	0.189	0.160	0.718
17	0.154	0.247	3.845	5.198	17.087	4.221	0.180	0.157	1.182
18	0.433	1.019	7.600	9.255	32.052	7.377	0.591	0.552	0.759
19	0.946	2.323	5.854	9.288	29.079	6.525	0.474	0.427	1.117
20	5.822	10.316	10.249	12.646	43.430	9.687	1.052	1.018	1.517
21	0.133	0.375	4.577	4.981	16.951	4.848	0.205	0.179	1.257
22	0.457	1.342	6.603	9.821	38.845	7.126	0.692	0.509	0.530
23	0.021	0.096	4.180	5.671	18.176	4.536	0.206	0.186	0.300
24	0.173	0.291	5.563	7.294	22.990	5.826	0.335	0.319	0.738
25	0.033	0.091	1.425	2.956	8.692	2.091	0.045	0.033	1.531
26	0.242	0.482	6.692	7.545	27.655	7.023	0.486	0.397	0.804
27	0.673	2.261	4.714	7.341	25.595	5.352	0.342	0.272	0.918
28	0.014	0.028	3.033	3.304	11.382	3.083	0.088	0.079	0.715
29	0.705	2.209	3.936	5.479	16.917	4.038	0.171	0.169	1.545
30	0.017	0.035	2.888	3.555	11.320	3.126	0.088	0.081	0.700
31	0.012	0.028	2.723	3.744	12.259	3.122	0.096	0.080	0.511
32	0.062	0.177	3.927	4.189	14.081	3.967	0.140	0.129	1.205
33	0.129	0.299	3.261	4.724	14.375	3.444	0.124	0.121	1.255
34	0.223	0.408	1.690	6.942	22.424	2.675	0.150	0.092	0.807
35	0.604	2.576	9.516	16.051	57.167	9.204	1.315	1.200	0.288
36	0.133	0.416	3.427	4.118	13.379	3.487	0.117	0.111	1.722
37	0.190	0.611	4.209	5.875	18.330	4.775	0.219	0.194	1.392
38	0.200	0.582	4.580	5.781	20.002	5.026	0.251	0.208	1.487
39	0.052	0.127	4.276	4.986	17.482	4.697	0.205	0.167	0.779
40	1.463	2.581	5.536	7.179	23.516	5.577	0.328	0.312	1.939
41	1.064	3.380	4.917	12.472	34.457	5.794	0.499	0.482	1.010
42	0.294	0.489	4.505	8.378	31.391	5.719	0.449	0.296	0.719
43	0.301	0.601	6.063	8.092	28.011	6.899	0.483	0.385	0.865
44	0.323	0.806	3.486	7.314	23.602	4.859	0.287	0.200	1.297
45	0.227	0.354	3.933	6.501	22.813	5.068	0.289	0.201	0.960
46	0.072	0.173	4.796	6.793	21.520	5.804	0.312	0.256	0.533
47	0.054	0.126	2.981	3.763	11.219	3.091	0.087	0.088	1.153
48	0.002	0.005	1.667	2.050	6.305	1.717	0.027	0.027	0.561
49	0.080	0.202	3.798	4.688	14.879	3.770	0.140	0.140	0.865
50	0.003	0.011	2.058	2.646	8.188	2.184	0.045	0.043	0.390
51	0.364	0.676	4.880	7.274	20.777	5.344	0.278	0.279	1.165
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2	0.059	0.136	3.633	5.216	16.163	3.879	0.157	0.149	0.784
3	0.083	0.211	3.466	3.933	13.148	3.467	0.114	0.107	1.281
4	0.049	0.126	3.027	4.428	12.646	3.207	0.101	0.105	1.023
5	0.004	0.012	2.254	2.739	9.026	2.224	0.050	0.048	0.413
6	0.066	0.182	2.509	4.164	11.013	2.871	0.079	0.082	1.172
7	0.040	0.303	3.046	6.031	16.366	3.781	0.155	0.144	0.385
8	4.307	7.497	4.943	11.565	29.411	6.256	0.460	0.449	1.617
9	0.251	0.460	3.312	6.808	19.810	4.592	0.227	0.177	0.979
10	0.109	0.209	4.469	5.198	17.058	4.553	0.194	0.182	1.006
11	0.020	0.064	2.612	4.202	11.337	3.013	0.085	0.086	0.710
12	0.010	0.027	1.673	2.354	6.665	1.998	0.033	0.031	1.238
13	0.005	0.017	2.558	3.184	9.667	2.606	0.063	0.064	0.377
14	0.017	0.047	2.537	3.163	9.173	2.730	0.063	0.063	0.845
15	0.156	0.357	3.105	3.630	11.718	3.059	0.090	0.089	1.984
16	0.496	1.498	3.688	7.971	23.076	4.837	0.279	0.231	1.062
17	0.097	0.211	3.514	3.858	12.669	3.425	0.108	0.106	1.402
18	0.015	0.045	2.234	2.843	9.386	2.324	0.055	0.050	0.937
19	0.015	0.041	3.000	3.715	10.778	2.970	0.080	0.088	0.565
20	0.007	0.023	2.662	3.378	11.376	2.694	0.077	0.071	0.423
21	0.010	0.071	2.885	4.088	12.580	3.113	0.098	0.093	0.312
22	0.020	0.067	2.674	3.641	10.202	2.743	0.070	0.076	0.774
23	0.005	0.009	1.941	2.438	8.082	2.096	0.042	0.037	0.530
24	0.094	0.349	2.932	3.509	10.841	3.047	0.083	0.081	2.044
25	0.042	0.130	2.598	4.490	11.942	3.133	0.094	0.092	0.946
26	0.044	0.182	1.604	2.311	6.687	1.877	0.031	0.029	2.104
27	0.049	0.119	2.818	3.448	10.414	2.988	0.078	0.076	1.158
28	0.112	0.295	4.647	5.228	18.128	4.607	0.209	0.191	0.834
29	1.181	5.512	3.626	7.662	19.509	4.543	0.222	0.218	2.164
30	0.078	0.239	2.966	3.629	11.960	2.882	0.086	0.085	1.665
31	0.016	0.040	2.054	2.604	8.405	2.090	0.044	0.042	1.193
32	0.133	0.264	3.526	4.008	13.454	3.419	0.115	0.111	1.572
33	0.023	0.103	2.488	4.181	11.759	2.758	0.081	0.082	0.733
34	0.028	0.187	3.376	6.094	16.842	4.360	0.184	0.162	0.395
35	0.003	0.010	2.058	2.628	8.482	2.109	0.045	0.042	0.422
36	0.060	0.169	2.876	3.210	9.865	3.022	0.075	0.072	1.979
37	0.041	0.092	2.534	4.791	13.958	3.151	0.110	0.095	0.683
38	0.051	0.118	3.367	4.437	14.181	3.586	0.127	0.117	0.909
39	0.323	0.545	4.747	9.608	24.939	5.860	0.365	0.358	0.651
40	0.424	0.811	2.828	4.463	12.938	3.306	0.107	0.099	2.356
41	0.315	0.524	3.432	4.980	14.519	3.980	0.144	0.134	1.701
42	0.066	0.176	2.482	3.060	9.082	2.609	0.059	0.060	1.963
43	0.108	0.279	2.829	4.298	13.230	3.376	0.112	0.095	1.206
44	0.639	2.114	4.957	9.395	25.968	6.032	0.392	0.366	1.109
45	0.148	0.424	3.121	3.948	11.926	3.295	0.098	0.097	2.209
46	0.221	0.393	3.803	6.053	18.164	4.583	0.208	0.181	1.031
47	0.009	0.021	1.782	2.158	6.541	1.799	0.029	0.030	0.933
48	0.077	0.178	3.345	4.520	13.440	3.752	0.126	0.119	1.234
49	0.001	0.003	1.249	1.627	4.931	1.263	0.016	0.016	0.420
50	0.001	0.002	1.171	1.571	5.218	1.191	0.016	0.014	0.365
51	0.025	0.056	2.550	2.828	9.049	2.602	0.059	0.057	1.291
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2	0.003	0.008	1.614	2.232	6.529	1.706	0.028	0.028	0.544
3	0.004	0.008	2.024	2.328	7.829	1.956	0.038	0.037	0.595
4	0.152	0.463	3.752	6.083	20.202	4.746	0.240	0.179	0.764
5	0.110	0.280	3.307	5.198	14.592	3.553	0.130	0.135	1.248
6	0.074	0.206	2.337	3.921	10.721	2.726	0.073	0.072	1.265
7	0.054	0.145	3.253	4.288	12.309	3.606	0.111	0.110	0.924
8	0.130	0.248	3.443	4.427	13.709	3.601	0.123	0.120	1.325
9	0.020	0.057	2.337	2.977	8.842	2.448	0.054	0.055	1.207
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11	0.875	1.999	5.504	11.272	31.139	6.996	0.545	0.487	0.882
12	0.025	0.094	2.229	5.284	13.469	2.867	0.097	0.093	0.481
13	0.033	0.056	2.807	3.647	10.997	2.972	0.082	0.080	0.984
14	0.058	0.183	3.309	4.297	13.094	3.291	0.108	0.112	1.192
15	0.230	0.762	4.694	6.020	17.946	5.054	0.227	0.222	1.171
16	0.006	0.021	2.550	3.222	9.787	2.806	0.069	0.065	0.377
17	0.008	0.022	2.539	3.357	10.019	2.758	0.069	0.067	0.526
18	0.006	0.012	1.792	2.444	7.653	2.150	0.041	0.034	0.834
19	0.051	0.155	2.582	3.108	9.392	2.699	0.063	0.063	1.671
20	0.027	0.052	2.791	3.230	9.826	2.820	0.069	0.071	1.005
21	0.078	0.135	3.086	3.614	10.669	3.209	0.086	0.088	1.562
22	0.018	0.041	2.968	3.431	10.338	2.993	0.077	0.080	0.871
23	0.025	0.041	2.996	3.439	10.693	3.209	0.086	0.081	0.826
24	0.080	0.247	3.390	4.303	13.330	3.390	0.113	0.115	1.321
25	0.006	0.011	1.980	2.183	6.667	2.038	0.034	0.034	0.957
26	0.013	0.024	1.860	2.600	7.731	1.939	0.037	0.038	0.960
27	0.057	0.177	1.771	2.520	7.349	2.020	0.037	0.035	1.909
28	0.034	0.101	2.142	2.834	8.480	2.306	0.049	0.048	1.758
29	0.030	0.104	2.525	3.927	10.784	2.783	0.075	0.078	0.972
30	0.031	0.079	2.552	3.426	10.614	2.776	0.074	0.069	0.998
31	0.058	0.230	2.391	2.810	8.625	2.316	0.050	0.053	1.969
32	0.019	0.039	3.067	3.601	11.501	3.064	0.088	0.087	0.793
33	0.036	0.108	0.981	1.591	4.414	1.106	0.012	0.012	2.888
34	0.043	0.091	3.448	4.293	13.109	3.606	0.118	0.116	0.848
35	0.027	0.068	2.188	3.205	9.355	2.372	0.055	0.055	1.086
36	0.204	0.441	4.669	5.375	16.745	4.748	0.199	0.197	1.128
37	0.145	0.259	2.815	3.184	10.027	2.889	0.072	0.070	2.243
38	0.079	0.196	3.412	3.903	11.686	3.419	0.100	0.105	1.424
39	1.014	2.041	6.801	10.575	28.975	7.694	0.557	0.565	1.066
40	0.016	0.073	1.988	2.577	7.813	2.160	0.042	0.040	1.274
41	0.022	0.082	2.507	3.337	10.511	2.750	0.072	0.066	0.695
42	0.056	0.146	3.141	3.432	11.178	3.152	0.088	0.085	1.217
43	0.034	0.085	2.409	3.774	10.852	2.821	0.077	0.071	0.845
44	0.026	0.050	2.316	2.781	8.572	2.264	0.049	0.051	1.334
45	0.040	0.098	2.113	2.553	7.909	2.222	0.044	0.042	1.627
46	0.014	0.067	1.016	1.949	4.922	1.111	0.014	0.016	1.743
47	0.071	0.245	2.801	3.116	10.051	2.771	0.070	0.069	2.029
48	0.005	0.014	1.964	2.682	8.337	2.070	0.043	0.041	0.565
49	0.056	0.155	3.187	3.553	11.772	3.139	0.092	0.089	1.483
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aspect	ratio	bottleneck	bulge	locat	nonsperic	aneurysm	vaneurysm	sundulation	ellipticity	ir	mean of m
eAR	BF	BL	NSI	AVSV	AASA	UI	EI	MAA	mm ⁻¹		
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5	1.625	1.471	0.153	0.270	0.485	0.671	0.079	0.240	0.318		
6	2.417	2.012	0.364	0.370	0.285	0.545	0.277	0.271	0.254		
7	1.534	1.000	0.052	0.311	0.311	0.529	0.101	0.282	0.322		
8	1.811	1.836	0.626	0.278	0.370	0.567	0.077	0.255	0.302		
9	1.739	1.358	0.340	0.270	0.390	0.580	0.023	0.264	0.325		
10	0.657	1.101	0.202	0.249	0.549	0.709	0.034	0.237	0.322		
11	2.499	2.064	0.491	0.257	0.555	0.721	0.045	0.234	0.090		
12	1.115	1.117	0.351	0.254	0.478	0.650	0.043	0.240	0.324		
13	0.821	1.004	0.019	0.258	0.555	0.723	0.037	0.247	0.308		
14	1.490	1.649	0.475	0.279	0.407	0.605	0.046	0.267	0.354		
15	1.441	1.113	0.499	0.236	0.639	0.770	0.018	0.231	0.239		
16	2.401	2.536	0.414	0.304	0.261	0.465	0.077	0.284	0.259		
17	1.644	1.768	0.543	0.249	0.431	0.603	0.027	0.240	0.216		
18	0.531	1.148	0.113	0.299	0.285	0.491	0.079	0.275	0.356		
19	0.805	1.000	0.010	0.291	0.460	0.667	0.039	0.276	0.401		
20	2.082	1.729	0.453	0.261	0.396	0.579	0.073	0.245	0.185		
21	0.798	1.000	0.031	0.289	0.441	0.647	0.037	0.277	0.666		
22	2.164	1.847	0.528	0.267	0.459	0.644	0.047	0.251	0.163		
23	1.052	1.172	0.466	0.239	0.628	0.766	0.017	0.233	0.524		
24	1.452	1.214	0.464	0.260	0.454	0.633	0.029	0.251	0.389		
25	1.513	1.531	0.674	0.275	0.390	0.584	0.074	0.252	0.292		
26	1.214	1.180	0.285	0.266	0.562	0.737	0.054	0.248	0.315		
27	1.924	1.583	0.324	0.243	0.494	0.655	0.022	0.235	0.179		
28	0.997	1.153	0.390	0.278	0.354	0.550	0.034	0.266	0.283		
29	1.402	1.454	0.443	0.226	0.748	0.845	0.016	0.220	0.200		
30	0.802	0.986	0.424	0.286	0.396	0.600	0.079	0.259	0.239		
31	0.701	0.998	0.026	0.297	0.377	0.589	0.080	0.272	0.357		
32	0.874	0.993	0.153	0.232	0.680	0.799	0.016	0.226	0.132		
33	1.016	1.204	0.520	0.299	0.349	0.561	0.112	0.264	0.321		
34	0.985	1.417	0.453	0.271	0.385	0.577	0.053	0.253	0.303		
35	1.330	1.958	0.536	0.354	0.188	0.404	0.204	0.300	0.317		
36	2.226	1.674	0.290	0.322	0.275	0.496	0.119	0.276	0.176		
37	1.023	1.178	0.492	0.254	0.522	0.690	0.024	0.245	0.337		
38	0.787	1.281	0.383	0.279	0.344	0.540	0.066	0.257	0.354		
39	1.444	1.163	0.261	0.307	0.277	0.486	0.099	0.278	0.371		
40	0.897	1.049	0.432	0.258	0.539	0.709	0.039	0.243	0.499		
41	1.353	1.145	0.347	0.266	0.404	0.591	0.042	0.253	0.325		
42	0.998	1.361	0.313	0.263	0.473	0.654	0.055	0.246	0.271		
43	1.134	1.112	0.234	0.247	0.595	0.746	0.033	0.231	0.128		
44	1.358	1.027	0.320	0.288	0.400	0.605	0.087	0.256	0.284		
45	0.780	1.024	0.204	0.259	0.578	0.743	0.032	0.248	0.335		
46	2.421	1.532	0.475	0.270	0.351	0.541	0.036	0.259	0.193		
47	3.215	1.713	0.478	0.224	0.662	0.777	0.012	0.220	0.088		
48	1.163	1.378	0.409	0.268	0.413	0.601	0.055	0.254	0.274		
49	1.594	2.251	0.194	0.327	0.241	0.456	0.136	0.277	0.212		
50	1.202	1.308	0.446	0.255	0.413	0.591	0.032	0.242	0.336		
51	2.428	1.802	0.503	0.242	0.588	0.734	0.027	0.232	0.135		
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2	1.036	0.977	0.145	0.297	0.405	0.618	0.109	0.264	0.331
3	1.215	1.183	0.417	0.254	0.499	0.669	0.022	0.244	0.258
4	0.651	1.059	0.327	0.319	0.256	0.470	0.037	0.304	0.154
5	0.920	1.169	0.349	0.271	0.352	0.543	0.052	0.257	0.345
6	0.581	1.000	0.015	0.318	0.415	0.647	0.050	0.301	0.368
7	1.233	1.019	0.561	0.280	0.437	0.635	0.069	0.258	0.435
8	0.527	1.000	0.154	0.309	0.456	0.680	0.067	0.284	0.343
9	2.223	1.872	0.519	0.236	0.528	0.679	0.019	0.229	0.169
10	1.037	1.000	0.024	0.329	0.323	0.556	0.099	0.287	0.313
11	0.555	1.091	0.219	0.279	0.399	0.596	0.047	0.265	0.413
12	3.305	1.703	0.484	0.262	0.382	0.566	0.041	0.252	0.142
13	1.927	2.168	0.604	0.306	0.347	0.565	0.145	0.256	0.232
14	1.149	1.205	0.410	0.246	0.503	0.666	0.026	0.237	0.314
15	0.890	1.187	0.333	0.238	0.559	0.706	0.019	0.231	0.494
16	1.757	2.633	0.381	0.268	0.380	0.569	0.049	0.251	0.223
17	1.063	1.000	0.054	0.332	0.264	0.489	0.126	0.292	0.373
18	0.666	0.999	0.185	0.282	0.488	0.685	0.059	0.262	0.302
19	0.626	1.000	0.072	0.336	0.313	0.550	0.102	0.301	0.437
20	0.698	1.278	0.503	0.299	0.383	0.597	0.104	0.257	0.391
21	1.850	1.899	0.554	0.259	0.479	0.656	0.059	0.239	0.432
22	1.374	2.359	0.431	0.279	0.312	0.506	0.047	0.264	0.285
23	0.700	1.000	0.077	0.267	0.568	0.742	0.027	0.255	0.443
24	1.534	1.155	0.439	0.242	0.569	0.719	0.027	0.233	0.261
25	0.590	0.998	0.009	0.309	0.405	0.630	0.084	0.281	0.578
26	0.653	1.067	0.304	0.284	0.437	0.638	0.025	0.274	0.355
27	1.043	1.303	0.312	0.347	0.290	0.533	0.202	0.281	0.330
28	1.137	1.351	0.350	0.262	0.379	0.563	0.031	0.253	0.321
29	1.279	1.434	0.449	0.258	0.453	0.630	0.051	0.244	0.176
30	0.850	0.997	0.026	0.264	0.531	0.708	0.044	0.248	0.397
31	2.714	1.699	0.589	0.288	0.251	0.443	0.067	0.270	0.220
32	1.361	1.480	0.572	0.244	0.470	0.635	0.018	0.238	0.367
33	1.509	1.147	0.305	0.255	0.420	0.597	0.025	0.247	0.326
34	2.705	2.766	0.544	0.245	0.488	0.652	0.027	0.235	0.119
35	1.056	1.184	0.275	0.268	0.505	0.688	0.068	0.237	0.167
36	0.951	0.962	0.134	0.271	0.346	0.537	0.041	0.258	0.334
37	0.957	1.203	0.325	0.298	0.388	0.602	0.103	0.263	0.331
38	0.547	0.970	0.043	0.307	0.353	0.572	0.072	0.283	0.258
39	2.558	2.061	0.539	0.335	0.221	0.436	0.163	0.293	0.213
40	0.738	0.964	0.338	0.238	0.616	0.754	0.029	0.228	0.320
41	1.018	0.996	0.078	0.276	0.444	0.639	0.063	0.252	0.293
42	1.601	1.728	0.463	0.272	0.366	0.558	0.059	0.250	0.157
43	0.902	0.999	0.139	0.280	0.526	0.718	0.069	0.254	0.354
44	2.623	1.546	0.263	0.339	0.185	0.389	0.152	0.296	0.310
45	0.398	0.991	0.076	0.300	0.349	0.562	0.070	0.277	0.298
46	0.561	1.013	0.325	0.291	0.396	0.605	0.081	0.264	0.374
47	1.690	1.350	0.455	0.324	0.203	0.405	0.088	0.304	0.462
48	1.328	1.691	0.552	0.279	0.413	0.610	0.078	0.251	0.273
49	1.649	1.000	0.110	0.263	0.403	0.588	0.033	0.255	0.148
50	0.979	1.218	0.257	0.267	0.457	0.642	0.070	0.248	0.296
51	1.853	1.713	0.549	0.256	0.488	0.661	0.045	0.239	0.181
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2	2.281	1.444	0.689	0.298	0.324	0.534	0.091	0.270	0.297
3	3.872	1.683	0.422	0.260	0.511	0.685	0.052	0.231	0.073
4	0.694	1.000	0.050	0.295	0.436	0.647	0.057	0.271	0.532
5	1.031	1.009	0.069	0.257	0.417	0.597	0.009	0.255	0.456
6	0.485	1.000	0.001	0.301	0.407	0.623	0.018	0.296	0.593
7	1.480	1.156	0.560	0.275	0.478	0.669	0.091	0.246	0.152
8	1.377	1.384	0.467	0.247	0.545	0.704	0.039	0.232	0.241
9	0.875	0.965	0.010	0.278	0.346	0.542	0.053	0.260	0.393
10	0.689	1.096	0.434	0.238	0.511	0.666	0.017	0.232	0.406
11	0.765	0.994	0.048	0.262	0.556	0.727	0.021	0.253	0.494
12	1.398	1.116	0.237	0.278	0.416	0.613	0.051	0.261	0.401
13	0.661	0.999	0.114	0.313	0.276	0.490	0.059	0.295	0.631
14	0.860	1.185	0.206	0.270	0.375	0.565	0.042	0.255	0.565
15	1.009	0.969	0.008	0.325	0.315	0.545	0.115	0.294	0.283
16	0.998	1.142	0.263	0.277	0.406	0.602	0.047	0.259	0.353
17	1.456	1.326	0.441	0.227	0.614	0.742	0.012	0.222	0.274
18	0.952	1.314	0.224	0.280	0.395	0.593	0.070	0.253	0.198
19	1.590	1.708	0.279	0.336	0.343	0.586	0.158	0.260	0.163
20	1.980	1.982	0.453	0.229	0.559	0.699	0.010	0.226	0.088
21	1.291	1.403	0.357	0.271	0.343	0.533	0.037	0.258	0.286
22	0.730	1.334	0.118	0.365	0.283	0.538	0.170	0.299	0.230
23	0.375	1.000	0.059	0.449	0.195	0.484	0.115	0.409	0.320
24	0.924	1.092	0.359	0.251	0.584	0.740	0.016	0.244	0.268
25	2.164	1.461	0.559	0.277	0.342	0.538	0.060	0.263	0.453
26	0.864	1.229	0.217	0.241	0.495	0.654	0.016	0.236	0.243
27	1.259	2.051	0.108	0.277	0.285	0.476	0.041	0.263	0.182
28	0.767	1.023	0.225	0.293	0.487	0.695	0.054	0.271	0.483
29	2.097	2.949	0.546	0.395	0.229	0.491	0.282	0.285	0.215
30	0.796	1.018	0.284	0.285	0.471	0.672	0.044	0.267	0.482
31	0.613	1.000	0.040	0.335	0.390	0.637	0.134	0.277	0.535
32	1.273	1.147	0.315	0.288	0.328	0.530	0.064	0.268	0.354
33	1.722	1.509	0.519	0.283	0.401	0.602	0.072	0.256	0.303
34	2.094	1.054	0.310	0.272	0.512	0.698	0.064	0.230	0.254
35	0.503	1.009	0.204	0.303	0.218	0.413	0.069	0.288	0.174
36	2.034	1.750	0.499	0.327	0.273	0.496	0.148	0.275	0.304
37	1.712	1.261	0.377	0.364	0.247	0.492	0.205	0.283	0.281
38	1.711	1.227	0.332	0.334	0.285	0.516	0.172	0.271	0.255
39	0.827	1.121	0.175	0.298	0.379	0.592	0.071	0.272	0.346
40	2.496	2.359	0.471	0.236	0.555	0.702	0.021	0.229	0.137
41	2.173	1.152	0.520	0.280	0.296	0.489	0.061	0.260	0.138
42	1.053	1.060	0.327	0.241	0.584	0.730	0.029	0.230	0.197
43	1.015	1.152	0.472	0.264	0.475	0.657	0.052	0.243	0.184
44	1.953	1.081	0.491	0.267	0.382	0.570	0.046	0.258	0.206
45	1.232	1.346	0.387	0.231	0.633	0.761	0.013	0.227	0.245
46	0.624	0.994	0.101	0.300	0.390	0.606	0.056	0.281	0.278
47	1.404	1.529	0.477	0.289	0.388	0.594	0.095	0.258	0.401
48	0.669	1.000	0.086	0.317	0.389	0.619	0.083	0.295	0.974
49	1.076	1.550	0.450	0.282	0.363	0.562	0.090	0.253	0.328
50	0.472	0.969	0.129	0.365	0.268	0.520	0.154	0.315	0.791
51	1.586	1.369	0.274	0.262	0.507	0.684	0.060	0.238	0.198
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2	1.054	1.201	0.355	0.310	0.384	0.608	0.117	0.267	0.349
3	1.453	1.452	0.652	0.279	0.363	0.561	0.078	0.254	0.339
4	1.412	1.316	0.338	0.345	0.316	0.563	0.180	0.278	0.418
5	0.509	0.985	0.000	0.415	0.237	0.520	0.241	0.341	0.717
6	1.700	1.489	0.626	0.290	0.329	0.532	0.091	0.265	0.359
7	0.615	1.352	0.249	0.387	0.104	0.287	0.215	0.329	0.418
8	2.990	1.941	0.524	0.242	0.556	0.709	0.032	0.227	0.092
9	1.452	1.358	0.550	0.269	0.507	0.691	0.070	0.243	0.237
10	1.149	1.250	0.248	0.317	0.447	0.680	0.142	0.259	0.296
11	0.990	1.009	0.242	0.339	0.281	0.514	0.113	0.296	0.459
12	1.459	1.117	0.411	0.319	0.310	0.533	0.146	0.276	0.646
13	0.461	0.915	0.154	0.420	0.217	0.495	0.213	0.349	0.588
14	0.979	1.289	0.449	0.293	0.344	0.552	0.055	0.274	0.566
15	2.355	1.916	0.548	0.264	0.415	0.599	0.051	0.247	0.269
16	1.750	1.650	0.095	0.378	0.242	0.495	0.270	0.279	0.226
17	1.580	1.845	0.205	0.313	0.394	0.622	0.141	0.263	0.347
18	1.146	1.285	0.421	0.284	0.318	0.516	0.080	0.254	0.594
19	0.706	1.000	0.010	0.303	0.334	0.548	0.075	0.282	0.538
20	0.530	1.000	0.157	0.402	0.233	0.503	0.195	0.355	0.507
21	0.410	1.061	0.241	0.443	0.113	0.333	0.239	0.370	0.537
22	1.027	1.194	0.485	0.299	0.280	0.485	0.078	0.273	0.501
23	0.617	1.045	0.099	0.340	0.394	0.647	0.200	0.262	0.841
24	2.354	1.474	0.312	0.305	0.248	0.451	0.079	0.280	0.315
25	1.355	1.113	0.287	0.305	0.291	0.501	0.098	0.269	0.398
26	2.590	2.710	0.626	0.371	0.190	0.417	0.218	0.305	0.462
27	1.336	1.605	0.479	0.265	0.392	0.579	0.050	0.246	0.397
28	0.946	1.511	0.221	0.295	0.336	0.544	0.118	0.249	0.289
29	3.649	1.959	0.320	0.326	0.199	0.401	0.074	0.305	0.151
30	2.097	1.414	0.346	0.366	0.243	0.487	0.261	0.285	0.355
31	1.486	1.127	0.438	0.271	0.360	0.551	0.091	0.247	0.546
32	1.842	1.648	0.293	0.274	0.465	0.656	0.076	0.247	0.279
33	1.112	0.957	0.276	0.323	0.186	0.382	0.159	0.290	0.471
34	0.552	0.987	0.043	0.396	0.123	0.326	0.180	0.344	0.392
35	0.526	0.996	0.113	0.357	0.279	0.527	0.180	0.317	0.764
36	2.102	1.299	0.521	0.280	0.343	0.540	0.042	0.268	0.364
37	1.039	1.074	0.564	0.284	0.403	0.605	0.100	0.246	0.419
38	1.125	1.149	0.251	0.288	0.390	0.595	0.102	0.251	0.378
39	1.068	1.010	0.476	0.279	0.533	0.725	0.101	0.237	0.207
40	3.180	2.032	0.487	0.236	0.514	0.666	0.017	0.229	0.207
41	2.128	1.947	0.420	0.240	0.584	0.730	0.029	0.230	0.211
42	2.303	1.525	0.379	0.275	0.350	0.544	0.072	0.252	0.354
43	1.536	1.691	0.692	0.313	0.333	0.554	0.138	0.256	0.331
44	1.728	1.239	0.351	0.339	0.242	0.466	0.201	0.274	0.189
45	2.647	1.653	0.685	0.319	0.299	0.522	0.142	0.279	0.284
46	1.362	1.469	0.396	0.257	0.529	0.699	0.059	0.233	0.244
47	1.119	1.538	0.595	0.288	0.384	0.589	0.086	0.261	0.685
48	1.487	1.206	0.279	0.306	0.371	0.590	0.138	0.259	0.331
49	0.542	0.946	0.453	0.346	0.283	0.523	0.186	0.289	1.245
50	0.481	0.962	0.216	0.379	0.260	0.520	0.222	0.310	1.290
51	1.403	1.314	0.236	0.291	0.404	0.612	0.096	0.258	0.498
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2	0.711	0.977	0.072	0.350	0.270	0.510	0.175	0.286	0.960
3	0.708	0.998	0.033	0.322	0.406	0.642	0.142	0.283	0.778
4	0.980	1.519	0.420	0.333	0.277	0.506	0.154	0.261	0.273
5	1.826	1.137	0.564	0.281	0.356	0.554	0.090	0.257	0.286
6	1.820	1.472	0.417	0.290	0.323	0.526	0.097	0.255	0.339
7	1.099	1.472	0.213	0.286	0.359	0.562	0.041	0.272	0.360
8	1.629	1.712	0.402	0.277	0.472	0.665	0.101	0.240	0.288
9	1.468	1.378	0.359	0.288	0.330	0.533	0.071	0.266	0.513
10	1.421	1.272	0.704	0.270	0.405	0.595	0.075	0.243	0.158
11	0.887	1.004	0.010	0.354	0.222	0.450	0.172	0.290	0.503
12	1.207	1.141	0.506	0.268	0.543	0.721	0.073	0.241	0.427
13	1.556	1.359	0.236	0.324	0.270	0.490	0.155	0.284	0.360
14	1.395	1.551	0.291	0.282	0.286	0.480	0.051	0.264	0.222
15	0.432	0.970	0.141	0.391	0.247	0.513	0.180	0.323	0.548
16	0.640	1.000	0.066	0.355	0.317	0.572	0.129	0.310	0.553
17	0.948	0.993	0.061	0.298	0.422	0.637	0.094	0.267	0.685
18	1.924	1.521	0.592	0.274	0.314	0.505	0.048	0.261	0.385
19	1.151	1.409	0.443	0.276	0.489	0.680	0.078	0.251	0.443
20	1.759	1.666	0.358	0.272	0.542	0.725	0.062	0.245	0.330
21	0.999	1.000	0.060	0.308	0.387	0.610	0.109	0.270	0.463
22	0.886	1.166	0.485	0.265	0.569	0.741	0.067	0.240	0.439
23	1.677	1.400	0.378	0.369	0.242	0.489	0.251	0.278	0.358
24	1.025	1.064	0.274	0.260	0.532	0.704	0.026	0.252	0.717
25	1.287	1.313	0.633	0.284	0.481	0.681	0.112	0.248	0.603
26	2.382	2.568	0.604	0.321	0.273	0.492	0.156	0.268	0.404
27	2.160	1.506	0.348	0.320	0.298	0.521	0.102	0.286	0.439
28	1.372	1.184	0.514	0.395	0.198	0.446	0.325	0.294	0.524
29	1.231	1.411	0.288	0.294	0.349	0.557	0.099	0.256	0.453
30	2.389	1.586	0.667	0.295	0.232	0.425	0.075	0.276	0.374
31	0.932	0.994	0.365	0.305	0.434	0.655	0.102	0.272	0.483
32	4.155	2.651	0.700	0.325	0.284	0.507	0.137	0.272	0.473
33	1.009	1.166	0.421	0.266	0.454	0.639	0.044	0.252	0.377
34	1.468	1.390	0.440	0.274	0.372	0.565	0.063	0.254	0.475
35	1.277	1.687	0.423	0.265	0.432	0.618	0.063	0.242	0.231
36	2.472	2.341	0.557	0.254	0.537	0.702	0.046	0.239	0.274
37	1.625	1.394	0.333	0.295	0.358	0.568	0.111	0.263	0.329
38	1.466	1.326	0.386	0.250	0.478	0.647	0.037	0.235	0.142
39	1.520	1.268	0.547	0.363	0.169	0.381	0.221	0.303	0.600
40	0.843	1.420	0.333	0.352	0.220	0.447	0.171	0.290	0.536
41	1.325	1.726	0.471	0.302	0.340	0.554	0.113	0.265	0.381
42	1.130	1.404	0.483	0.289	0.371	0.576	0.088	0.261	0.405
43	1.639	1.526	0.331	0.261	0.497	0.674	0.048	0.244	0.474
44	1.870	2.178	0.437	0.320	0.344	0.573	0.168	0.262	0.442
45	3.059	1.575	0.476	0.309	0.176	0.361	0.142	0.289	0.651
46	2.282	1.516	0.635	0.300	0.269	0.472	0.077	0.275	0.360
47	0.732	0.995	0.012	0.324	0.313	0.541	0.148	0.286	0.680
48	1.679	1.311	0.233	0.310	0.313	0.530	0.136	0.269	0.383
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	absMAA	MSD	HMC	MLN	GAA	absGAA	GSD	HGC	GLN
	mm ⁻¹	mm ⁻¹	%	-	mm ⁻²	mm ⁻²	mm ⁻²	%	-
5	0.370	0.303	27.483	0.329	0.069	0.227	0.376	170.270	2.699
6	0.328	0.307	99.650	0.491	0.034	0.179	0.308	561.209	5.898
7	0.382	0.330	39.608	0.316	0.048	0.220	0.383	193.206	2.283
8	0.343	0.255	35.989	0.317	0.050	0.192	0.287	202.369	2.361
9	0.337	0.247	25.724	0.306	0.081	0.152	0.244	111.783	1.818
10	0.348	0.234	10.601	0.264	0.090	0.155	0.217	56.300	1.293
11	0.140	0.155	68.740	0.506	0.006	0.030	0.072	337.335	7.205
12	0.379	0.315	27.518	0.311	0.080	0.199	0.306	125.715	1.876
13	0.325	0.237	-4.035	0.233	0.076	0.159	0.256	38.871	1.205
14	0.376	0.331	22.618	0.325	0.092	0.203	0.412	115.984	2.393
15	0.248	0.178	7.167	0.294	0.047	0.083	0.136	54.474	1.768
16	0.294	0.242	65.689	0.374	0.041	0.130	0.235	310.560	3.334
17	0.232	0.170	32.321	0.326	0.042	0.071	0.102	131.248	1.942
18	0.380	0.249	39.230	0.262	0.102	0.203	0.260	172.089	1.276
19	0.404	0.211	-2.756	0.215	0.132	0.193	0.229	12.202	0.746
20	0.215	0.197	46.687	0.382	0.024	0.082	0.158	281.687	4.003
21	0.671	0.414	-0.486	0.222	0.361	0.563	0.758	23.583	0.845
22	0.199	0.192	44.389	0.398	0.020	0.063	0.127	232.352	4.009
23	0.543	0.286	2.134	0.252	0.241	0.363	0.400	28.454	1.043
24	0.399	0.190	13.360	0.256	0.120	0.191	0.207	54.113	1.056
25	0.307	0.212	21.546	0.290	0.053	0.152	0.204	138.982	1.721
26	0.340	0.239	10.459	0.284	0.081	0.165	0.226	74.818	1.560
27	0.203	0.158	28.289	0.329	0.028	0.056	0.096	122.201	2.377
28	0.315	0.227	33.131	0.287	0.073	0.131	0.186	133.613	1.570
29	0.216	0.119	3.469	0.271	0.036	0.056	0.064	27.970	1.247
30	0.271	0.231	16.426	0.271	0.038	0.130	0.217	140.469	1.842
31	0.382	0.264	-3.851	0.197	0.096	0.246	0.282	55.765	0.735
32	0.140	0.088	2.641	0.257	0.016	0.025	0.033	36.799	1.203
33	0.387	0.372	50.037	0.365	0.077	0.284	0.468	327.761	3.296
34	0.333	0.246	41.619	0.324	0.085	0.154	0.209	177.817	1.951
35	0.354	0.270	84.214	0.364	0.055	0.217	0.303	487.876	2.950
36	0.237	0.244	86.955	0.450	0.019	0.087	0.200	441.938	5.629
37	0.371	0.235	13.847	0.266	0.100	0.161	0.201	51.703	1.185
38	0.439	0.399	46.462	0.326	0.087	0.306	0.492	240.832	2.349
39	0.407	0.281	37.388	0.281	0.076	0.231	0.343	163.135	1.613
40	0.570	0.384	4.723	0.241	0.184	0.475	0.580	60.221	1.122
41	0.362	0.272	20.362	0.280	0.081	0.167	0.275	85.294	1.573
42	0.308	0.246	27.931	0.317	0.060	0.144	0.226	147.719	2.208
43	0.164	0.148	40.176	0.378	0.015	0.033	0.059	142.546	2.862
44	0.343	0.312	37.421	0.341	0.048	0.213	0.351	242.425	2.908
45	0.387	0.269	3.259	0.237	0.098	0.204	0.253	45.488	1.042
46	0.226	0.209	46.111	0.364	0.027	0.073	0.137	206.103	2.868
47	0.096	0.068	19.469	0.339	0.007	0.012	0.020	92.486	2.471
48	0.289	0.212	30.106	0.314	0.061	0.121	0.182	145.513	1.983
49	0.281	0.269	107.395	0.461	0.030	0.133	0.249	629.400	5.743
50	0.393	0.319	32.247	0.311	0.093	0.194	0.294	119.328	1.750
51	0.165	0.153	31.289	0.381	0.015	0.037	0.066	136.383	2.960

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2	0.350	0.247	13.398	0.258	0.070	0.203	0.269	112.222	1.370
3	0.287	0.208	15.684	0.280	0.052	0.102	0.226	66.441	2.078
4	0.182	0.175	57.716	0.334	0.022	0.042	0.081	218.754	2.151
5	0.356	0.234	30.075	0.275	0.096	0.198	0.247	164.159	1.450
6	0.388	0.259	-7.566	0.195	0.122	0.195	0.277	10.566	0.715
7	0.460	0.300	6.766	0.251	0.122	0.315	0.390	69.545	1.155
8	0.407	0.329	-3.969	0.208	0.118	0.246	0.302	36.806	0.780
9	0.203	0.182	35.467	0.372	0.023	0.063	0.105	179.517	3.037
10	0.419	0.407	48.732	0.337	0.078	0.257	0.381	224.679	2.102
11	0.473	0.333	13.718	0.224	0.139	0.309	0.393	78.607	0.935
12	0.161	0.146	47.887	0.385	0.015	0.043	0.081	264.046	3.689
13	0.278	0.232	61.744	0.390	0.035	0.115	0.193	289.460	3.489
14	0.343	0.232	18.223	0.283	0.082	0.158	0.233	88.126	1.628
15	0.516	0.267	7.079	0.243	0.221	0.329	0.340	41.759	0.958
16	0.275	0.261	54.542	0.398	0.039	0.108	0.207	242.212	3.573
17	0.402	0.312	34.161	0.275	0.096	0.248	0.417	176.386	1.726
18	0.327	0.269	1.580	0.244	0.071	0.179	0.283	72.216	1.339
19	0.523	0.441	13.316	0.229	0.147	0.443	0.626	107.707	1.104
20	0.491	0.422	46.646	0.329	0.120	0.372	0.524	231.396	2.211
21	0.484	0.309	19.917	0.289	0.080	0.373	0.597	129.208	2.242
22	0.318	0.236	50.879	0.336	0.061	0.135	0.240	202.896	2.567
23	0.463	0.263	1.081	0.234	0.180	0.269	0.319	28.479	0.951
24	0.298	0.229	19.650	0.310	0.057	0.120	0.208	94.046	2.157
25	0.601	0.450	-12.547	0.189	0.274	0.589	0.757	24.710	0.673
26	0.368	0.232	16.362	0.257	0.120	0.161	0.209	60.852	1.110
27	0.385	0.324	48.503	0.340	0.063	0.256	0.413	281.276	2.831
28	0.340	0.253	36.700	0.321	0.085	0.162	0.290	161.584	2.334
29	0.205	0.197	40.081	0.374	0.025	0.068	0.150	216.724	3.849
30	0.437	0.302	3.354	0.240	0.136	0.240	0.328	34.409	1.029
31	0.234	0.160	59.080	0.336	0.034	0.082	0.108	276.784	2.173
32	0.374	0.216	17.165	0.279	0.114	0.175	0.261	71.811	1.539
33	0.356	0.235	21.604	0.277	0.073	0.173	0.277	101.693	1.713
34	0.163	0.184	59.477	0.479	0.013	0.047	0.138	347.994	8.316
35	0.268	0.333	43.610	0.421	0.021	0.093	0.193	166.645	3.114
36	0.398	0.341	33.368	0.288	0.094	0.204	0.327	128.610	1.558
37	0.415	0.393	32.874	0.323	0.084	0.229	0.342	134.917	1.756
38	0.320	0.293	-0.625	0.200	0.038	0.168	0.269	62.166	0.895
39	0.255	0.212	83.131	0.388	0.023	0.103	0.163	433.185	3.457
40	0.379	0.308	14.760	0.291	0.088	0.207	0.331	89.730	1.849
41	0.395	0.322	15.166	0.254	0.043	0.241	0.361	105.098	1.550
42	0.201	0.181	48.023	0.352	0.012	0.064	0.109	248.305	2.981
43	0.392	0.291	1.273	0.245	0.094	0.233	0.293	55.595	1.109
44	0.368	0.321	93.888	0.400	0.051	0.203	0.379	462.490	3.849
45	0.350	0.276	20.654	0.231	0.081	0.163	0.223	93.445	0.961
46	0.428	0.351	7.344	0.228	0.100	0.274	0.369	72.784	0.947
47	0.478	0.292	47.932	0.282	0.105	0.283	0.429	171.297	1.482
48	0.348	0.308	47.938	0.367	0.054	0.186	0.289	236.237	2.935
49	0.167	0.145	30.251	0.322	0.010	0.043	0.078	162.837	2.388
50	0.343	0.294	34.369	0.325	0.075	0.203	0.309	211.068	2.415
51	0.234	0.207	30.349	0.335	0.016	0.074	0.146	129.073	2.742
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2	0.310	0.203	40.308	0.321	0.062	0.127	0.156	158.831	1.680
3	0.134	0.159	116.852	0.652	0.004	0.032	0.070	729.119	12.129
4	0.582	0.368	1.515	0.213	0.245	0.414	0.448	25.923	0.694
5	0.456	0.212	15.229	0.243	0.171	0.207	0.272	32.309	0.940
6	0.596	0.330	-4.095	0.194	0.295	0.427	0.550	10.610	0.637
7	0.198	0.195	35.769	0.362	0.010	0.071	0.132	235.187	3.551
8	0.287	0.219	20.911	0.302	0.047	0.113	0.167	100.239	1.872
9	0.442	0.314	19.405	0.241	0.102	0.267	0.354	94.929	1.064
10	0.422	0.250	13.919	0.250	0.164	0.215	0.238	56.828	1.001
11	0.523	0.306	4.891	0.240	0.221	0.313	0.342	26.158	0.871
12	0.462	0.355	30.353	0.311	0.127	0.265	0.410	111.064	1.816
13	0.694	0.535	9.189	0.210	0.239	0.801	1.159	98.527	0.957
14	0.632	0.437	20.122	0.248	0.262	0.507	0.657	83.067	1.073
15	0.287	0.214	18.435	0.266	0.052	0.111	0.229	88.334	1.656
16	0.384	0.290	31.078	0.302	0.114	0.181	0.260	109.950	1.561
17	0.289	0.180	12.421	0.289	0.069	0.095	0.137	43.848	1.499
18	0.240	0.200	49.804	0.341	0.036	0.079	0.118	206.468	2.274
19	0.240	0.234	97.060	0.481	0.018	0.087	0.128	487.833	4.638
20	0.095	0.071	28.605	0.350	0.007	0.012	0.023	123.417	2.849
21	0.302	0.200	35.247	0.296	0.068	0.112	0.147	124.830	1.462
22	0.324	0.338	121.985	0.512	0.040	0.148	0.249	593.122	4.969
23	0.334	0.280	-5.348	0.180	0.085	0.189	0.332	52.250	0.772
24	0.271	0.137	11.424	0.266	0.071	0.080	0.092	34.642	1.143
25	0.472	0.278	31.700	0.294	0.131	0.275	0.419	114.179	1.681
26	0.246	0.119	19.664	0.260	0.058	0.064	0.064	51.720	1.000
27	0.233	0.223	89.689	0.436	0.028	0.080	0.135	433.125	3.965
28	0.534	0.370	0.416	0.228	0.195	0.369	0.501	30.857	0.949
29	0.312	0.312	151.925	0.593	0.026	0.159	0.256	935.858	7.911
30	0.526	0.357	6.666	0.243	0.197	0.375	0.483	54.078	1.073
31	0.559	0.295	4.862	0.210	0.250	0.355	0.369	25.014	0.660
32	0.363	0.233	26.305	0.276	0.093	0.198	0.265	140.458	1.494
33	0.359	0.305	48.969	0.371	0.077	0.185	0.285	219.141	2.764
34	0.335	0.338	54.332	0.440	0.050	0.171	0.468	262.402	6.402
35	0.199	0.168	69.450	0.300	0.016	0.056	0.091	303.266	1.787
36	0.363	0.302	68.165	0.377	0.052	0.219	0.295	369.005	2.910
37	0.349	0.311	83.616	0.408	0.044	0.209	0.311	478.957	3.737
38	0.334	0.316	73.015	0.394	0.042	0.195	0.284	424.433	3.396
39	0.377	0.293	17.496	0.259	0.093	0.191	0.292	85.111	1.259
40	0.154	0.123	31.337	0.360	0.016	0.033	0.058	137.452	2.922
41	0.155	0.120	44.422	0.320	0.010	0.037	0.061	224.235	2.390
42	0.227	0.165	11.027	0.270	0.029	0.076	0.109	80.816	1.565
43	0.255	0.255	33.511	0.334	0.026	0.107	0.171	194.240	2.452
44	0.209	0.129	20.799	0.280	0.026	0.060	0.102	100.045	1.762
45	0.253	0.159	10.847	0.290	0.056	0.080	0.103	53.801	1.446
46	0.317	0.254	9.439	0.232	0.058	0.141	0.240	68.197	1.174
47	0.436	0.318	35.395	0.324	0.115	0.280	0.420	170.562	2.199
48	0.974	0.334	4.159	0.204	0.852	0.945	0.784	8.047	0.571
49	0.372	0.298	35.316	0.314	0.074	0.231	0.414	206.100	2.662
50	0.791	0.300	8.528	0.188	0.627	0.663	0.529	24.912	0.511
51	0.225	0.170	22.277	0.313	0.034	0.068	0.114	101.540	2.151
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2	0.395	0.337	26.292	0.304	0.106	0.215	0.343	119.503	1.779
3	0.345	0.208	27.427	0.291	0.095	0.150	0.229	104.142	1.671
4	0.481	0.370	49.783	0.340	0.141	0.339	0.471	228.326	2.284
5	0.717	0.172	0.717	0.165	0.476	0.494	0.292	-2.452	0.350
6	0.360	0.183	26.541	0.277	0.083	0.154	0.221	89.651	1.407
7	0.420	0.192	75.210	0.252	0.135	0.181	0.207	215.113	0.927
8	0.114	0.110	38.262	0.407	0.008	0.019	0.049	180.146	5.047
9	0.242	0.132	15.827	0.287	0.046	0.076	0.105	73.711	1.611
10	0.363	0.333	33.399	0.348	0.076	0.189	0.303	155.409	2.388
11	0.545	0.457	35.031	0.288	0.193	0.368	0.588	125.531	1.531
12	0.664	0.437	23.027	0.275	0.240	0.730	0.921	150.513	1.489
13	0.589	0.286	-5.813	0.161	0.347	0.429	0.381	9.752	0.395
14	0.568	0.184	26.758	0.252	0.283	0.309	0.258	53.829	0.861
15	0.297	0.218	30.931	0.323	0.053	0.124	0.194	140.585	2.194
16	0.290	0.329	105.626	0.537	0.032	0.148	0.425	646.131	9.678
17	0.393	0.341	45.084	0.379	0.096	0.269	0.401	266.984	3.148
18	0.594	0.180	30.718	0.252	0.316	0.331	0.285	60.140	0.880
19	0.569	0.351	21.800	0.248	0.239	0.421	1.604	92.936	3.043
20	0.523	0.311	-7.988	0.163	0.232	0.306	0.414	-5.200	0.449
21	0.543	0.371	39.201	0.218	0.241	0.362	0.570	137.911	0.872
22	0.546	0.364	37.232	0.277	0.195	0.408	0.621	157.810	1.634
23	0.873	0.447	13.886	0.235	0.691	0.832	0.948	41.574	0.896
24	0.341	0.238	48.851	0.314	0.055	0.157	0.237	200.304	1.940
25	0.440	0.311	38.254	0.292	0.125	0.259	0.359	156.080	1.601
26	0.524	0.447	84.399	0.402	0.138	0.440	0.790	445.200	3.938
27	0.431	0.279	31.785	0.299	0.136	0.222	0.294	107.420	1.554
28	0.362	0.304	49.502	0.326	0.067	0.191	0.295	224.935	2.304
29	0.165	0.136	80.958	0.391	0.015	0.035	0.074	323.417	3.489
30	0.391	0.288	50.280	0.329	0.069	0.237	0.307	251.364	2.052
31	0.551	0.257	16.638	0.248	0.216	0.402	0.423	80.139	1.007
32	0.322	0.285	28.080	0.346	0.058	0.168	0.298	165.452	2.882
33	0.482	0.297	40.044	0.252	0.141	0.354	0.464	199.146	1.251
34	0.407	0.307	44.513	0.228	0.099	0.252	0.444	217.488	1.200
35	0.767	0.275	3.142	0.177	0.594	0.632	0.378	14.077	0.420
36	0.364	0.139	24.614	0.263	0.095	0.133	0.144	56.210	0.992
37	0.425	0.219	19.227	0.263	0.137	0.223	0.314	75.266	1.328
38	0.403	0.274	22.733	0.279	0.113	0.232	0.333	114.462	1.583
39	0.264	0.252	33.935	0.365	0.031	0.116	0.252	198.855	3.979
40	0.223	0.159	28.928	0.341	0.039	0.065	0.143	118.067	3.175
41	0.256	0.244	28.024	0.377	0.031	0.105	0.236	163.323	4.077
42	0.381	0.243	32.272	0.299	0.085	0.197	0.259	138.150	1.661
43	0.385	0.313	55.871	0.369	0.082	0.234	0.360	283.973	3.034
44	0.241	0.245	92.100	0.448	0.020	0.098	0.167	521.985	4.429
45	0.308	0.213	43.675	0.325	0.043	0.134	0.208	190.504	2.243
46	0.276	0.227	25.543	0.336	0.051	0.108	0.209	122.525	2.754
47	0.703	0.413	20.526	0.276	0.370	0.689	0.789	102.406	1.304
48	0.387	0.315	34.960	0.321	0.076	0.237	0.340	188.784	2.155
49	1.246	0.507	5.409	0.190	1.456	1.771	1.521	26.783	0.528
50	1.290	0.436	2.759	0.174	1.617	1.792	1.226	13.602	0.418
51	0.520	0.377	23.268	0.304	0.197	0.380	0.577	113.641	1.815
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2	0.978	0.554	22.089	0.237	0.888	1.297	1.236	102.055	0.872
3	0.793	0.359	-1.413	0.201	0.561	0.741	0.666	14.568	0.599
4	0.371	0.370	78.107	0.406	0.058	0.229	0.371	427.990	3.659
5	0.320	0.265	29.756	0.313	0.050	0.157	0.273	158.021	2.246
6	0.414	0.326	51.809	0.338	0.073	0.248	0.370	232.553	2.444
7	0.395	0.282	28.826	0.291	0.104	0.216	0.310	129.108	1.660
8	0.349	0.308	36.082	0.359	0.061	0.192	0.311	192.483	2.890
9	0.566	0.434	35.500	0.307	0.218	0.438	0.681	150.907	1.871
10	0.201	0.237	57.108	0.454	0.011	0.091	0.499	454.480	15.975
11	0.572	0.377	61.654	0.298	0.184	0.483	0.553	285.505	1.644
12	0.450	0.243	6.697	0.256	0.150	0.274	0.309	54.358	1.170
13	0.423	0.363	49.203	0.329	0.083	0.279	0.447	246.705	2.375
14	0.270	0.257	52.916	0.353	0.041	0.090	0.158	189.102	2.229
15	0.677	0.576	15.981	0.220	0.295	0.543	0.734	59.595	0.760
16	0.615	0.430	6.457	0.213	0.291	0.469	0.609	40.678	0.786
17	0.717	0.438	1.433	0.223	0.383	0.619	0.769	23.782	0.812
18	0.394	0.224	31.241	0.284	0.101	0.197	0.275	118.561	1.495
19	0.501	0.363	15.854	0.284	0.148	0.372	0.510	98.952	1.638
20	0.416	0.481	32.256	0.425	-0.035	0.396	3.326	301.410	22.151
21	0.517	0.364	10.600	0.245	0.156	0.394	0.477	79.837	1.090
22	0.474	0.330	1.492	0.255	0.155	0.349	0.439	60.040	1.264
23	0.443	0.394	72.470	0.383	0.091	0.325	0.686	393.159	4.508
24	0.717	0.244	-0.307	0.223	0.459	0.548	0.439	5.803	0.691
25	0.631	0.386	13.614	0.279	0.315	0.503	0.598	63.297	1.292
26	0.436	0.294	51.879	0.336	0.092	0.240	0.339	190.884	1.993
27	0.492	0.408	42.402	0.337	0.126	0.340	0.542	184.095	2.209
28	0.552	0.458	60.888	0.351	0.111	0.581	0.852	393.852	2.740
29	0.518	0.409	38.234	0.316	0.150	0.401	0.663	185.284	2.293
30	0.418	0.324	58.963	0.335	0.073	0.282	0.490	307.733	2.848
31	0.529	0.450	11.413	0.276	0.194	0.421	0.745	86.600	1.692
32	0.609	0.623	80.026	0.459	0.130	0.591	1.244	415.731	5.422
33	0.409	0.258	14.050	0.259	0.115	0.203	0.303	57.781	1.302
34	0.498	0.281	25.777	0.277	0.205	0.274	0.301	75.337	1.155
35	0.297	0.299	40.100	0.372	0.042	0.133	0.260	195.973	3.215
36	0.297	0.221	17.446	0.320	0.050	0.129	0.218	100.845	2.327
37	0.380	0.315	37.038	0.330	0.069	0.253	0.385	228.068	2.567
38	0.171	0.152	34.278	0.350	0.015	0.043	0.100	163.667	3.608
39	0.611	0.415	58.447	0.307	0.181	0.614	0.818	313.327	1.864
40	0.594	0.462	60.049	0.326	0.204	0.578	0.816	319.459	2.242
41	0.424	0.366	38.583	0.340	0.107	0.296	0.508	215.801	2.702
42	0.486	0.372	32.390	0.297	0.110	0.312	0.450	131.456	1.699
43	0.513	0.295	16.990	0.278	0.186	0.333	0.424	73.202	1.443
44	0.511	0.407	46.090	0.352	0.083	0.447	0.953	264.583	4.138
45	0.653	0.286	64.988	0.297	0.187	0.566	0.711	260.920	1.612
46	0.397	0.269	54.190	0.324	0.089	0.203	0.300	205.775	2.049
47	0.742	0.476	10.353	0.216	0.421	0.637	0.722	40.798	0.712
48	0.478	0.451	59.272	0.379	0.099	0.390	0.685	332.115	3.557
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STROBE Statement—Checklist of items that should be included in reports of *cohort studies*

	Item No	Recommendation	Page No
Title and abstract	1	(a) Indicate the study's design with a commonly used term in the title or the abstract	1
		(b) Provide in the abstract an informative and balanced summary of what was done and what was found	2
Introduction			
Background/rationale	2	Explain the scientific background and rationale for the investigation being reported	3
Objectives	3	State specific objectives, including any prespecified hypotheses	3-4
Methods			
Study design	4	Present key elements of study design early in the paper	5-8
Setting	5	Describe the setting, locations, and relevant dates, including periods of recruitment, exposure, follow-up, and data collection	n.a.
Participants	6	(a) Give the eligibility criteria, and the sources and methods of selection of participants. Describe methods of follow-up (b) For matched studies, give matching criteria and number of exposed and unexposed	n.a.
Variables	7	Clearly define all outcomes, exposures, predictors, potential confounders, and effect modifiers. Give diagnostic criteria, if applicable	6-8
Data sources/ measurement	8*	For each variable of interest, give sources of data and details of methods of assessment (measurement). Describe comparability of assessment methods if there is more than one group	5
Bias	9	Describe any efforts to address potential sources of bias	13
Study size	10	Explain how the study size was arrived at	5
Quantitative variables	11	Explain how quantitative variables were handled in the analyses. If applicable, describe which groupings were chosen and why	6-7
Statistical methods	12	(a) Describe all statistical methods, including those used to control for confounding	8
		(b) Describe any methods used to examine subgroups and interactions	8
		(c) Explain how missing data were addressed	n.a.
		(d) If applicable, explain how loss to follow-up was addressed	n.a.
		(e) Describe any sensitivity analyses	5-8
Results			
Participants	13*	(a) Report numbers of individuals at each stage of study—eg numbers potentially eligible, examined for eligibility, confirmed eligible, included in the study, completing follow-up, and analysed	5
		(b) Give reasons for non-participation at each stage	n.a.
		(c) Consider use of a flow diagram	n.a.
Descriptive data	14*	(a) Give characteristics of study participants (eg demographic, clinical, social) and information on exposures and potential confounders	n.a.
		(b) Indicate number of participants with missing data for each variable of interest	n.a.
		(c) Summarise follow-up time (eg, average and total amount)	n.a.
Outcome data	15*	Report numbers of outcome events or summary measures over time	n.a.

1	Main results	16	(a) Give unadjusted estimates and, if applicable, confounder-adjusted estimates and their precision (eg, 95% confidence interval). Make clear which confounders were adjusted for and why they were included	9-10
2			(b) Report category boundaries when continuous variables were categorized	n.a.
3			(c) If relevant, consider translating estimates of relative risk into absolute risk for a meaningful time period	n.a.
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6	Other analyses	17	Report other analyses done—eg analyses of subgroups and interactions, and sensitivity analyses	9-10
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11	Discussion			
12	Key results	18	Summarise key results with reference to study objectives	11
13	Limitations	19	Discuss limitations of the study, taking into account sources of potential bias or imprecision. Discuss both direction and magnitude of any potential bias	13
14				
15	Interpretation	20	Give a cautious overall interpretation of results considering objectives, limitations, multiplicity of analyses, results from similar studies, and other relevant evidence	13
16				
17	Generalisability	21	Discuss the generalisability (external validity) of the study results	11-12
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21	Other information			
22	Funding	22	Give the source of funding and the role of the funders for the present study and, if applicable, for the original study on which the present article is based	14
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*Give information separately for exposed and unexposed groups.

Note: An Explanation and Elaboration article discusses each checklist item and gives methodological background and published examples of transparent reporting. The STROBE checklist is best used in conjunction with this article (freely available on the Web sites of PLoS Medicine at <http://www.plosmedicine.org/>, Annals of Internal Medicine at <http://www.annals.org/>, and Epidemiology at <http://www.epidem.com/>). Information on the STROBE Initiative is available at <http://www.strobe-statement.org>.

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Geometric uncertainty in intracranial aneurysm rupture status discrimination: a two-site retrospective study.

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Geometric uncertainty in intracranial aneurysm rupture status discrimination: a two-site retrospective study.

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Abstract

Objectives: Assessing the risk associated with unruptured intracranial aneurysms (IA) is essential in clinical decision making. Several geometric risk parameters have been proposed for this purpose. However, performance of these parameters has been inconsistent. This study evaluates the performance and robustness of geometric risk parameters on two datasets and compare it to the uncertainty inherent in assessing these parameters and quantifies inter-parameter correlations.

Methods: Two datasets containing 244 ruptured and unruptured IA geometries from 178 patients were retrospectively analyzed. IAs were stratified by anatomical region, based on the PHASES score locations. 37 geometric risk parameters representing four groups (size, neck, non-dimensional, and curvature parameters) were assessed. Analysis included standardized absolute differences (SAD) between ruptured and unruptured IAs, ratios of SAD to median relative uncertainty (MRU) associated with the parameters, and inter-parameter correlation.

Results: The ratio of SAD to MRU was lower for higher-dimensional size parameters (i.e., areas and volumes) than for one-dimensional size parameters. Non-dimensional size parameters performed comparatively well with regard to SAD and MRU. SAD was higher in the posterior anatomical region. Correlation of parameters was strongest within parameter (sub)groups and between size and curvature parameters, while anatomical region did not strongly affect correlation patterns.

Conclusion: Non-dimensional parameters and few parameters from other groups were comparatively robust, suggesting that they might generalize better to other datasets. The data on discriminative performance and inter-parameter correlations presented in this study may aid in developing and choosing robust geometric parameters for use in rupture risk models.

Strengths and limitations of this study

- This study provides location-specific estimates of the discriminative ability of a large set of geometric parameters for IA rupture status assessment, while also considering uncertainty.
- The analysis was performed on two independent datasets to assess robustness of the findings.
- Even though the relative uncertainty in acquisition of each geometric risk parameter was evaluated based on more than 20 individual segmentations performed during the Multiple Aneurysms Anatomy Challenge, this evaluation was only performed on five aneurysms in total.

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Introduction

A relevant part of the general population harbors one or more unruptured intracranial aneurysms (IAs), with the overall prevalence estimated around 3% [1]. While most IAs do not rupture [2], the question of whether and when to treat them remains relevant due to the poor prognosis of ruptured IAs [3, 4] as well as the risk of intervention [3, 5]. Current American Heart Association/American Stroke Association guidelines list several modifiable and non-modifiable risk factors for IA growth and/or rupture, including IA location, growth rate, morphology, smoking status, alcohol consumption, hypertension, age, sex, previous IA, and family history [6]. Attempts have been made to develop scoring systems to quantify rupture risk, growth risk, and/or support treatment decisions, these include the PHASES score by Greving et al. [7], the UIATS by Etminan et al. [8] and the ELAPSS score by Backes et al. [9]. All three of these scores are based on clinically available data and all include geometric rupture risk parameters: IA size in case of the PHASES score [7], surface irregularity, size ratio, as well as aspect ratio in case of the UIATS [8], and IA size as well as surface irregularity for the ELAPSS score [9]. While these metrics were designed to support clinical decision making, performance on clinical data has been mixed [10-12] and improvements, particularly for patients harboring multiple IAs, are desired by clinicians [13].

The aim of this paper is to assess the ability of a broad number of proposed geometric risk parameters to differentiate between unruptured and ruptured IAs while also comparing their discriminative ability relative to the uncertainty encountered in determining them. Any acquisition of patient-specific IA geometries and subsequent use of these geometries to derive geometric risk parameters is affected by a number of uncertainty-introducing factors. Starting with the medical imaging acquisition itself, which is followed by image data pre-processing, segmentation, geometry reconstruction including post-processing (e.g., smoothing, checking of topology), and finally calculation of the geometric risk parameters. All these processing steps are associated with some errors, resulting in uncertainty, which negatively affects the ability of parameters to discriminate IA rupture status. Discrimination of rupture status on an individual IA level is, however, necessary if these parameters are to support the clinical decision-making process, including any decisions regarding treatment modalities. Previous studies found high variability in the uncertainty of different geometric risk parameters as well as differences in their ability to differentiate between ruptured and unruptured IAs [14-16]. Furthermore, for geometric risk parameters with multiple alternative definitions, the specific implementation can affect the discriminative performance of the parameter itself and any derived parameters, as demonstrated by Lauric et al. for parameters incorporating IA and neck size [17].

The current study was performed to facilitate optimal selection of geometric rupture risk parameters by identifying geometric parameters, which are good discriminators while also exhibiting low uncertainty. The analysis is performed on two datasets processed by different research groups and is differentiated by

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3 anatomical region, in order to assess how the rupture status discrimination of the geometric parameters is
4 affected by geometry processing as well as anatomical location. Additionally, correlation of the geometric
5 risk parameters with each other is assessed.
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Methods

Medical imaging data

IA geometries were retrospectively reconstructed and segmented from 3D rotational angiography data acquired for routine clinical indications. Data was collected consecutively. The inclusion criteria of the datasets were imaging modality and the corresponding acquisition resolution. Cases with considerable segmentation artifacts such as close vessels that appear to be merged or holes in the segmented lumen were rejected from the analysis. 142 IAs were acquired in the Helios Klinikum Berlin-Buch (Berlin, Germany), 38 in KRH Klinikum Nordstadt (Hanover, Germany), 23 in the University Medical Center Schleswig-Holstein (UKSH) (Kiel, Germany), and 41 in the University Hospital Magdeburg (Magdeburg, Germany). Processing of the imaging data, including segmentation, was performed at two sites: Berlin, which processed 142 IAs from Helios Klinikum Berlin-Buch (dataset 1), and Magdeburg, which processed 102 IAs from KRH Klinikum Nordstadt, UKSH, and University Hospital Magdeburg (dataset 2). Overall, 244 IAs from 178 patients were included, from which geometric risk parameters were subsequently calculated. Based on the PHASES score [7], aneurysm location was classified into four anatomical regions: internal carotid artery (ICA), middle cerebral artery (MCA), anterior region (all vessels anterior of the ICA/MCA), and posterior region (all vessels posterior of the ICA/MCA). The distribution of the individual IA locations and their assignment to the four anatomical regions are shown in Table 1.

Table 1: Frequency and rupture status of individual IA locations by dataset. ACA: anterior cerebral artery, AComA: anterior communicating artery, AChA: anterior choroidal artery, ICA: internal carotid artery, MCA: middle cerebral artery, PComA: posterior communicating artery, PCA: posterior cerebral artery, SCA: superior cerebellar artery, BA: basilar artery, PICA: posterior inferior cerebellar artery, VA: vertebral artery.

Anatomical region	Vessel	Dataset 1 unruptured	Dataset 1 ruptured	Dataset 2 unruptured	Dataset 2 ruptured
Anterior	ACA	3	1	2	2
	AComA	10	22	11	5
ICA	AChA	0	1	1	2
	ICA	29	8	19	4
MCA	MCA	28	10	31	8
Posterior	PComA	8	10	2	4
	PCA	0	1	0	0
	SCA	0	0	1	1
	BA	4	3	3	4
	PICA	0	4	1	0
	VA	0	0	0	1

Geometric risk parameters

Historically, several geometric parameters for IA rupture risk assessment have been proposed. In order to have access to information on parameter uncertainty, the parameters chosen for this study were limited to a subset of the parameters reported in Goubergrits et al. [14], a parameter uncertainty study performed on segmentation data obtained during the Multiple Aneurysms AnaTomy Challenge (MATCH) 2018 [18]. The major outcome of this study was the median relative uncertainty (MRU) of geometric parameters. Briefly, five aneurysms were segmented and reconstructed by 26 international research groups, which participated in the MATCH challenge. These segmentations were used to calculate the median and the 68.3% range between the 84.13th and the 15.87th percentile of all selected geometric parameters for each of the five aneurysms. The uncertainty range was selected with respect to the range of \pm one standard deviation for normally distributed data reported in other studies. The uncertainty was defined as the uncertainty range divided by the median value and calculated for each geometric parameter. Finally, the average of all five aneurysms was calculated to define the MRU. For a detailed description of the parameters and the rationale for choosing the parameters, the interested reader is referred to Goubergrits et al. [14]. Briefly, most of the proposed geometric parameters describe aneurysm and/or aneurysmal neck size or shape, or irregularity. These parameters were previously proposed as predictors for rupture risk. Table 2 lists the geometric parameters, their abbreviations and MRU values, as well as their respective references.

Table 2: List of the investigated geometric parameters, their descriptions, and median relative uncertainties (MRU). Note that terminology and implementation in the references might differ subtly. Derived and modified from tables 1-5 from Goubergrits et al. [14], used under Creative Commons Attribution License (CC BY 4.0). The CC BY 4.0 license text is available at <https://creativecommons.org/licenses/by/4.0/>.

Parameter group	Parameter name, unit [exemplary reference]	Parameter abbreviation	Short description	MRU
Size	Height, mm [19]	H	Maximum perpendicular distance from the neck plane to the aneurysm surface	0.140
	Maximum dimension, mm [20]	L_{\max}	Maximum distance between two points on the aneurysm surface	0.157
	Maximum height, mm [15]	H_{\max}	Maximum distance between the centroid of the neck and the aneurysm surface	0.123
	Maximum diameter, mm [17]	D_{\max}	Maximum neck plane-parallel distance between two points on the aneurysm surface	0.169
	Bulge height, mm [19]	H_b	Distance between the neck plane and the maximum diameter	0.373
	Surface area, mm ² [15]	A	Surface area of the aneurysm	0.215

	Convex hull surface area, mm ² [15]	A_{CH}	Surface area of the aneurysm's convex hull	0.277
	Minimal bounding sphere surface area, mm ² [21]	A_{MBS}	Surface area of the aneurysm's minimal bounding sphere	0.305
	Closed surface area, mm ²	A_{closed}	Surface area of the neck-closed aneurysm	0.283
	Volume, mm ³ [15]	V	Volume of the neck-closed aneurysm	0.392
	Convex hull volume, mm ³ [15]	V_{CH}	Volume of the aneurysm's convex hull	0.399
	Minimal bounding sphere volume, mm ³ [21]	V_{MBS}	Volume of the aneurysm's minimal bounding sphere	0.451
Neck	Minimum neck diameter, mm [17]	$D_{neck,min}$	Minimum distance between two opposite points on the neck perimeter	0.306
	Maximum neck diameter, mm [22]	$D_{neck,max}$	Maximum distance between two points on the neck perimeter	0.348
	Neck perimeter, mm [19]	P_{neck}	Perimeter of the aneurysm neck	0.374
	Equivalent neck diameter, mm [19]	$D_{neck,equiv}$	Hydraulic diameter of the aneurysm neck	0.276
	Neck area, mm ² [19]	A_{neck}	Area of the aneurysm neck	0.593
	Elliptical neck area, mm ²	$A_{neck,elliptical}$	Neck area calculated as the product of the minimum and maximum neck diameter	0.650
Non-dimensional	Aspect ratio [22]	AR	Ratio of height to maximum neck diameter	0.293
	Equivalent aspect ratio [19]	eAR	Ratio of height to equivalent neck diameter	0.326
	Bottleneck factor [19]	BF	Ratio of maximum diameter to maximum neck diameter	0.201
	Bulge location [19]	BL	Ratio of bulge height to height	0.301
	Nonsphericity index [15]	NSI	Normalized ratio of volume to surface area relative to a hemisphere	0.108
	Aneurysm volume to bounding sphere volume [21]	AVSV	Ratio of volume to minimal bounding sphere volume	0.173
	Aneurysm surface area to bounding sphere area [21]	AASA	Ratio of surface area to minimal bounding sphere surface area	0.095

	Undulation index [15]	UI	1 minus the ratio of volume to convex hull volume	0.709
	Ellipticity index [15]	EI	Normalized ratio of convex hull volume to convex hull surface area relative to a hemisphere	0.051
Curvature	Mean of mean curvature, mm ⁻¹ [19]	MAA	Surface average of local mean curvature	0.136
	Mean of absolute mean curvature, mm ⁻¹	absMAA	Surface average of the magnitude of the local mean curvature	0.133
	Standard deviation of mean curvature, mm ⁻¹	MSD	Standard deviation of the local mean curvature	1.011
	High mean curvature, % [21]	HMC	Relative increase of the mean of absolute mean curvature over the mean curvature of the minimal bounding sphere	0.396
	L2-norm of mean curvature [19]	MLN	Scale invariant measure of surface irregularity, uses mean curvature	0.150
	Mean of Gaussian curvature, mm ⁻² [19]	GAA	Surface average of local Gaussian curvature	0.344
	Mean of absolute Gaussian curvature, mm ⁻²	absGAA	Surface average of the magnitude of the local Gaussian curvature	0.485
	Standard deviation of Gaussian curvature, mm ⁻²	GSD	Standard deviation of the local Gaussian curvature	1.798
	High Gaussian curvature, % [21]	HGC	Relative increase of the mean of absolute Gaussian curvature over the Gaussian curvature of the minimal bounding sphere	0.822
L2-norm of Gaussian curvature [19]	GLN	Scale invariant measure of surface irregularity, uses Gaussian curvature	0.545	

Since the diameter of the parent vessel was not available for all IAs studied, size ratio could not be calculated and was excluded. Furthermore, UI and CR as well as NSI and NPR are directly related through $CR = 1 - UI$ and $IPR = \frac{\sqrt[3]{18\pi}}{1 - NSI}$, respectively. CR and IPR were therefore not included in the analysis, in order to avoid redundancy. Geometric risk parameters were calculated from the IA geometries using MATLAB (version R2017b, MathWorks, Natick, USA), Python (version 3.7.1, Python Software Foundation, Delaware, USA), and ZIBAmira (version 2015.28, Zuse Institute Berlin, Germany). The individual parameter values, IA location, and rupture status for each IA in this study, as well as the exact

values of the inter-parameter correlation coefficients are provided as supplemental material 1 and 2 respectively.

Statistical analysis

Since most of the geometric risk parameters were non-normally distributed, as assessed by Q-Q plots and Shapiro-Wilk tests, the median was used to quantify central tendency and the interquartile range was used to quantify dispersion. Correlations were quantified using Pearson's r with correlations $|r| \geq 0.75$ referred to as strong, while those with $0.75 > |r| \geq 0.25$ and $|r| < 0.25$ referred to as moderate and weak, respectively. Statistical analysis was performed using SPSS (version 28.0.0.0, IBM, Armonk, USA) and MATLAB.

The discriminative ability of the individual parameters was assessed by standardizing the absolute difference between the medians of the ruptured and unruptured IAs with the weighted arithmetic mean of the IQRs of the two groups. This measure of effect size will be referred to as the standardized absolute group difference (SAD). Furthermore, the ratio of the SAD to the relative uncertainty, a measure of the uncertainty associated with parameter calculation, from Goubergrits et al. [14] was calculated for all parameters and will be referred to as the group difference-uncertainty ratio (DUR). The equations for SAD and DUR are thus $SAD = \frac{(n_r + n_u) \cdot |m_r - m_u|}{n_r IQR_r + n_u IQR_u}$ and $DUR = \frac{SAD}{MRU}$, where n_i , m_i , and IQR_i are the sample sizes, median values, and interquartile ranges of the geometric parameters evaluated for ruptured (subscript r) and unruptured (subscript u) samples, while MRU is the median relative uncertainty from Goubergrits et al. [14], which is also listed in Table 2. SAD and DUR may take any value ≥ 0 with higher values indicating stronger discriminative ability and a better ratio of discriminative ability to uncertainty, respectively. SAD and DUR values of zero would indicate no discriminative ability and the worst possible ratio of discriminative ability to uncertainty, respectively. Additionally, the correlation coefficients between the parameters were calculated. Analysis of SAD and DUR as well as the correlation coefficients was performed individually for each anatomical region and each dataset.

Patient and public involvement

Due to the purely retrospective manner of this study, no involvement of patients or the general public was considered.

Results

Figure 1 shows SAD for all geometric risk parameters by anatomical region and dataset. Considering both datasets, the following parameters achieved the comparatively highest SAD for each anatomical region: curvature (HMC, MLN, HGC, GLN) and non-dimensional (AR, eAR, AVSV, AASA) parameters in the anterior region, curvature (HMC, HGC) and non-dimensional (NSI, AASA, EI) parameters in the ICA, non-dimensional (AR, eAR, BL, AVSV, AASA) parameters in the MCA, and size (H, L_{\max} , A, A_{MBS}) and curvature (MSD, absGAA, GSD) parameters in the posterior region. Compared to the other anatomical regions, SAD was higher in the posterior region and more parameters exhibited relatively high SAD. Looking at all anatomical regions combined, curvature (HMC, MLN, absGAA, HGC, GLN) and non-dimensional (AR, eAR, AVSV, AASA) parameters as well as one neck ($D_{\text{neck,min}}$) and one size (H_b) parameter show comparatively high SAD in both datasets. Furthermore, the differences between the two datasets become less pronounced when combining all anatomical regions. Moreover, this combined evaluation resulted in SAD being higher for the size parameters in site 2 compared to site 1. Here, it is worthwhile to note that the SAD of this combined assessment is not the average of the SAD of all four region-specific evaluations. Thus, pooling for some parameters can result in the absolute difference between the ruptured and unruptured groups to be close to zero, which results in SAD values close to zero as observed for the one-dimensional size parameters of the site 1 dataset.

Figure 2 shows DUR for all geometric risk parameters by anatomical region and dataset. Considering both datasets, the following parameters achieved the comparatively highest DUR for each anatomical region: non-dimensional (AASA, EI) and one curvature (MLN) parameter in the anterior region, non-dimensional (EI, AASA, NSI) parameters in the ICA, non-dimensional (AASA, EI) parameters in the MCA, and size parameters (H, L_{\max} , H_{\max} , A), curvature (MAA, absMAA), and one non-dimensional (EI) parameter in the posterior region. Similar to SAD, DUR in the posterior region was overall higher and more parameters exhibited relatively high DUR, compared to the other anatomical regions. Looking at all anatomical regions combined, non-dimensional (NSI, AVSV, AASA, EI) and curvature (absMAA, MLN) parameters show comparatively high DUR in both datasets. As for SAD, the differences between the two datasets are less pronounced when looking at all anatomical regions combined.

Figures 3 and 4 show correlation coefficients between the geometric risk parameters by anatomical region for both datasets. The following general features are present in most data correlation plots: The size parameters (H, L_{\max} , H_{\max} , D_{\max} , H_b , A, A_{CH} , A_{MBS} , A_{closed} , V, V_{CH} , V_{MBS}) are generally strongly correlated with each other. Similarly, the neck parameters ($D_{\text{neck,min}}$, $D_{\text{neck,max}}$, P_{neck} , $D_{\text{neck,equiv}}$, A_{neck} , $A_{\text{neck,elliptical}}$) are also generally strongly correlated with each other.

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3 Within the non-dimensional parameter group, there are two distinct subgroups in most plots: one formed by
4 AR, eAR, BF, and BL and one formed by NSI, AVSV, AASA, UI, and EI. Within the latter subgroup,
5 several of the correlations are negative but their magnitude is overall moderate to strong. The curvature
6 parameters also form two subgroups, one formed by dimensional curvature parameters (MAA, absMAA,
7 MDS, GAA, absGAA, GSD) and one by non-dimensional curvature parameters (HMC, MLN, HGC, GLN).
8 With regard to correlations between parameter groups, there is generally moderate to strong correlation
9 between the size and neck parameters. Additionally, the size and neck parameters are generally moderately
10 correlated with the curvature parameters, the direction of the correlation being positive for the non-
11 dimensional curvature parameters and negative for the dimensional curvature parameters.
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Discussion

Previous research has assessed the impact of uncertainty on geometric risk parameters in a limited fashion. Ma et al. examined the influence of random noise on the calculation of 14 geometric risk parameters, finding curvature parameters more susceptible to random noise than size, neck, and non-dimensional parameters [19]. Others have examined the influence of imaging modality [23] and CT angiography reconstruction kernel [24] on geometric risk parameters. Regarding image acquisition, Ramachandran et al. have examined the influence of imaging modality [23], while O'Meara et al. [24] and Berg et al. [25] have focused on the reconstruction kernel's effect on geometric and hemodynamic risk parameters, respectively. The current study as well as the earlier uncertainty study based on the MATCH challenge were both based on 3D rotational angiography imaging, which is the routine imaging modality in both centers involved in this study. Other sensitivity and uncertainty aspects of computational fluid dynamics approaches to IAs have been explored, e.g., by Cebral et al. [26], Sarrami-Foroushani et al. [27], and Schneiders et al. [28]. To the authors' knowledge there is, however, no comprehensive publication relating discriminative performance and uncertainty of geometric risk parameters, while also providing detailed data on their correlation with each other.

Looking at the parameter groups examined in this study, the following findings can be made: the size and neck parameters measuring areas (A , A_{CH} , A_{MBS} , A_{closed} , A_{neck} , $A_{neck,elliptical}$) and volumes (V , V_{CH} , V_{MBS}) generally do not achieve high DUR, despite having SAD similar to the size and neck parameters measuring length (H , L_{max} , H_{max} , D_{max} , H_b , $D_{neck,min}$, $D_{neck,max}$, P_{neck} , $D_{neck,equiv}$). The cause is the higher uncertainty encountered in determining the higher-dimensional parameters when compared to the one-dimensional parameters [14]. This suggests that higher-dimensional size parameters tend to be less robust and thus less suitable for use in practical risk models than one-dimensional size parameters. Like Lauric et al. [17], there are instances of noticeable differences in the discriminative performance of parameters capturing the same aspect of IA geometry, e.g., for the neck size parameters. The non-dimensional parameters exhibit comparatively high SAD and DUR, except for BL and UI, which exhibit lower discriminative ability and/or higher uncertainty in their calculation. The curvature parameters show substantial variability in SAD and DUR depending on the anatomical region and the parameter, with MLN performing comparatively well overall. It is notable that the posterior region tends to exhibit higher SAD and DUR than the other regions, indicating more pronounced geometric differences between ruptured and unruptured IAs in this region. Regarding the differences in SAD and DUR between datasets 1 and 2, it is likely that differences in the patient collectives, subsample sizes, and reconstruction techniques are the main causes. The latter could in the future be tackled by machine learning-based segmentation methods, which can reduce operator-induced uncertainty. Examples of such methods have previously been presented, e.g., in the context of the CADA challenge [29].

Regarding the correlation patterns, there is substantial similarity between all analyzed anatomical regions and datasets. Parameters tend to be most strongly correlated with other parameters from the same parameter group, except for the non-dimensional and curvature parameters, which form two subgroups each. This is reasonable, given that the parameters within each parameter group capture similar aspects of IA geometry. For the size and neck parameter groups this is obvious, since they both capture aspects of IA and neck size, respectively. The two distinct correlation subgroups within the non-dimensional parameter group are likely caused by the underlying parameter subgroups capturing different aspects of aneurysm shape. While the parameters of the first subgroup (AR, eAR, BF, BL) are simply ratios of one-dimensional size parameters, the second subgroup (NSI, AVSV, AASA, UI, EI) is formed by parameters relating aneurysm area and/or volume to geometric reference objects, e.g., the minimal bounding sphere or convex hull. The negative correlation between AVSV and AASA with the other parameters from the second subgroup is due to the parameter definitions, which cause AVSV and AASA to increase with increasing sphericity, while the other parameters tend to decrease with increasing sphericity. The curvature parameters also form two subgroups, with the first subgroup consisting of the dimensional parameters quantifying the mean or dispersion of IA surface curvature (MAA, absMAA, MSD, GAA, absGAA, GSD) and the second subgroup consisting of non-dimensional, scale invariant curvature parameters (HMC, MLN, HGC, GLN). Since the former parameters intrinsically decrease with IA size, while the latter parameters increase with IA size, the negative correlation of the two subgroups with each other makes sense. It should be noted that the positive correlation of the non-dimensional curvature parameters with IA size is not an intrinsic property of the non-dimensional parameters themselves, since they are designed to be scale invariant. It rather indicates that curvature and irregularities of the IA surface increase in larger IAs.

For a geometric risk parameter to be a good candidate for rupture risk prediction, it should generally have a high SAD, in order to be able to differentiate between ruptured and unruptured IAs. Additionally, DUR should be high, indicating low sensitivity of the parameter to the imaging, segmentation, and calculation workflow, by which it is calculated. This is desirable because it allows models including such parameters to generalize well to other datasets. Finally, when choosing a set of parameters, data from the correlation analysis can be used to identify parameters that are not strongly correlated. Neyazi et al. have previously used this method to derive a two-parameter rupture status prediction model from a set of 49 geometric and hemodynamic rupture risk parameters, identifying AR and the maximal relative residence time as the most suitable model parameters [13]. Other attempts to identify suitable rupture status prediction models based on geometric risk parameters have been attempted, e.g., Dhar et al. [15] and Zhang et al. [30], but results have generally been inconsistent. Possible reasons for the discrepant findings regarding optimal parameter choice are the sample sizes used and the uncertainty inherent in the workflow by which the parameters are calculated. This may lead to the selection of less robust parameters that perform well on a given dataset but

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3 generalize less well to others. Based on the results of this study and considering SAD, DUR, as well as the
4 correlation between geometric risk parameters, examples of more robust parameter choices could look as
5 follows:
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- 8 • H_{\max} , $D_{\text{neck},\text{min}}$, AR, AASA, and MLN for the anterior region.
- 9 • L_{\max} , P_{neck} , AR, AASA, and HGC for the ICA.
- 10 • D_{\max} , $D_{\text{neck},\text{min}}$, eAR, AASA, and HMC for the MCA.
- 11 • L_{\max} , $D_{\text{neck},\text{min}}$, BL, EI, and absMAA for the posterior region.
- 12 • H_b , $D_{\text{neck},\text{min}}$, AR, AASA, and MLN if looking at all anatomical regions combined.

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17 Overall, while individual size, neck, and curvature parameters achieved good discriminative performance
18 and robustness, the non-dimensional parameters tended to perform well as a group. This suggests that non-
19 dimensional geometric risk parameters can provide comparatively good discriminative performance, while
20 the nondimensionalization itself mitigates some of the uncertainty introduced through the workflow by
21 which the parameters are calculated [14]. Neither did we attempt to develop a novel aneurysm rupture risk
22 prediction model, nor did we test earlier published models [16, 31]. We decided against this analysis due to
23 the large variety of published proposed risk models. Testing them as well as the propagation of the
24 parameter's uncertainty towards assessment of rupture risk should be tested in a separate study. Finally,
25 elaborated models will also require further information such as hypertension status, earlier SAH as well as
26 hemodynamic parameters, which were unavailable within this study.
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34 Limitations

35 IAs were grouped by anatomical region because IA location is an important determinant of rupture risk, as
36 demonstrated by its weight in current risk scores [7-9]. However, by analyzing the datasets by anatomical
37 region, some subsamples become quite small. Small sample size might affect the accuracy of the median
38 and interquartile range estimates derived from these groups. This limitation is, however, partially mitigated
39 by also analyzing all anatomical regions combined and using two datasets, in order to get a more
40 comprehensive picture of the risk parameters' performance. The major focus of the study was the analysis
41 of the performance and robustness of 37 geometric risk parameters. Thus, not all findings of this study could
42 be assessed in depth. For example, we decided for grouping of aneurysms by anatomical regions as
43 recommended by clinical scores, such as such as PHASES score [7]. While we observed differences in both
44 SAD and DUR based on the aneurysms' location within the circulation, the underlying mechanisms for
45 these differences cannot be assessed by the available data. However, Tykocki & Kostkiewicz found
46 significant differences between some geometric parameters (parent artery size, size ratio and aspect ratio)
47 of aneurysms for the anterior and the posterior regions [32]. They associated the difference in these
48 parameters to different impacts on the intra-aneurysmal hemodynamics such as vortex formation and wall
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3 shear stress. Why these geometric parameters might result in different hemodynamic conditions and rupture
4 risks must be investigated in a dedicated study. This is especially important as this study's findings
5 demonstrated differences in the SAD not only between locations and the cohorts, but also when all aneurysm
6 locations were evaluated together.
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10 Another potential limitation is the uncertainty values from Goubergrits et al. [14], which were used to
11 calculate DUR. These values were calculated on a sample containing MCA and posterior region IAs [14].
12 While it does not seem particularly probable, it is possible that IA location and size might affect the
13 uncertainty inherent in calculating the geometric risk parameters in a relevant manner, which in turn could
14 influence DUR results. Respectively the generalization of MRU values from the uncertainty study [14]
15 should be considered with caution, especially as those values were calculated only based on five aneurysms.
16 A more fundamental limitations is the focus on geometric risk parameters. These parameters serve as proxies
17 for the pathophysiological processes leading to IA rupture through the latter's influence on the geometry of
18 the IA surface. Due to their nature, geometric risk parameters cannot directly capture the hemodynamic,
19 mechanical, or biochemical aspects of IA rupture. Nevertheless, they are among the most intensely
20 researched types of IA rupture risk parameters, due to the comparative ease with which they can be
21 calculated from clinical data.
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24 All parameters included within this study have been discussed in previous literature as potential risk
25 parameters. Note, however, that the list of parameters investigated in this study is not exhaustive. More
26 proposed geometric parameters can be found in recent literature [33]. The parameters investigated here are
27 limited to a set of parameters investigated earlier in frames of the uncertainty study [14]. Second, these
28 parameters were constrained to parameters, that can be calculated automatically.
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31 Finally, the calculation of geometric parameters including the ostium plane depends on a sufficient reference
32 plane selection. Recently, Berg et al. quantified the potential effect of neck curve variations on
33 hemodynamic predictions [34]. These findings could be transferred to the cases included in this study in
34 future work.
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37 Due to the retrospective nature of this work, only the parameters' capabilities to discriminate the rupture
38 status could be assessed by comparing their respective values observed in ruptured or unruptured IA. To
39 adequately assess the capabilities of any model using these parameters for rupture risk assessment, it has to
40 be evaluated on a longitudinal cohort containing only UIA.
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45 Conclusion

46 Based on datasets from two research groups, the present study provides location-specific estimates of the
47 discriminative ability of a large set of geometric risk parameters for IA rupture status assessment, while also
48 considering uncertainty. Additionally, correlation patterns between the parameters are identified. The
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3 presented data is potentially useful in evaluating geometric risk parameters for use in rupture risk models or
4 when choosing input parameters for machine learning approaches to rupture risk prediction. It may also be
5 helpful when designing future geometric risk parameters for clinical use.
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Conflict of interest statement

The authors declare that there is no conflict of interest.

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Data Availability Statement

All individual parameter values as well as the correlation coefficients are made available as supplemental material.

Ethical approval statements

In this study, patient-specific 3D reconstructions of intracranial aneurysms based on routine information were evaluated retrospectively. Use of retrospective data was approved by the local ethics committees (Ethikkommission der Charité - Universitätsmedizin Berlin: EA2/222/19; Ethikkommission der Med. Hochschule Hannover: NOVA Nr. 68/20).

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Author contributions

All roles according to CRediT (contributor roles taxonomy). Conceptualization: LG, JS, FH, JB, and PB. Methodology: FH, JS, and LG. Resources: AS, IES, OB, NL, SS, and PB. Investigation: JB, FH, and JS. Formal Analysis: FH. Funding acquisition: LG, PB, and SS. Supervision: LG. Writing – original draft: FH, LG, and JB. Writing – review & editing: PB, SS, AS, IES, OB, NL, and JS.

References

1. Vlak, M.H., A. Algra, R. Brandenburg, and G.J. Rinkel, *Prevalence of unruptured intracranial aneurysms, with emphasis on sex, age, comorbidity, country, and time period: a systematic review and meta-analysis*. *Lancet Neurol*, 2011. **10**(7): p. 626-36.
2. Brown, R.D., Jr. and J.P. Broderick, *Unruptured intracranial aneurysms: epidemiology, natural history, management options, and familial screening*. *Lancet Neurol*, 2014. **13**(4): p. 393-404.
3. Wiebers, D.O., J.P. Whisnant, J. Huston, 3rd, I. Meissner, R.D. Brown, Jr., D.G. Piepgras, G.S. Forbes, K. Thielen, D. Nichols, W.M. O'Fallon, J. Peacock, L. Jaeger, N.F. Kassell, G.L. Kongable-Beckman, J.C. Torner, and I. International Study of Unruptured Intracranial Aneurysms, *Unruptured intracranial aneurysms: natural history, clinical outcome, and risks of surgical and endovascular treatment*. *Lancet*, 2003. **362**(9378): p. 103-10.
4. Rackauskaite, D., E. Svanborg, E. Andersson, K. Lowhagen, L. Csajbok, and B. Nellgard, *Prospective study: Long-term outcome at 12-15 years after aneurysmal subarachnoid hemorrhage*. *Acta Neurol Scand*, 2018. **138**(5): p. 400-407.
5. Pontes, F.G.B., E.M. da Silva, J.C. Baptista-Silva, and V. Vasconcelos, *Treatments for unruptured intracranial aneurysms*. *Cochrane Database Syst Rev*, 2021. **5**: p. CD013312.
6. Thompson, B.G., et al., *Guidelines for the Management of Patients With Unruptured Intracranial Aneurysms: A Guideline for Healthcare Professionals From the American Heart Association/American Stroke Association*. *Stroke*, 2015. **46**(8): p. 2368-400.
7. Greving, J.P., M.J. Wermer, R.D. Brown, Jr., A. Morita, S. Juvela, M. Yonekura, T. Ishibashi, J.C. Torner, T. Nakayama, G.J. Rinkel, and A. Algra, *Development of the PHASES score for prediction of risk of rupture of intracranial aneurysms: a pooled analysis of six prospective cohort studies*. *Lancet Neurol*, 2014. **13**(1): p. 59-66.
8. Etminan, N., et al., *The unruptured intracranial aneurysm treatment score: a multidisciplinary consensus*. *Neurology*, 2015. **85**(10): p. 881-9.
9. Backes, D., et al., *ELAPSS score for prediction of risk of growth of unruptured intracranial aneurysms*. *Neurology*, 2017. **88**(17): p. 1600-1606.
10. Juvela, S., *PHASES score and treatment scoring with cigarette smoking in the long-term prediction of rupturing of unruptured intracranial aneurysms*. *J Neurosurg*, 2022. **136**(1): p. 156-162.
11. Molenberg, R., M.W. Aalbers, A. Mazuri, G.J. Luijckx, J.D.M. Metzemaekers, R.J.M. Groen, M. Uyttenboogaart, and J.M.C. van Dijk, *The Unruptured Intracranial Aneurysm Treatment Score as a predictor of aneurysm growth or rupture*. *Eur J Neurol*, 2021. **28**(3): p. 837-843.
12. Hernandez-Duran, S., D. Mielke, V. Rohde, and V. Malinova, *Is the unruptured intracranial aneurysm treatment score (UIATS) sensitive enough to detect aneurysms at risk of rupture?* *Neurosurg Rev*, 2021. **44**(2): p. 987-993.
13. Neyazi, B., V.M. Swiatek, M. Skalej, O. Beuing, K.P. Stein, J. Hattingen, B. Preim, P. Berg, S. Saalfeld, and I.E. Sandalcioglu, *Rupture risk assessment for multiple intracranial aneurysms: why there is no need for dozens of clinical, morphological and hemodynamic parameters*. *Ther Adv Neurol Disord*, 2020. **13**: p. 1756286420966159.
14. Goubergrits, L., F. Hellmeier, J. Bruening, A. Spuler, H.C. Hege, S. Voss, G. Janiga, S. Saalfeld, O. Beuing, and P. Berg, *Multiple Aneurysms AnaTomy CHallenge 2018 (MATCH): uncertainty quantification of geometric rupture risk parameters*. *Biomed Eng Online*, 2019. **18**(1): p. 35.
15. Dhar, S., M. Tremmel, J. Mocco, M. Kim, J. Yamamoto, A.H. Siddiqui, L.N. Hopkins, and H. Meng, *Morphology parameters for intracranial aneurysm rupture risk assessment*. *Neurosurgery*, 2008. **63**(2): p. 185-96; discussion 196-7.
16. Detmer, F.J., B.J. Chung, F. Mut, M. Slawski, F. Hamzei-Sichani, C. Putman, C. Jimenez, and J.R. Czebral, *Development and internal validation of an aneurysm rupture probability model based on patient characteristics and aneurysm location, morphology, and hemodynamics*. *Int J Comput Assist Radiol Surg*, 2018. **13**(11): p. 1767-1779.

17. Lauric, A., M.I. Baharoglu, and A.M. Malek, *Ruptured status discrimination performance of aspect ratio, height/width, and bottleneck factor is highly dependent on aneurysm sizing methodology*. Neurosurgery, 2012. **71**(1): p. 38-45.
18. Berg, P., et al., *Multiple Aneurysms AnaTomy CHallenge 2018 (MATCH): Phase I: Segmentation*. Cardiovasc Eng Technol, 2018. **9**(4): p. 565-581.
19. Ma, B., R.E. Harbaugh, and M.L. Raghavan, *Three-dimensional geometrical characterization of cerebral aneurysms*. Ann Biomed Eng, 2004. **32**(2): p. 264-73.
20. Lauric, A., E.L. Miller, M.I. Baharoglu, and A.M. Malek, *3D shape analysis of intracranial aneurysms using the writhe number as a discriminant for rupture*. Ann Biomed Eng, 2011. **39**(5): p. 1457-69.
21. Chien, A., J. Sayre, and F. Vinuela, *Comparative morphological analysis of the geometry of ruptured and unruptured aneurysms*. Neurosurgery, 2011. **69**(2): p. 349-56.
22. Ujiie, H., Y. Tamano, K. Sasaki, and T. Hori, *Is the aspect ratio a reliable index for predicting the rupture of a saccular aneurysm?* Neurosurgery, 2001. **48**(3): p. 495-502; discussion 502-3.
23. Ramachandran, M., R. Retarekar, R.E. Harbaugh, D. Hasan, B. Policeni, R. Rosenwasser, C. Ogilvy, and M.L. Raghavan, *Sensitivity of Quantified Intracranial Aneurysm Geometry to Imaging Modality*. Cardiovasc Eng Technol, 2013. **4**(1): p. 75-86.
24. O'Meara, B., J.P. Rahal, A. Lauric, and A.M. Malek, *Benefit of a sharp computed tomography angiography reconstruction kernel for improved characterization of intracranial aneurysms*. Neurosurgery, 2014. **10 Suppl 1**: p. 97-105; discussion 105.
25. Berg, P., S. Saalfeld, S. Voss, T. Redel, B. Preim, G. Janiga, and O. Beuing, *Does the DSA reconstruction kernel affect hemodynamic predictions in intracranial aneurysms? An analysis of geometry and blood flow variations*. J Neurointerv Surg, 2018. **10**(3): p. 290-296.
26. Cebal, J.R., M.A. Castro, S. Appanaboyina, C.M. Putman, D. Millan, and A.F. Frangi, *Efficient pipeline for image-based patient-specific analysis of cerebral aneurysm hemodynamics: technique and sensitivity*. IEEE Trans Med Imaging, 2005. **24**(4): p. 457-67.
27. Sarrami-Foroushani, A., T. Lassila, and A.F. Frangi, *Virtual endovascular treatment of intracranial aneurysms: models and uncertainty*. Wiley Interdiscip Rev Syst Biol Med, 2017. **9**(4).
28. Schneiders, J.J., H.A. Marquering, L. Antiga, R. van den Berg, E. VanBavel, and C.B. Majoie, *Intracranial aneurysm neck size overestimation with 3D rotational angiography: the impact on intra-aneurysmal hemodynamics simulated with computational fluid dynamics*. AJNR Am J Neuroradiol, 2013. **34**(1): p. 121-8.
29. Ivantsits, M., et al., *Detection and analysis of cerebral aneurysms based on X-ray rotational angiography - the CADA 2020 challenge*. Med Image Anal, 2021. **77**: p. 102333.
30. Zheng, Y., F. Xu, J. Ren, Q. Xu, Y. Liu, Y. Tian, and B. Leng, *Assessment of intracranial aneurysm rupture based on morphology parameters and anatomical locations*. J Neurointerv Surg, 2016. **8**(12): p. 1240-1246.
31. Lall, R.R., C.S. Eddleman, B.R. Bendok, and H.H. Batjer, *Unruptured intracranial aneurysms and the assessment of rupture risk based on anatomical and morphological factors: sifting through the sands of data*. Neurosurg Focus, 2009. **26**(5): p. E2.
32. Tykocki, T. and B. Kostkiewicz, *Aneurysms of the anterior and posterior cerebral circulation: comparison of the morphometric features*. Acta Neurochir (Wien), 2014. **156**(9): p. 1647-54.
33. Juchler, N., S. Schilling, P. Bijlenga, V. Kurtcuoglu, and S. Hirsch, *Shape Trumps Size: Image-Based Morphological Analysis Reveals That the 3D Shape Discriminates Intracranial Aneurysm Disease Status Better Than Aneurysm Size*. Front Neurol, 2022. **13**: p. 809391.
34. Berg, P., B. Behrendt, S. Voss, O. Beuing, B. Neyazi, I.E. Sandalcioglu, B. Preim, and S. Saalfeld, *VICTORIA: Virtual neck Curve and True Ostium Reconstruction of Intracranial Aneurysms*. Cardiovasc Eng Technol, 2021. **12**(4): p. 454-465.

Figures

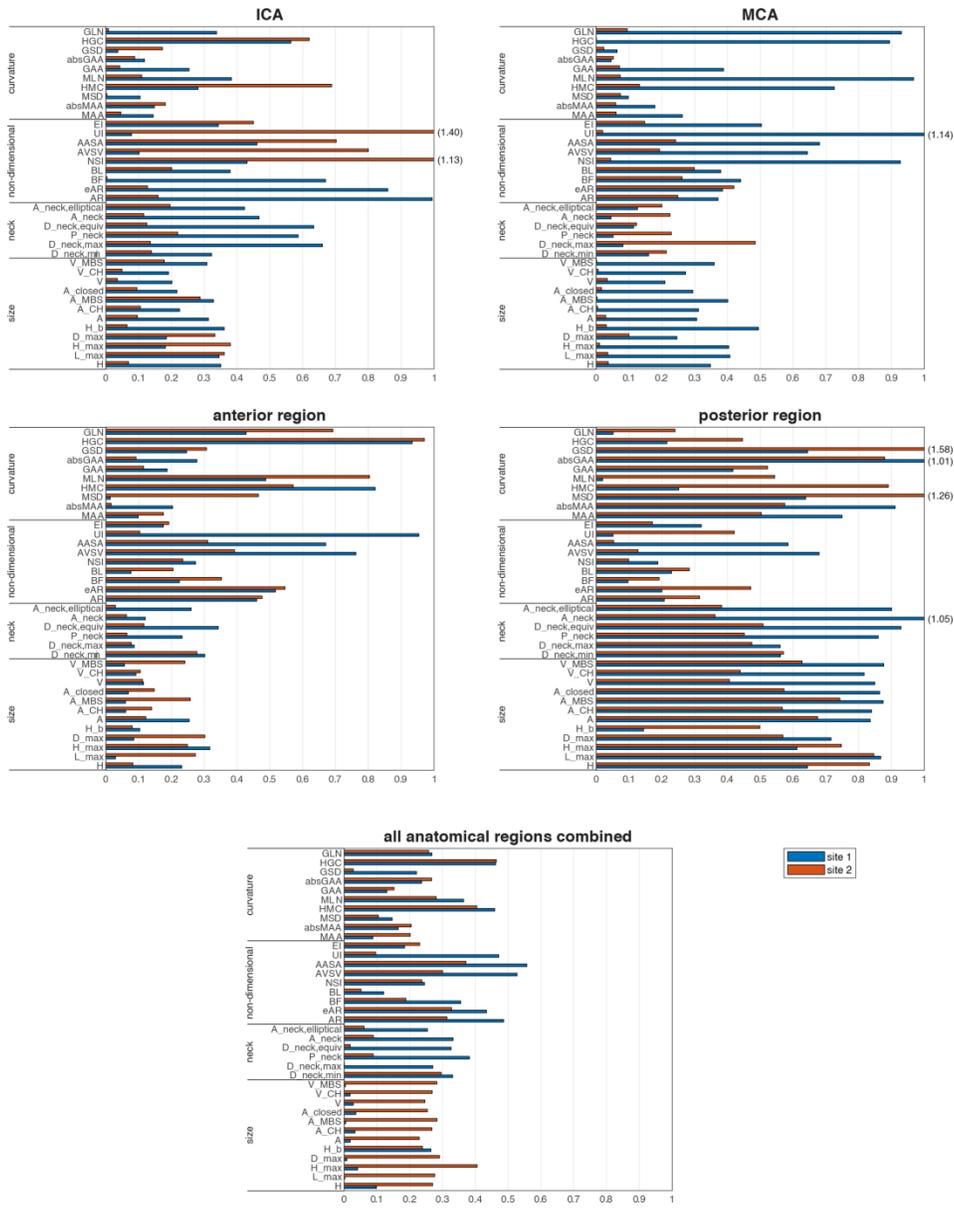
Figure 1: Standardized absolute group difference (SAD) for each anatomical region and dataset.

Figure 2: Group difference-uncertainty ratio (DUR) for each anatomical region and dataset.

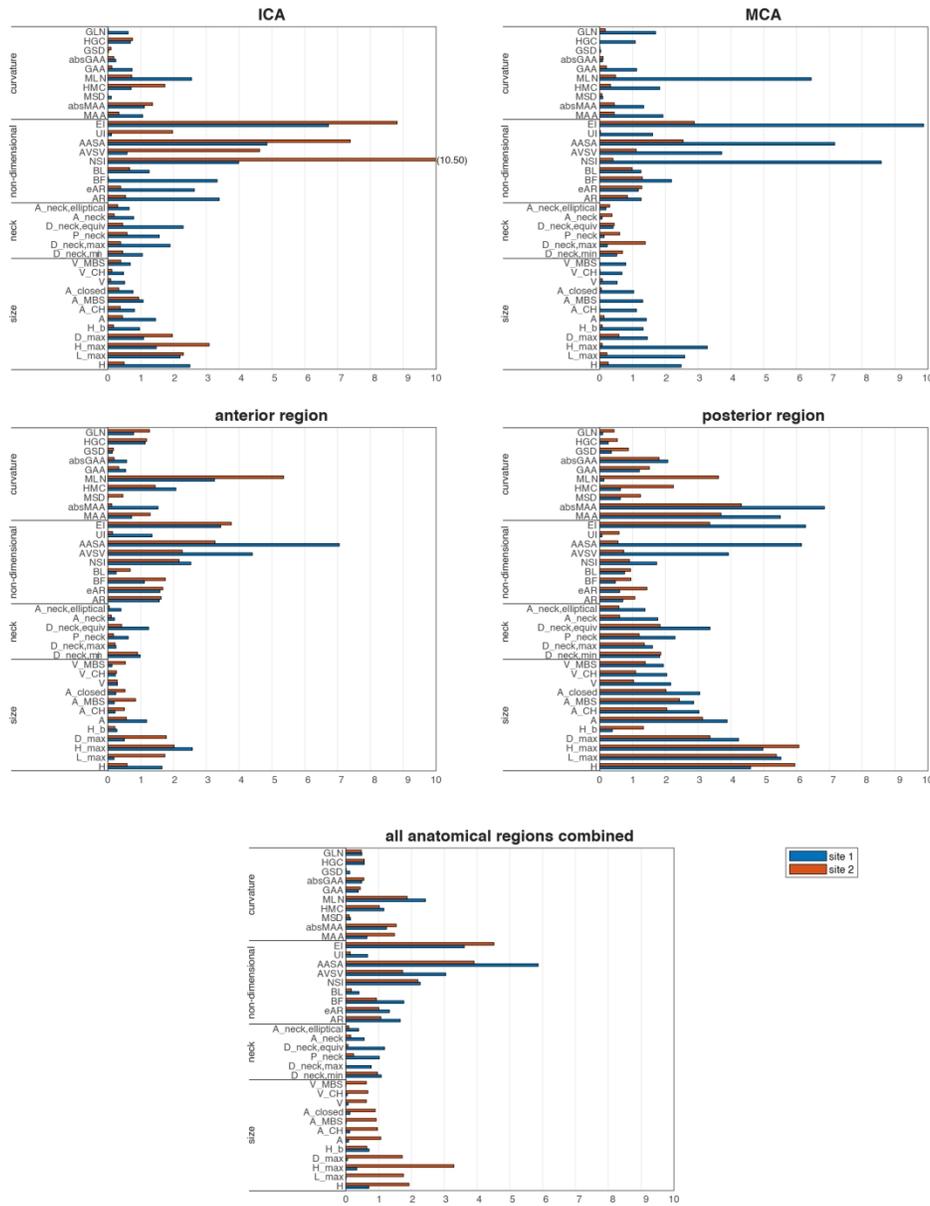
Figure 3: Pearson's r for correlation between geometric risk parameters by anatomical region for dataset 1.

Figure 4: Pearson's r for correlation between geometric risk parameters by anatomical region for dataset 2.

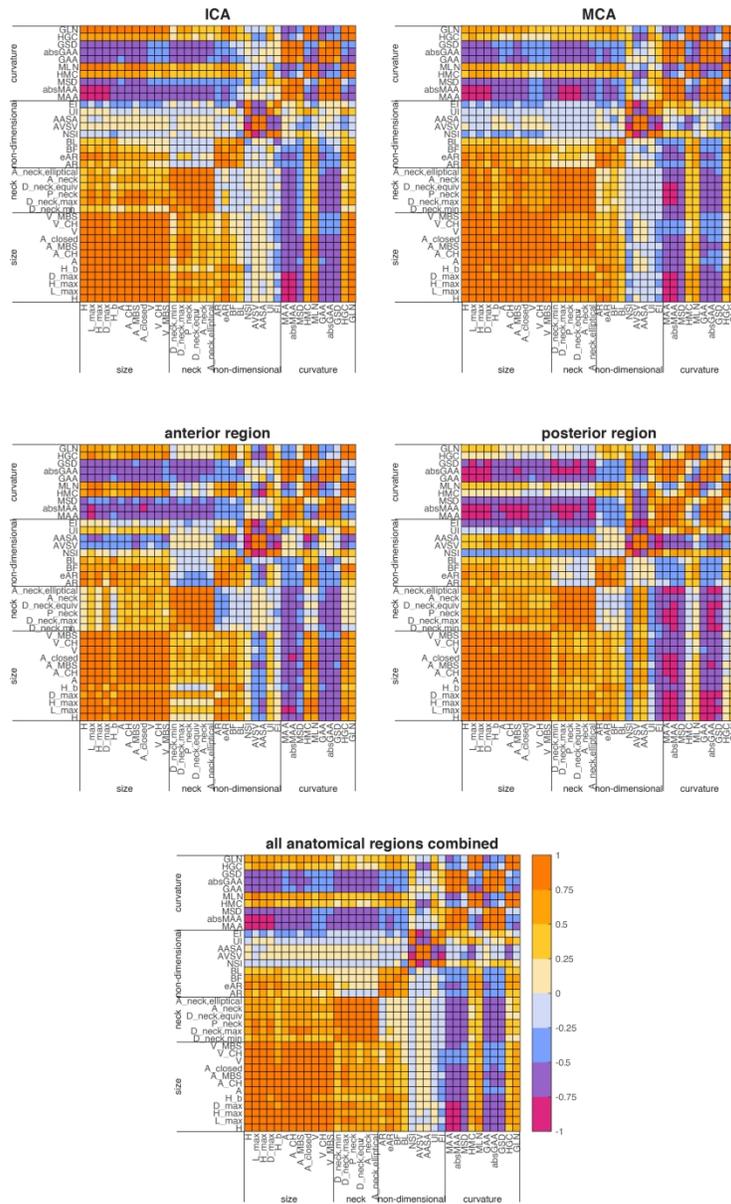
For peer review only



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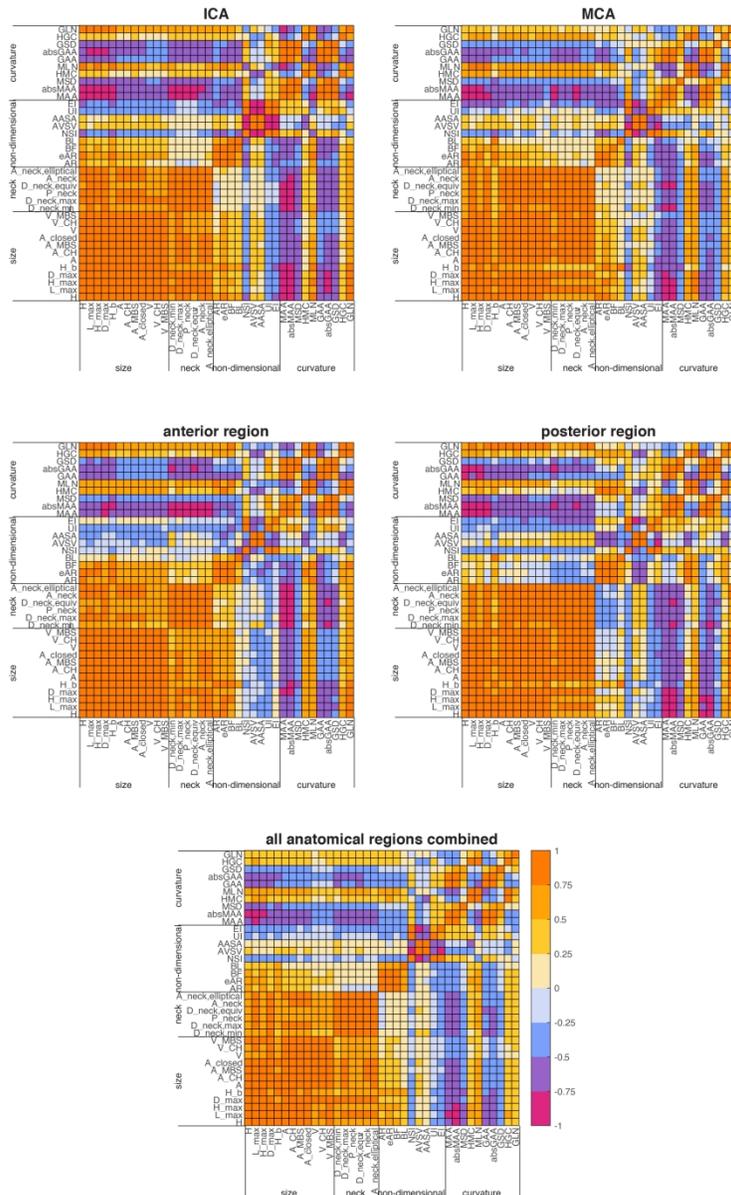


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	Pearson's r	H	L_max	H_max	D_max	H_b	A	A_CH
3	H	1.000	0.872	0.968	0.610	0.836	0.867	0.830
4	L_max	0.872	1.000	0.950	0.884	0.648	0.962	0.960
5	H_max	0.968	0.950	1.000	0.728	0.783	0.922	0.894
6	D_max	0.610	0.884	0.728	1.000	0.349	0.873	0.900
7	H_b	0.836	0.648	0.783	0.349	1.000	0.653	0.605
8	A	0.867	0.962	0.922	0.873	0.653	1.000	0.993
9	A_CH	0.830	0.960	0.894	0.900	0.605	0.993	1.000
10	A_MBS	0.835	0.973	0.919	0.863	0.596	0.967	0.957
11	A_closed	0.827	0.957	0.890	0.899	0.606	0.992	1.000
12	V	0.779	0.917	0.842	0.869	0.565	0.980	0.988
13	V_CH	0.778	0.924	0.846	0.880	0.548	0.982	0.988
14	V_MBS	0.769	0.918	0.857	0.822	0.522	0.934	0.919
15	D_neck,mir	0.220	0.402	0.246	0.535	0.125	0.415	0.484
16	D_neck,ma	0.153	0.466	0.248	0.642	-0.049	0.426	0.520
17	P_neck	0.059	0.376	0.158	0.554	-0.075	0.353	0.454
18	D_neck,eqt	0.159	0.428	0.224	0.609	-0.014	0.417	0.508
19	A_neck	0.089	0.392	0.170	0.583	-0.064	0.390	0.491
20	A_neck,elli	0.179	0.448	0.240	0.630	0.028	0.450	0.541
21	AR	0.867	0.582	0.784	0.236	0.849	0.579	0.503
22	eAR	0.879	0.639	0.819	0.304	0.801	0.608	0.536
23	BF	0.701	0.727	0.749	0.684	0.595	0.735	0.682
24	BL	0.627	0.461	0.580	0.273	0.884	0.464	0.423
25	NSI	0.173	0.275	0.235	0.216	-0.021	0.142	0.129
26	AVSV	-0.393	-0.491	-0.481	-0.331	-0.275	-0.315	-0.287
27	AASA	-0.455	-0.558	-0.551	-0.378	-0.337	-0.380	-0.350
28	UI	0.405	0.494	0.463	0.437	0.137	0.365	0.356
29	EI	0.012	0.091	0.067	0.013	-0.075	-0.034	-0.050
30	MAA	-0.661	-0.763	-0.698	-0.727	-0.481	-0.702	-0.740
31	absMAA	-0.692	-0.755	-0.711	-0.701	-0.547	-0.710	-0.747
32	MSD	-0.504	-0.453	-0.465	-0.370	-0.517	-0.489	-0.513
33	HMC	0.672	0.801	0.776	0.698	0.434	0.706	0.672
34	MLN	0.727	0.775	0.790	0.706	0.500	0.745	0.704
35	GAA	-0.627	-0.693	-0.655	-0.632	-0.443	-0.590	-0.621
36	absGAA	-0.647	-0.688	-0.659	-0.626	-0.534	-0.639	-0.672
37	GSD	-0.547	-0.567	-0.541	-0.507	-0.511	-0.550	-0.584
38	HGC	0.618	0.783	0.727	0.735	0.322	0.710	0.685
39	GLN	0.614	0.729	0.698	0.731	0.300	0.711	0.681

	A_MBS	A_closed	V	V_CH	V_MBS	D_neck,min	D_neck,max	P_neck
1								
2								
3	0.835	0.827	0.779	0.778	0.769	0.220	0.153	0.059
4	0.973	0.957	0.917	0.924	0.918	0.402	0.466	0.376
5	0.919	0.890	0.842	0.846	0.857	0.246	0.248	0.158
6	0.863	0.899	0.869	0.880	0.822	0.535	0.642	0.554
7	0.596	0.606	0.565	0.548	0.522	0.125	-0.049	-0.075
8	0.967	0.992	0.980	0.982	0.934	0.415	0.426	0.353
9	0.957	1.000	0.988	0.988	0.919	0.484	0.520	0.454
10	1.000	0.952	0.939	0.953	0.984	0.346	0.375	0.290
11	0.952	1.000	0.989	0.988	0.913	0.494	0.526	0.462
12	0.939	0.989	1.000	0.998	0.920	0.486	0.503	0.457
13	0.953	0.988	0.998	1.000	0.940	0.460	0.485	0.430
14	0.984	0.913	0.920	0.940	1.000	0.298	0.302	0.223
15	0.346	0.494	0.486	0.460	0.298	1.000	0.685	0.681
16	0.375	0.526	0.503	0.485	0.302	0.685	1.000	0.952
17	0.290	0.462	0.457	0.430	0.223	0.681	0.952	1.000
18	0.361	0.516	0.504	0.485	0.310	0.907	0.870	0.857
19	0.321	0.500	0.503	0.477	0.263	0.780	0.944	0.974
20	0.377	0.550	0.543	0.517	0.316	0.909	0.909	0.886
21	0.568	0.498	0.454	0.459	0.527	-0.127	-0.328	-0.375
22	0.610	0.529	0.473	0.480	0.553	-0.208	-0.214	-0.304
23	0.753	0.675	0.643	0.668	0.743	0.043	-0.096	-0.153
24	0.362	0.427	0.370	0.348	0.268	0.087	-0.061	-0.064
25	0.334	0.113	0.080	0.131	0.361	-0.197	-0.061	-0.176
26	-0.501	-0.273	-0.225	-0.261	-0.486	0.179	0.068	0.160
27	-0.558	-0.337	-0.288	-0.320	-0.535	0.160	0.041	0.130
28	0.494	0.340	0.273	0.321	0.477	-0.152	0.134	-0.008
29	0.166	-0.065	-0.072	-0.032	0.209	-0.227	-0.193	-0.269
30	-0.636	-0.743	-0.667	-0.654	-0.529	-0.582	-0.679	-0.648
31	-0.627	-0.752	-0.683	-0.661	-0.516	-0.646	-0.664	-0.637
32	-0.379	-0.521	-0.510	-0.474	-0.310	-0.620	-0.396	-0.402
33	0.801	0.661	0.604	0.639	0.770	-0.028	0.133	-0.011
34	0.753	0.697	0.631	0.658	0.708	-0.009	0.127	-0.014
35	-0.547	-0.622	-0.527	-0.520	-0.433	-0.446	-0.584	-0.543
36	-0.551	-0.678	-0.607	-0.582	-0.440	-0.652	-0.603	-0.580
37	-0.453	-0.592	-0.545	-0.515	-0.360	-0.695	-0.549	-0.547
38	0.811	0.672	0.627	0.670	0.805	-0.029	0.180	0.038
39	0.748	0.672	0.626	0.664	0.737	-0.038	0.158	0.024
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	D_neck, equi	A_neck	A_neck, ellipt	AR	eAR	BF	BL	NSI
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3	0.159	0.089	0.179	0.867	0.879	0.701	0.627	0.173
4	0.428	0.392	0.448	0.582	0.639	0.727	0.461	0.275
5	0.224	0.170	0.240	0.784	0.819	0.749	0.580	0.235
6	0.609	0.583	0.630	0.236	0.304	0.684	0.273	0.216
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8	-0.014	-0.064	0.028	0.849	0.801	0.595	0.884	-0.021
9	0.417	0.390	0.450	0.579	0.608	0.735	0.464	0.142
10	0.508	0.491	0.541	0.503	0.536	0.682	0.423	0.129
11	0.361	0.321	0.377	0.568	0.610	0.753	0.362	0.334
12	0.516	0.500	0.550	0.498	0.529	0.675	0.427	0.113
13	0.504	0.503	0.543	0.454	0.473	0.643	0.370	0.080
14	0.485	0.477	0.517	0.459	0.480	0.668	0.348	0.131
15	0.310	0.263	0.316	0.527	0.553	0.743	0.268	0.361
16	0.907	0.780	0.909	-0.127	-0.208	0.043	0.087	-0.197
17	0.870	0.944	0.909	-0.328	-0.214	-0.096	-0.061	-0.061
18	0.857	0.974	0.886	-0.375	-0.304	-0.153	-0.064	-0.176
19	1.000	0.927	0.953	-0.267	-0.298	-0.034	-0.040	-0.113
20	0.927	1.000	0.949	-0.353	-0.317	-0.119	-0.074	-0.157
21	0.953	0.949	1.000	-0.266	-0.247	-0.036	0.004	-0.155
22	-0.267	-0.353	-0.266	1.000	0.946	0.687	0.672	0.175
23	-0.298	-0.317	-0.247	0.946	1.000	0.669	0.627	0.253
24	-0.034	-0.119	-0.036	0.687	0.669	1.000	0.525	0.300
25	-0.040	-0.074	0.004	0.672	0.627	0.525	1.000	-0.267
26	-0.113	-0.157	-0.155	0.175	0.253	0.300	-0.267	1.000
27	0.141	0.175	0.161	-0.403	-0.468	-0.491	-0.075	-0.823
28	0.129	0.153	0.138	-0.450	-0.524	-0.532	-0.148	-0.751
29	0.019	-0.021	-0.047	0.320	0.427	0.442	-0.027	0.824
30	-0.219	-0.243	-0.226	0.085	0.141	0.157	-0.325	0.922
31	-0.656	-0.622	-0.632	-0.337	-0.379	-0.384	-0.446	0.044
32	-0.678	-0.632	-0.667	-0.377	-0.393	-0.371	-0.492	0.103
33	-0.516	-0.461	-0.553	-0.319	-0.252	-0.158	-0.456	0.370
34	0.017	-0.024	0.030	0.536	0.649	0.764	0.318	0.542
35	0.022	-0.028	0.035	0.591	0.685	0.804	0.463	0.314
36	-0.543	-0.499	-0.495	-0.365	-0.417	-0.365	-0.436	-0.045
37	-0.634	-0.575	-0.635	-0.368	-0.375	-0.327	-0.513	0.183
38	-0.631	-0.563	-0.640	-0.296	-0.265	-0.203	-0.488	0.303
39	0.077	0.033	0.055	0.449	0.560	0.753	0.186	0.602
40	0.064	0.022	0.042	0.453	0.551	0.779	0.234	0.427
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	AVSV	AASA	UI	EI	MAA	absMAA	MSD	HMC
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3	-0.393	-0.455	0.405	0.012	-0.661	-0.692	-0.504	0.672
4	-0.491	-0.558	0.494	0.091	-0.763	-0.755	-0.453	0.801
5	-0.481	-0.551	0.463	0.067	-0.698	-0.711	-0.465	0.776
6	-0.331	-0.378	0.437	0.013	-0.727	-0.701	-0.370	0.698
7	-0.275	-0.337	0.137	-0.075	-0.481	-0.547	-0.517	0.434
8	-0.315	-0.380	0.365	-0.034	-0.702	-0.710	-0.489	0.706
9	-0.287	-0.350	0.356	-0.050	-0.740	-0.747	-0.513	0.672
10	-0.501	-0.558	0.494	0.166	-0.636	-0.627	-0.379	0.801
11	-0.273	-0.337	0.340	-0.065	-0.743	-0.752	-0.521	0.661
12	-0.225	-0.288	0.273	-0.072	-0.667	-0.683	-0.510	0.604
13	-0.261	-0.320	0.321	-0.032	-0.654	-0.661	-0.474	0.639
14	-0.486	-0.535	0.477	0.209	-0.529	-0.516	-0.310	0.770
15	0.179	0.160	-0.152	-0.227	-0.582	-0.646	-0.620	-0.028
16	0.068	0.041	0.134	-0.193	-0.679	-0.664	-0.396	0.133
17	0.160	0.130	-0.008	-0.269	-0.648	-0.637	-0.402	-0.011
18	0.141	0.129	0.019	-0.219	-0.656	-0.678	-0.516	0.017
19	0.175	0.153	-0.021	-0.243	-0.622	-0.632	-0.461	-0.024
20	0.161	0.138	-0.047	-0.226	-0.632	-0.667	-0.553	0.030
21	-0.403	-0.450	0.320	0.085	-0.337	-0.377	-0.319	0.536
22	-0.468	-0.524	0.427	0.141	-0.379	-0.393	-0.252	0.649
23	-0.491	-0.532	0.442	0.157	-0.384	-0.371	-0.158	0.764
24	-0.075	-0.148	-0.027	-0.325	-0.446	-0.492	-0.456	0.318
25	-0.823	-0.751	0.824	0.922	0.044	0.103	0.370	0.542
26	1.000	0.988	-0.699	-0.776	0.120	0.070	-0.205	-0.736
27	0.988	1.000	-0.667	-0.702	0.177	0.129	-0.138	-0.785
28	-0.699	-0.667	1.000	0.556	-0.297	-0.203	0.211	0.706
29	-0.776	-0.702	0.556	1.000	0.257	0.273	0.377	0.341
30	0.120	0.177	-0.297	0.257	1.000	0.974	0.558	-0.424
31	0.070	0.129	-0.203	0.273	0.974	1.000	0.709	-0.339
32	-0.205	-0.138	0.211	0.377	0.558	0.709	1.000	0.032
33	-0.736	-0.785	0.706	0.341	-0.424	-0.339	0.032	1.000
34	-0.488	-0.536	0.586	0.075	-0.511	-0.427	0.009	0.912
35	0.207	0.254	-0.399	0.184	0.968	0.923	0.460	-0.446
36	0.021	0.088	-0.094	0.314	0.933	0.973	0.764	-0.290
37	-0.118	-0.050	0.060	0.393	0.798	0.880	0.904	-0.119
38	-0.689	-0.718	0.778	0.366	-0.422	-0.320	0.097	0.961
39	-0.487	-0.516	0.661	0.173	-0.452	-0.345	0.122	0.881
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3		0.727	-0.627	-0.647	-0.547	0.618	0.614
4		0.775	-0.693	-0.688	-0.567	0.783	0.729
5		0.790	-0.655	-0.659	-0.541	0.727	0.698
6		0.706	-0.632	-0.626	-0.507	0.735	0.731
7		0.500	-0.443	-0.534	-0.511	0.322	0.300
8		0.745	-0.590	-0.639	-0.550	0.710	0.711
9		0.704	-0.621	-0.672	-0.584	0.685	0.681
10		0.753	-0.547	-0.551	-0.453	0.811	0.748
11		0.697	-0.622	-0.678	-0.592	0.672	0.672
12		0.631	-0.527	-0.607	-0.545	0.627	0.626
13		0.658	-0.520	-0.582	-0.515	0.670	0.664
14		0.708	-0.433	-0.440	-0.360	0.805	0.737
15		-0.009	-0.446	-0.652	-0.695	-0.029	-0.038
16		0.127	-0.584	-0.603	-0.549	0.180	0.158
17		-0.014	-0.543	-0.580	-0.547	0.038	0.024
18		0.022	-0.543	-0.634	-0.631	0.077	0.064
19		-0.028	-0.499	-0.575	-0.563	0.033	0.022
20		0.035	-0.495	-0.635	-0.640	0.055	0.042
21		0.591	-0.365	-0.368	-0.296	0.449	0.453
22		0.685	-0.417	-0.375	-0.265	0.560	0.551
23		0.804	-0.365	-0.327	-0.203	0.753	0.779
24		0.463	-0.436	-0.513	-0.488	0.186	0.234
25		0.314	-0.045	0.183	0.303	0.602	0.427
26		-0.488	0.207	0.021	-0.118	-0.689	-0.487
27		-0.536	0.254	0.088	-0.050	-0.718	-0.516
28		0.586	-0.399	-0.094	0.060	0.778	0.661
29		0.075	0.184	0.314	0.393	0.366	0.173
30		-0.511	0.968	0.933	0.798	-0.422	-0.452
31		-0.427	0.923	0.973	0.880	-0.320	-0.345
32		0.009	0.460	0.764	0.904	0.097	0.122
33		0.912	-0.446	-0.290	-0.119	0.961	0.881
34		1.000	-0.519	-0.372	-0.166	0.886	0.941
35		-0.519	1.000	0.888	0.724	-0.438	-0.459
36		-0.372	0.888	1.000	0.937	-0.231	-0.256
37		-0.166	0.724	0.937	1.000	-0.051	-0.034
38		0.886	-0.438	-0.231	-0.051	1.000	0.939
39		0.941	-0.459	-0.256	-0.034	0.939	1.000
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unit	-	-	-	-	-	1=ruptured	mm
1	1	Berlin	Berlin	AComA	anterior	1	5.748
2	2	Berlin	Berlin	PComA	posterior	0	8.261
3	3	Berlin	Berlin	PICA	posterior	1	6.023
4	4	Berlin	Berlin	AComA	anterior	1	5.698
5	5	Berlin	Berlin	ACA	anterior	0	5.667
6	6	Berlin	Berlin	MCA	MCA	0	2.849
7	7	Berlin	Berlin	ICA	ICA	0	19.575
8	8	Berlin	Berlin	MCA	MCA	0	4.199
9	9	Berlin	Berlin	MCA	MCA	0	3.795
10	10	Berlin	Berlin	AComA	anterior	1	5.051
11	11	Berlin	Berlin	MCA	MCA	0	6.789
12	12	Berlin	Berlin	ICA	ICA	1	7.610
13	13	Berlin	Berlin	MCA	MCA	0	8.157
14	14	Berlin	Berlin	AComA	anterior	1	2.542
15	15	Berlin	Berlin	PComA	posterior	1	3.196
16	16A	Berlin	Berlin	ICA	ICA	1	9.587
17	16B	Berlin	Berlin	ACA	anterior	0	1.879
18	17A	Berlin	Berlin	ICA	ICA	0	12.261
19	17B	Berlin	Berlin	ICA	ICA	0	2.791
20	17C	Berlin	Berlin	AComA	anterior	0	4.530
21	18	Berlin	Berlin	MCA	MCA	1	5.597
22	19	Berlin	Berlin	AComA	anterior	1	5.177
23	20	Berlin	Berlin	PComA	posterior	1	10.569
24	21	Berlin	Berlin	ICA	ICA	0	4.966
25	22	Berlin	Berlin	ICA	ICA	0	7.908
26	23	Berlin	Berlin	MCA	MCA	1	4.598
27	24	Berlin	Berlin	ICA	ICA	0	2.906
28	25	Berlin	Berlin	BA	posterior	0	8.473
29	26	Berlin	Berlin	MCA	MCA	1	4.210
30	27	Berlin	Berlin	AComA	anterior	1	4.597
31	28	Berlin	Berlin	MCA	MCA	1	5.480
32	29	Berlin	Berlin	ICA	ICA	0	12.780
33	30A	Berlin	Berlin	ICA	ICA	0	4.078
34	30B	Berlin	Berlin	AComA	anterior	0	3.135
35	30C	Berlin	Berlin	AComA	anterior	1	5.085
36	30D	Berlin	Berlin	MCA	MCA	0	2.715
37	30E	Berlin	Berlin	PICA	posterior	1	4.983
38	31	Berlin	Berlin	MCA	MCA	0	4.542
39	32	Berlin	Berlin	ICA	ICA	0	9.475
40	33	Berlin	Berlin	AComA	anterior	1	6.212
41	34	Berlin	Berlin	AComA	anterior	0	3.383
42	35	Berlin	Berlin	ICA	ICA	1	11.690
43	36	Berlin	Berlin	BA	posterior	0	20.748
44	37	Berlin	Berlin	AComA	anterior	1	5.543
45	38	Berlin	Berlin	AComA	anterior	0	8.400
46	39	Berlin	Berlin	ICA	ICA	1	4.290
47	40	Berlin	Berlin	PComA	posterior	1	13.786

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2	41	Berlin	Berlin	ACoMA	anterior	1	4.301
3	42	Berlin	Berlin	PCoMA	posterior	0	5.891
4	43	Berlin	Berlin	ICA	ICA	0	6.872
5	44	Berlin	Berlin	PICA	posterior	1	4.213
6	45A	Berlin	Berlin	ICA	ICA	0	2.414
7	45B	Berlin	Berlin	ICA	ICA	1	3.501
8	45C	Berlin	Berlin	ICA	ICA	0	2.297
9	46	Berlin	Berlin	BA	posterior	0	11.175
10	47	Berlin	Berlin	ICA	ICA	0	4.636
11	48	Berlin	Berlin	MCA	MCA	0	2.204
12	49	Berlin	Berlin	MCA	MCA	1	16.986
13	50	Berlin	Berlin	PCoMA	posterior	1	7.588
14	51	Berlin	Berlin	ACoMA	anterior	0	5.047
15	52	Berlin	Berlin	ACA	anterior	1	2.779
16	53	Berlin	Berlin	AChA	ICA	1	6.830
17	54	Berlin	Berlin	PCoMA	posterior	1	4.857
18	55	Berlin	Berlin	ACoMA	anterior	0	3.330
19	56	Berlin	Berlin	MCA	MCA	1	2.092
20	57A	Berlin	Berlin	ICA	ICA	0	2.831
21	57B	Berlin	Berlin	ICA	ICA	0	4.277
22	57C	Berlin	Berlin	ICA	ICA	0	4.910
23	57D	Berlin	Berlin	ACoMA	anterior	1	2.565
24	57E	Berlin	Berlin	MCA	MCA	0	6.612
25	57F	Berlin	Berlin	MCA	MCA	0	1.536
26	57G	Berlin	Berlin	MCA	MCA	0	3.139
27	58	Berlin	Berlin	PCoMA	posterior	1	3.998
28	59	Berlin	Berlin	ICA	ICA	0	4.875
29	60A	Berlin	Berlin	MCA	MCA	0	8.547
30	60B	Berlin	Berlin	MCA	MCA	0	3.172
31	61	Berlin	Berlin	ACoMA	anterior	1	10.866
32	62	Berlin	Berlin	ICA	ICA	1	4.541
33	63	Berlin	Berlin	ACoMA	anterior	1	5.524
34	64	Berlin	Berlin	ICA	ICA	1	13.839
35	65	Berlin	Berlin	ICA	ICA	0	7.768
36	66	Berlin	Berlin	ACoMA	anterior	1	3.652
37	67	Berlin	Berlin	MCA	MCA	1	4.031
38	68	Berlin	Berlin	ACoMA	anterior	1	2.672
39	69	Berlin	Berlin	ICA	ICA	0	11.746
40	70	Berlin	Berlin	ACoMA	anterior	1	2.739
41	71	Berlin	Berlin	PCoMA	posterior	0	3.684
42	72A	Berlin	Berlin	PCoMA	posterior	0	9.969
43	72B	Berlin	Berlin	ACoMA	anterior	0	3.769
44	73	Berlin	Berlin	ACoMA	anterior	1	7.640
45	74	Berlin	Berlin	ICA	ICA	0	2.422
46	75A	Berlin	Berlin	PCoMA	posterior	0	2.277
47	75B	Berlin	Berlin	BA	posterior	1	4.556
48	76	Berlin	Berlin	PCoMA	posterior	1	4.974
49	77	Berlin	Berlin	MCA	MCA	0	10.165
50	78	Berlin	Berlin	MCA	MCA	0	5.020
51	79	Berlin	Berlin	ICA	ICA	0	9.202
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2	80	Berlin	Berlin	AComA	anterior	1	8.132
3	81	Berlin	Berlin	ICA	ICA	0	21.514
4	82A	Berlin	Berlin	ICA	ICA	0	2.039
5	82B	Berlin	Berlin	MCA	MCA	0	3.698
6	82C	Berlin	Berlin	ACA	anterior	0	1.486
7	83	Berlin	Berlin	PComA	posterior	0	10.503
8	84A	Berlin	Berlin	ICA	ICA	0	6.331
9	84B	Berlin	Berlin	MCA	MCA	0	3.509
10	85	Berlin	Berlin	MCA	MCA	0	2.996
11	86	Berlin	Berlin	MCA	MCA	0	2.575
12	87	Berlin	Berlin	AComA	anterior	1	3.971
13	88A	Berlin	Berlin	MCA	MCA	0	1.489
14	88B	Berlin	Berlin	MCA	MCA	0	2.304
15	89	Berlin	Berlin	ICA	ICA	0	5.728
16	90	Berlin	Berlin	MCA	MCA	0	4.016
17	91	Berlin	Berlin	AComA	anterior	0	6.147
18	92	Berlin	Berlin	PComA	posterior	0	7.023
19	93	Berlin	Berlin	PComA	posterior	1	10.373
20	94	Berlin	Berlin	MCA	MCA	0	19.183
21	95	Berlin	Berlin	AComA	anterior	1	6.261
22	96	Berlin	Berlin	ICA	ICA	0	5.202
23	97A	Berlin	Berlin	ICA	ICA	0	1.702
24	97B	Berlin	Berlin	AComA	anterior	0	5.381
25	98	Berlin	Berlin	PICA	posterior	1	4.524
26	99	Berlin	Berlin	PComA	posterior	0	6.067
27	100A	Berlin	Berlin	MCA	MCA	1	6.738
28	100B	Berlin	Berlin	ICA	ICA	0	2.364
29	100C	Berlin	Berlin	ICA	ICA	0	8.467
30	100D	Berlin	Berlin	MCA	MCA	0	2.488
31	100E	Berlin	Berlin	MCA	MCA	0	1.914
32	101	Berlin	Berlin	PComA	posterior	1	5.048
33	102	Berlin	Berlin	AComA	anterior	1	5.931
34	103	Berlin	Berlin	PCA	posterior	1	5.602
35	104	Berlin	Berlin	MCA	MCA	0	4.629
36	105	Berlin	Berlin	ICA	ICA	1	7.092
37	106	Berlin	Berlin	MCA	MCA	1	8.177
38	107	Berlin	Berlin	PComA	posterior	1	8.598
39	108	Berlin	Berlin	AComA	anterior	1	3.886
40	109	Berlin	Berlin	BA	posterior	1	13.918
41	110	Berlin	Berlin	BA	posterior	0	12.591
42	111	Berlin	Berlin	AComA	anterior	0	6.025
43	112	Berlin	Berlin	BA	posterior	1	7.000
44	113A	Berlin	Berlin	MCA	MCA	0	9.488
45	113B	Berlin	Berlin	MCA	MCA	0	6.242
46	114	Berlin	Berlin	MCA	MCA	1	3.622
47	115A	Hanover	Magdeburg	MCA	MCA	1	4.340
48	115B	Hanover	Magdeburg	MCA	MCA	0	1.149
49	116A	Hanover	Magdeburg	AComA	anterior	1	4.055
50	116B	Hanover	Magdeburg	AComA	anterior	0	1.031
51	117A	Hanover	Magdeburg	BA	posterior	1	8.476
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2	117B	Hanover	Magdeburg	ACoMA	anterior	0	4.088
3	118A	Hanover	Magdeburg	ACoMA	anterior	0	5.039
4	118B	Hanover	Magdeburg	PCoMA	posterior	1	4.528
5	119	Hanover	Magdeburg	MCA	MCA	1	1.132
6	120A	Hanover	Magdeburg	MCA	MCA	1	4.881
7	120B	Hanover	Magdeburg	ICA	ICA	1	2.325
8	121	Hanover	Magdeburg	ICA	ICA	1	18.704
9	122	Hanover	Magdeburg	ICA	ICA	0	6.667
10	123A	Hanover	Magdeburg	PCoMA	posterior	1	5.230
11	123B	Hanover	Magdeburg	MCA	MCA	0	2.984
12	124A	Hanover	Magdeburg	ACA	anterior	1	2.914
13	124B	Hanover	Magdeburg	ACoMA	anterior	0	1.201
14	124C	Hanover	Magdeburg	ACoMA	anterior	0	2.671
15	125	Hanover	Magdeburg	ICA	ICA	0	7.204
16	126A	Hanover	Magdeburg	MCA	MCA	1	8.466
17	126B	Hanover	Magdeburg	MCA	MCA	0	5.410
18	127A	Hanover	Magdeburg	ACoMA	anterior	1	2.663
19	127B	Hanover	Magdeburg	MCA	MCA	0	2.098
20	128A	Hanover	Magdeburg	ICA	ICA	1	1.429
21	128B	Hanover	Magdeburg	ICA	ICA	0	1.275
22	129A	Hanover	Magdeburg	BA	posterior	1	2.818
23	129B	Hanover	Magdeburg	SCA	posterior	0	1.293
24	130A	Hanover	Magdeburg	MCA	MCA	1	7.171
25	130B	Hanover	Magdeburg	ACoMA	anterior	0	4.247
26	131A	Hanover	Magdeburg	BA	posterior	0	4.863
27	131B	Hanover	Magdeburg	BA	posterior	1	3.992
28	132A	Hanover	Magdeburg	PCoMA	posterior	0	4.359
29	132B	Hanover	Magdeburg	ACoMA	anterior	1	16.578
30	133A	Hanover	Magdeburg	BA	posterior	1	6.042
31	133B	Hanover	Magdeburg	ACoMA	anterior	0	3.105
32	134A	Hanover	Magdeburg	MCA	MCA	1	6.298
33	134B	Hanover	Magdeburg	MCA	MCA	0	3.067
34	135	Hanover	Magdeburg	ICA	ICA	0	2.406
35	136A	Kiel	Magdeburg	MCA	MCA	0	1.108
36	136B	Kiel	Magdeburg	MCA	MCA	0	6.352
37	137	Kiel	Magdeburg	MCA	MCA	0	3.274
38	138	Kiel	Magdeburg	MCA	MCA	0	4.033
39	139	Kiel	Magdeburg	MCA	MCA	0	6.259
40	140	Kiel	Magdeburg	MCA	MCA	0	10.513
41	141	Kiel	Magdeburg	MCA	MCA	0	8.471
42	142	Kiel	Magdeburg	MCA	MCA	0	6.008
43	143	Kiel	Magdeburg	MCA	MCA	0	5.184
44	144	Kiel	Magdeburg	MCA	MCA	0	10.421
45	145	Kiel	Magdeburg	MCA	MCA	0	8.720
46	146A	Kiel	Magdeburg	MCA	MCA	0	6.242
47	146B	Kiel	Magdeburg	ACA	anterior	0	2.012
48	147A	Kiel	Magdeburg	MCA	MCA	0	5.580
49	147B	Kiel	Magdeburg	MCA	MCA	0	0.684
50	147C	Kiel	Magdeburg	MCA	MCA	0	0.573
51	147D	Kiel	Magdeburg	ACA	anterior	0	3.651
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2	147E	Kiel	Magdeburg	AComA	anterior	0	1.213
3	147F	Kiel	Magdeburg	AComA	anterior	0	1.384
4	148	Kiel	Magdeburg	MCA	MCA	0	4.650
5	149	Kiel	Magdeburg	MCA	MCA	0	6.489
6	150	Kiel	Magdeburg	MCA	MCA	0	4.962
7	151	Kiel	Magdeburg	MCA	MCA	0	3.962
8	152	Magdeburg	Magdeburg	MCA	MCA	0	5.866
9	153	Magdeburg	Magdeburg	ACA	anterior	1	3.594
10	154	Magdeburg	Magdeburg	PComA	posterior	1	9.941
11	155A	Magdeburg	Magdeburg	AComA	anterior	1	2.543
12	155B	Magdeburg	Magdeburg	AComA	anterior	0	3.589
13	155C	Magdeburg	Magdeburg	MCA	MCA	0	5.120
14	156A	Magdeburg	Magdeburg	ICA	ICA	0	7.048
15	156B	Magdeburg	Magdeburg	ICA	ICA	0	1.214
16	156C	Magdeburg	Magdeburg	ICA	ICA	0	1.765
17	156D	Magdeburg	Magdeburg	ICA	ICA	0	2.037
18	157	Magdeburg	Magdeburg	VA	posterior	1	5.194
19	158	Magdeburg	Magdeburg	AChA	ICA	0	3.248
20	159	Magdeburg	Magdeburg	MCA	MCA	0	5.645
21	160A	Magdeburg	Magdeburg	AChA	ICA	1	2.988
22	160B	Magdeburg	Magdeburg	ICA	ICA	0	2.842
23	161A	Magdeburg	Magdeburg	ICA	ICA	1	5.684
24	161B	Magdeburg	Magdeburg	ICA	ICA	0	2.089
25	161C	Magdeburg	Magdeburg	PICA	posterior	0	2.497
26	162	Magdeburg	Magdeburg	AChA	ICA	1	4.811
27	163	Magdeburg	Magdeburg	ICA	ICA	0	4.981
28	164	Magdeburg	Magdeburg	MCA	MCA	0	3.817
29	165A	Magdeburg	Magdeburg	MCA	MCA	0	3.419
30	165B	Magdeburg	Magdeburg	PComA	posterior	0	5.533
31	165C	Magdeburg	Magdeburg	BA	posterior	0	2.856
32	165D	Magdeburg	Magdeburg	SCA	posterior	1	4.595
33	166	Magdeburg	Magdeburg	ICA	ICA	0	3.638
34	167	Magdeburg	Magdeburg	ICA	ICA	0	3.481
35	168	Magdeburg	Magdeburg	ICA	ICA	0	6.061
36	169	Magdeburg	Magdeburg	ICA	ICA	0	7.142
37	170	Magdeburg	Magdeburg	ICA	ICA	0	5.557
38	171	Magdeburg	Magdeburg	ICA	ICA	0	11.276
39	172A	Magdeburg	Magdeburg	AComA	anterior	1	3.283
40	172B	Magdeburg	Magdeburg	MCA	MCA	0	2.319
41	173A	Magdeburg	Magdeburg	MCA	MCA	1	4.176
42	173B	Magdeburg	Magdeburg	ICA	ICA	0	3.188
43	174	Magdeburg	Magdeburg	ICA	ICA	0	3.711
44	175	Magdeburg	Magdeburg	MCA	MCA	0	4.156
45	176	Magdeburg	Magdeburg	AComA	anterior	0	3.397
46	177A	Magdeburg	Magdeburg	PComA	posterior	1	6.322
47	177B	Magdeburg	Magdeburg	BA	posterior	0	1.516
48	178	Magdeburg	Magdeburg	MCA	MCA	1	5.269
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	maximum c	maximum h	maximum d	bulge height	surface area	convex hull	minimal box	closed area	volume
	L_max	H_max	D_max	H_b	A	A_CH	A_MBS	A_closed	V
	mm	mm	mm	mm	cm ²	cm ²	cm ²	cm ²	ml
5	6.629	5.790	5.713	0.877	0.887	1.018	1.495	1.003	0.083
6	11.888	8.544	10.931	3.003	2.391	2.722	4.652	2.537	0.269
7	7.306	6.133	4.862	0.313	0.742	0.914	1.677	0.888	0.064
8	7.867	6.544	7.165	3.567	1.018	1.146	1.979	1.122	0.097
9	7.336	6.315	6.104	1.929	0.888	1.022	1.749	1.014	0.085
10	6.275	4.482	5.783	0.575	0.693	0.906	1.269	0.900	0.074
11	23.888	20.508	23.475	9.621	12.495	13.243	18.371	13.239	4.106
12	6.597	4.534	6.403	1.473	0.746	0.934	1.422	0.924	0.076
13	5.837	3.939	5.183	0.070	0.568	0.802	1.099	0.795	0.060
14	6.518	5.449	5.861	2.398	0.713	0.822	1.338	0.809	0.059
15	8.495	6.902	7.441	3.391	1.540	1.813	2.341	1.803	0.215
16	11.246	9.797	10.200	3.153	1.755	1.899	3.981	1.853	0.195
17	11.394	8.611	10.972	4.429	2.218	2.475	4.079	2.459	0.334
18	7.308	4.479	7.292	0.287	0.574	0.844	1.684	0.826	0.059
19	4.672	3.411	4.157	0.033	0.354	0.489	0.729	0.486	0.027
20	13.627	11.834	11.081	4.341	3.153	3.480	5.839	3.381	0.526
21	2.875	1.899	2.875	0.057	0.126	0.180	0.276	0.178	0.006
22	14.303	12.591	12.333	6.473	3.921	4.285	6.591	4.242	0.730
23	3.763	2.874	3.382	1.302	0.281	0.342	0.445	0.341	0.018
24	5.669	4.725	4.473	2.104	0.553	0.648	1.015	0.643	0.044
25	7.910	6.289	6.673	3.770	1.024	1.175	1.970	1.151	0.101
26	6.439	5.233	5.830	1.474	0.815	0.991	1.327	0.978	0.081
27	12.632	11.229	10.859	3.425	3.001	3.307	5.029	3.293	0.523
28	8.453	6.020	7.820	1.936	0.987	1.244	2.245	1.236	0.112
29	9.521	8.035	9.229	3.504	2.125	2.439	2.878	2.433	0.344
30	8.530	5.733	7.294	1.949	1.050	1.420	2.328	1.397	0.132
31	4.793	3.005	4.741	0.075	0.310	0.479	0.797	0.470	0.025
32	14.667	10.280	13.848	1.293	4.122	5.440	6.782	5.419	1.129
33	7.677	4.990	6.526	2.190	0.873	1.094	1.890	1.060	0.085
34	8.500	5.691	8.412	2.083	1.088	1.325	2.270	1.310	0.124
35	10.420	6.548	10.246	2.938	1.204	1.480	3.411	1.377	0.112
36	15.754	13.711	11.401	3.704	3.516	3.937	7.802	3.868	0.564
37	6.137	4.508	5.343	2.007	0.663	0.820	1.184	0.817	0.063
38	6.677	3.854	6.460	1.201	0.590	0.769	1.402	0.757	0.054
39	6.751	5.481	4.736	1.330	0.577	0.716	1.432	0.696	0.045
40	3.661	2.760	3.246	1.172	0.232	0.303	0.424	0.301	0.014
41	6.655	5.163	5.034	1.727	0.691	0.832	1.391	0.823	0.062
42	8.135	5.839	7.993	1.423	1.186	1.438	2.167	1.417	0.142
43	16.986	10.740	15.845	2.213	5.926	6.882	9.209	6.869	1.564
44	7.950	6.713	6.080	1.989	1.030	1.244	2.022	1.224	0.108
45	5.212	3.563	5.005	0.689	0.483	0.669	0.895	0.665	0.046
46	12.891	11.777	8.932	5.558	2.584	2.875	5.260	2.844	0.398
47	24.926	21.090	22.734	9.915	14.654	15.321	19.652	15.279	5.424
48	8.946	6.977	8.075	2.268	1.298	1.555	2.541	1.527	0.157
49	14.786	10.742	14.206	1.633	2.875	3.216	6.868	3.132	0.407
50	6.715	5.085	5.948	1.913	0.712	0.843	1.420	0.839	0.066
51	15.827	13.957	14.042	6.937	5.487	5.906	7.992	5.870	1.249

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2	6.419	4.551	6.134	0.624	0.618	0.839	1.316	0.813	0.058
3	8.062	6.217	6.768	2.455	1.126	1.368	2.042	1.365	0.137
4	17.188	10.658	16.238	2.250	3.236	4.445	9.425	4.430	0.696
5	7.303	4.996	6.301	1.470	0.688	0.925	1.676	0.910	0.072
6	4.605	2.692	4.603	0.037	0.296	0.466	0.713	0.462	0.023
7	4.605	3.619	3.564	1.963	0.355	0.438	0.677	0.430	0.023
8	4.653	2.599	4.537	0.354	0.303	0.480	0.698	0.475	0.025
9	13.326	11.629	11.342	5.799	3.546	3.816	5.596	3.800	0.658
10	7.105	4.947	6.019	0.113	0.678	0.891	1.586	0.882	0.061
11	4.777	2.888	4.516	0.482	0.282	0.439	0.727	0.433	0.023
12	18.334	17.219	14.463	8.226	5.638	6.064	10.560	5.978	1.232
13	11.513	9.974	11.050	4.580	2.241	2.481	4.240	2.396	0.285
14	6.880	5.489	6.061	2.068	0.829	0.999	1.492	0.993	0.086
15	4.149	2.840	3.778	0.926	0.297	0.384	0.541	0.382	0.021
16	11.234	7.779	10.623	2.600	2.129	2.279	3.965	2.254	0.282
17	6.535	5.085	5.126	0.262	0.507	0.706	1.400	0.685	0.041
18	6.195	3.881	6.006	0.616	0.577	0.840	1.210	0.829	0.061
19	4.282	2.759	3.841	0.151	0.216	0.331	0.590	0.325	0.013
20	5.968	3.703	5.938	1.423	0.517	0.678	1.119	0.668	0.043
21	4.773	4.310	4.200	2.368	0.467	0.513	0.771	0.506	0.031
22	9.479	6.686	9.469	2.116	1.305	1.446	2.823	1.429	0.139
23	4.362	2.739	4.165	0.197	0.326	0.447	0.600	0.445	0.025
24	7.928	6.831	6.578	2.903	1.256	1.465	2.026	1.456	0.154
25	2.798	1.593	2.792	0.014	0.105	0.170	0.266	0.167	0.005
26	6.330	3.703	6.047	0.954	0.580	0.806	1.259	0.803	0.058
27	7.668	6.509	6.943	1.249	0.852	1.054	1.873	0.999	0.070
28	8.038	5.767	7.357	1.708	0.972	1.152	2.030	1.143	0.103
29	13.384	9.880	12.864	3.835	3.174	3.751	5.854	3.690	0.603
30	4.583	3.361	4.077	0.084	0.364	0.502	0.704	0.498	0.030
31	13.573	12.129	7.940	6.398	2.411	2.619	5.788	2.564	0.328
32	6.253	4.782	5.560	2.596	0.679	0.785	1.232	0.782	0.060
33	6.774	5.738	4.776	1.687	0.752	0.882	1.467	0.876	0.070
34	19.580	14.862	19.183	7.524	7.554	7.889	12.044	7.851	1.917
35	10.702	7.977	8.927	2.139	2.019	2.495	3.606	2.481	0.325
36	6.698	4.629	5.540	0.489	0.576	0.764	1.410	0.757	0.055
37	6.354	4.692	5.177	1.312	0.626	0.795	1.289	0.776	0.053
38	6.204	3.207	6.016	0.114	0.413	0.706	1.215	0.694	0.044
39	14.376	13.009	10.934	6.325	2.638	2.994	6.492	2.830	0.343
40	6.016	4.460	5.142	0.926	0.678	0.873	1.149	0.866	0.071
41	5.832	3.890	5.511	0.286	0.536	0.691	1.071	0.684	0.046
42	14.708	12.119	12.964	4.615	3.419	3.829	6.796	3.791	0.609
43	5.100	3.825	4.479	0.525	0.452	0.611	0.840	0.603	0.038
44	10.529	8.923	7.517	2.011	1.266	1.421	3.483	1.355	0.113
45	6.886	3.607	6.764	0.185	0.510	0.851	1.490	0.837	0.060
46	4.974	3.155	4.670	0.739	0.312	0.487	0.792	0.479	0.026
47	6.182	5.235	3.884	2.072	0.422	0.503	1.203	0.487	0.025
48	8.405	5.927	8.296	2.748	1.255	1.408	2.270	1.385	0.133
49	15.254	10.492	15.251	1.120	3.825	4.559	7.665	4.507	0.804
50	7.735	5.096	7.199	1.289	0.956	1.265	1.925	1.236	0.115
51	11.062	9.776	9.388	5.048	2.352	2.598	3.900	2.577	0.353
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2	9.022	8.308	5.532	5.605	1.258	1.403	2.566	1.369	0.125
3	32.342	25.628	30.344	9.085	21.842	22.485	32.901	22.541	9.061
4	3.400	2.107	3.340	0.103	0.171	0.249	0.382	0.247	0.010
5	5.047	4.006	3.660	0.257	0.368	0.480	0.802	0.479	0.028
6	3.134	1.819	3.062	0.002	0.128	0.204	0.325	0.203	0.007
7	13.558	11.007	11.469	5.880	3.372	4.048	5.907	3.950	0.645
8	8.282	6.772	7.749	2.957	1.357	1.578	2.227	1.567	0.170
9	5.390	3.909	3.582	0.036	0.363	0.503	0.917	0.497	0.029
10	5.401	3.552	5.038	1.301	0.435	0.613	0.917	0.611	0.042
11	3.966	2.604	3.799	0.123	0.269	0.369	0.506	0.368	0.019
12	5.633	4.386	4.464	0.942	0.531	0.621	1.001	0.614	0.039
13	3.149	1.664	3.147	0.170	0.102	0.155	0.311	0.153	0.005
14	3.784	2.577	3.258	0.475	0.191	0.258	0.454	0.256	0.011
15	7.951	6.459	5.903	0.045	0.885	1.210	2.142	1.167	0.093
16	6.817	4.506	6.387	1.055	0.691	0.886	1.462	0.880	0.067
17	7.784	6.322	6.895	2.712	1.231	1.415	1.903	1.412	0.152
18	12.441	7.739	12.162	1.572	2.313	2.941	4.898	2.904	0.402
19	16.422	12.513	15.861	2.894	4.492	4.998	8.482	4.966	0.797
20	27.009	21.425	25.069	8.693	14.959	16.042	22.918	16.010	5.763
21	8.947	7.350	6.990	2.234	1.135	1.351	2.515	1.341	0.128
22	13.291	8.491	13.104	0.615	2.474	3.251	5.883	3.166	0.379
23	5.671	2.993	5.671	0.100	0.283	0.495	1.011	0.489	0.019
24	8.214	5.554	7.968	1.932	1.237	1.574	2.124	1.572	0.170
25	5.584	4.790	4.319	2.528	0.481	0.539	0.980	0.527	0.031
26	9.725	6.554	9.274	1.314	1.459	1.953	2.971	1.944	0.238
27	16.284	12.471	15.055	0.726	3.620	4.000	8.331	3.963	0.645
28	3.707	2.472	3.379	0.531	0.221	0.311	0.445	0.309	0.014
29	16.159	11.384	16.159	4.627	3.858	4.256	8.203	4.029	0.506
30	4.053	2.688	3.620	0.707	0.258	0.349	0.516	0.347	0.016
31	3.744	1.985	3.743	0.076	0.186	0.285	0.442	0.282	0.011
32	6.956	5.626	4.803	1.591	0.669	0.821	1.525	0.808	0.058
33	7.936	6.362	7.128	3.081	1.178	1.318	2.163	1.302	0.120
34	9.195	6.126	7.318	1.738	1.708	1.836	2.661	1.858	0.209
35	17.009	8.810	16.189	0.942	2.437	3.849	9.088	3.752	0.562
36	9.263	7.602	7.208	3.536	1.222	1.383	2.696	1.338	0.114
37	10.514	8.759	7.409	3.082	1.494	1.771	3.482	1.712	0.151
38	10.231	8.838	7.094	2.851	1.488	1.803	3.372	1.739	0.166
39	6.100	4.339	5.591	0.679	0.516	0.732	1.220	0.722	0.048
40	17.012	13.949	16.935	6.552	6.058	6.416	9.100	6.386	1.433
41	18.621	14.380	14.373	6.548	4.829	5.408	10.893	5.328	0.999
42	9.774	6.785	8.878	1.968	1.741	2.204	3.001	2.190	0.285
43	10.375	7.553	9.325	3.307	1.779	2.280	3.443	2.262	0.286
44	11.542	9.849	7.908	4.661	2.103	2.433	4.190	2.390	0.308
45	8.757	6.907	8.753	2.415	1.552	1.848	2.420	1.841	0.224
46	6.793	4.234	6.753	0.367	0.597	0.920	1.502	0.910	0.068
47	6.195	5.019	5.753	2.072	0.634	0.738	1.213	0.721	0.049
48	2.123	1.222	2.050	0.099	0.062	0.091	0.144	0.089	0.002
49	7.276	4.568	7.267	1.827	0.795	0.957	1.663	0.935	0.073
50	2.744	1.425	2.563	0.133	0.078	0.128	0.237	0.123	0.003
51	10.853	8.721	9.956	2.319	2.269	2.569	3.723	2.547	0.342
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2	6.386	4.271	6.267	1.450	0.622	0.798	1.282	0.779	0.052
3	7.385	6.025	5.712	3.287	0.847	0.981	1.714	0.961	0.077
4	6.224	4.693	5.826	1.532	0.584	0.710	1.218	0.686	0.040
5	2.739	1.458	2.699	0.000	0.079	0.137	0.248	0.129	0.003
6	6.758	5.613	6.202	3.057	0.747	0.850	1.552	0.826	0.060
7	8.335	5.295	8.154	0.578	0.472	0.673	2.182	0.626	0.032
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9	24.223	19.791	22.453	9.808	12.666	13.149	18.524	13.126	4.170
10	9.429	7.753	9.246	3.668	1.763	2.018	2.881	1.991	0.233
11	7.279	5.501	6.496	1.296	0.962	1.180	1.701	1.156	0.093
12	4.951	3.068	4.238	0.721	0.311	0.403	0.770	0.396	0.018
13	3.677	3.075	2.630	1.197	0.197	0.240	0.431	0.230	0.008
14	3.184	1.674	2.913	0.185	0.096	0.166	0.322	0.159	0.004
15	4.432	3.209	4.075	1.200	0.283	0.349	0.626	0.346	0.016
16	8.784	7.818	6.956	3.946	1.370	1.477	2.435	1.460	0.148
17	13.905	9.021	13.148	0.801	2.857	3.336	6.331	3.136	0.362
18	7.117	5.697	7.117	1.111	0.959	1.100	1.716	1.067	0.083
19	4.398	3.418	3.652	1.122	0.260	0.319	0.609	0.314	0.014
20	4.263	2.616	3.714	0.022	0.236	0.323	0.576	0.316	0.014
21	3.378	1.853	3.377	0.224	0.119	0.210	0.389	0.196	0.005
22	5.130	2.891	4.336	0.308	0.177	0.292	0.827	0.275	0.008
23	5.027	3.392	4.348	1.368	0.315	0.392	0.795	0.385	0.019
24	2.603	1.519	2.548	0.128	0.096	0.144	0.214	0.138	0.004
25	8.733	7.733	5.173	2.236	1.000	1.104	2.399	1.082	0.087
26	6.282	4.788	4.997	1.219	0.529	0.634	1.242	0.623	0.038
27	6.960	6.297	6.263	3.045	0.617	0.691	1.556	0.649	0.035
28	6.109	4.679	5.536	1.914	0.602	0.685	1.173	0.680	0.047
29	8.258	5.056	7.901	0.962	0.957	1.190	2.143	1.166	0.099
30	21.893	19.479	15.008	5.305	5.825	6.171	15.090	6.046	1.094
31	7.690	6.527	5.130	2.092	0.820	0.984	1.861	0.906	0.058
32	4.236	3.327	2.935	1.359	0.267	0.320	0.564	0.310	0.014
33	7.909	6.999	6.604	1.846	1.191	1.329	1.991	1.306	0.123
34	5.815	3.677	4.000	0.846	0.324	0.434	1.062	0.406	0.019
35	7.097	4.213	6.014	0.103	0.332	0.541	1.582	0.515	0.023
36	2.628	1.504	2.617	0.126	0.075	0.129	0.227	0.120	0.003
37	6.801	6.385	4.171	3.307	0.723	0.806	1.476	0.797	0.058
38	5.605	3.754	5.144	1.846	0.487	0.608	0.987	0.597	0.037
39	6.085	4.188	5.097	1.013	0.566	0.707	1.164	0.693	0.046
40	10.066	6.868	9.700	2.978	1.972	2.370	3.227	2.338	0.291
41	11.565	10.869	9.066	5.115	2.694	2.806	4.206	2.801	0.417
42	10.003	8.861	9.695	3.555	2.151	2.310	3.143	2.295	0.306
43	6.948	6.210	4.669	2.279	0.766	0.840	1.517	0.825	0.061
44	8.098	6.481	7.268	3.584	1.033	1.168	2.064	1.144	0.093
45	15.923	12.736	11.639	3.653	3.319	3.922	7.966	3.711	0.511
46	9.220	8.728	6.525	5.970	1.325	1.489	2.729	1.424	0.127
47	8.947	7.049	8.891	2.469	1.606	1.828	2.595	1.814	0.208
48	3.410	2.529	3.319	1.196	0.188	0.222	0.369	0.217	0.008
49	6.977	5.759	5.449	1.556	0.777	0.934	1.530	0.903	0.066
50	1.627	0.900	1.540	0.310	0.031	0.050	0.090	0.047	0.001
51	1.571	0.846	1.511	0.124	0.026	0.044	0.080	0.041	0.001
52	4.670	3.829	3.715	0.862	0.374	0.442	0.707	0.433	0.023
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2	2.495	1.472	2.180	0.087	0.072	0.103	0.196	0.100	0.002
3	2.449	1.457	2.325	0.046	0.086	0.131	0.194	0.125	0.003
4	9.599	6.040	9.240	1.954	1.225	1.478	2.895	1.465	0.128
5	7.998	6.644	5.913	3.660	1.019	1.183	2.072	1.148	0.100
6	7.328	5.848	5.773	2.070	0.814	0.905	1.687	0.887	0.066
7	6.486	5.072	6.312	0.846	0.639	0.755	1.334	0.750	0.052
8	7.722	6.054	7.580	2.357	1.147	1.296	1.910	1.270	0.117
9	4.784	3.869	4.102	1.291	0.329	0.390	0.719	0.383	0.019
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11	15.603	11.496	14.341	7.003	4.024	4.638	7.675	4.569	0.809
12	5.647	3.274	5.306	0.026	0.355	0.466	1.003	0.451	0.021
13	4.724	3.696	4.160	1.815	0.429	0.518	0.707	0.510	0.030
14	6.943	5.844	5.841	1.209	0.657	0.807	1.560	0.764	0.049
15	11.331	8.473	9.336	2.050	1.711	1.957	4.035	1.938	0.218
16	3.405	1.788	3.124	0.171	0.121	0.195	0.369	0.189	0.005
17	3.375	1.970	3.356	0.117	0.146	0.221	0.377	0.215	0.007
18	2.674	2.099	2.427	0.125	0.119	0.164	0.251	0.160	0.005
19	6.651	5.678	4.727	3.075	0.642	0.716	1.397	0.705	0.049
20	4.557	3.452	4.551	1.438	0.388	0.466	0.672	0.457	0.025
21	6.241	5.711	6.021	2.024	0.837	0.928	1.273	0.922	0.073
22	4.200	3.054	3.431	0.180	0.273	0.358	0.574	0.350	0.016
23	4.277	3.071	4.011	1.379	0.341	0.433	0.576	0.427	0.023
24	7.789	6.371	6.026	2.151	0.819	0.987	1.906	0.932	0.060
25	2.779	2.123	2.323	0.573	0.137	0.172	0.243	0.171	0.006
26	3.590	2.777	3.414	1.580	0.240	0.286	0.408	0.278	0.012
27	6.957	6.079	6.471	2.907	0.713	0.780	1.524	0.750	0.048
28	5.784	5.145	4.269	1.733	0.498	0.560	1.051	0.547	0.030
29	5.795	4.770	4.652	1.961	0.401	0.530	1.068	0.476	0.021
30	5.333	3.786	4.835	0.986	0.424	0.507	0.893	0.498	0.028
31	7.607	6.500	4.457	3.691	0.723	0.793	1.818	0.773	0.053
32	4.095	3.019	3.578	1.043	0.276	0.374	0.556	0.364	0.017
33	5.900	5.509	4.218	3.215	0.545	0.570	1.098	0.557	0.031
34	5.574	3.949	5.005	1.532	0.505	0.630	0.977	0.624	0.041
35	5.053	3.735	4.455	1.533	0.398	0.461	0.803	0.454	0.025
36	9.075	6.193	9.068	2.564	1.532	1.753	2.802	1.731	0.191
37	7.748	7.232	7.453	3.980	1.306	1.395	1.963	1.378	0.139
38	7.203	5.799	5.440	1.852	0.826	0.957	1.631	0.925	0.070
39	15.720	12.308	14.026	4.352	4.479	5.063	7.782	5.036	0.977
40	5.186	4.052	3.267	1.796	0.280	0.347	0.845	0.322	0.012
41	5.388	2.932	4.739	0.773	0.335	0.421	0.912	0.407	0.018
42	6.487	5.148	5.922	1.965	0.654	0.765	1.340	0.742	0.050
43	5.446	3.837	5.297	1.539	0.461	0.549	0.932	0.537	0.031
44	4.406	3.846	4.243	1.228	0.391	0.445	0.653	0.440	0.025
45	5.714	4.684	5.562	1.815	0.544	0.612	1.026	0.588	0.034
46	5.047	4.191	3.070	1.619	0.276	0.311	0.801	0.289	0.012
47	7.755	6.941	4.725	4.013	0.823	0.909	1.891	0.893	0.066
48	2.901	1.778	2.668	0.019	0.107	0.158	0.278	0.150	0.004
49	6.661	5.753	4.657	1.227	0.646	0.769	1.394	0.738	0.048
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	ml	ml	mm	mm	mm	mm	cm ²	cm ²	-
5	0.091	0.172	2.903	3.885	13.086	3.537	0.116	0.089	1.479
6	0.372	0.943	2.992	5.434	17.029	3.417	0.145	0.128	1.520
7	0.071	0.204	3.276	4.862	14.831	3.926	0.146	0.125	1.239
8	0.105	0.262	2.412	3.903	13.317	3.147	0.105	0.074	1.460
9	0.087	0.217	2.835	4.497	15.471	3.260	0.126	0.100	1.260
10	0.076	0.134	4.243	5.252	19.040	4.336	0.206	0.175	0.543
11	4.299	7.404	7.102	11.374	37.990	7.833	0.744	0.634	1.721
12	0.080	0.160	2.937	5.732	18.940	3.767	0.178	0.132	0.733
13	0.062	0.108	3.700	5.163	19.585	4.624	0.226	0.150	0.735
14	0.062	0.145	3.135	3.555	11.360	3.390	0.096	0.088	1.421
15	0.219	0.337	4.061	6.687	22.302	4.713	0.263	0.213	1.015
16	0.211	0.747	2.896	4.022	12.395	3.169	0.098	0.091	1.892
17	0.343	0.775	4.591	6.207	19.420	4.961	0.241	0.224	1.314
18	0.064	0.205	3.911	6.350	21.036	4.791	0.252	0.195	0.400
19	0.028	0.058	3.525	4.157	13.267	3.968	0.132	0.115	0.769
20	0.567	1.327	4.216	6.408	19.835	4.605	0.228	0.212	1.496
21	0.006	0.014	1.920	2.875	8.841	2.356	0.052	0.043	0.654
22	0.765	1.591	5.778	6.676	22.660	5.667	0.321	0.303	1.837
23	0.018	0.028	2.370	2.886	9.061	2.653	0.060	0.054	0.967
24	0.045	0.096	2.781	3.684	11.481	3.120	0.090	0.080	1.230
25	0.110	0.260	3.374	4.360	13.771	3.700	0.127	0.116	1.284
26	0.085	0.144	4.129	4.939	15.345	4.263	0.164	0.160	1.048
27	0.535	1.061	5.283	6.859	21.247	5.494	0.292	0.285	1.541
28	0.116	0.316	4.399	6.782	20.002	4.982	0.249	0.234	0.732
29	0.349	0.459	5.692	6.345	21.843	5.642	0.308	0.284	1.246
30	0.144	0.334	5.051	7.400	24.248	5.730	0.347	0.294	0.621
31	0.027	0.067	3.554	4.752	15.381	4.143	0.159	0.133	0.612
32	1.148	1.661	6.103	13.945	53.525	9.693	1.297	0.668	0.608
33	0.096	0.244	3.241	5.421	18.057	4.145	0.187	0.138	0.776
34	0.131	0.322	4.742	5.937	19.016	4.669	0.222	0.221	0.774
35	0.140	0.592	3.148	5.233	16.748	4.119	0.172	0.129	1.047
36	0.640	2.049	6.067	6.812	24.497	5.741	0.352	0.325	1.876
37	0.065	0.121	3.929	4.537	15.469	3.986	0.154	0.140	0.899
38	0.057	0.156	2.964	5.044	16.782	3.982	0.167	0.117	0.622
39	0.049	0.161	2.859	4.073	13.567	3.522	0.119	0.091	1.249
40	0.015	0.026	2.338	3.094	9.103	3.028	0.069	0.057	0.878
41	0.065	0.154	3.388	4.395	14.337	3.683	0.132	0.117	1.134
42	0.150	0.300	4.221	5.874	20.243	4.553	0.230	0.195	0.773
43	1.618	2.628	7.460	14.252	45.129	8.355	0.943	0.835	0.665
44	0.118	0.270	3.389	5.919	16.909	4.575	0.193	0.158	1.049
45	0.048	0.080	4.100	4.888	16.858	4.339	0.183	0.157	0.692
46	0.413	1.134	4.955	5.832	21.532	4.829	0.260	0.227	2.005
47	5.489	8.192	4.856	13.272	38.744	6.453	0.625	0.506	1.563
48	0.166	0.381	4.146	5.861	19.226	4.767	0.229	0.191	0.946
49	0.471	1.692	4.251	6.311	19.493	5.268	0.257	0.211	1.331
50	0.068	0.159	3.330	4.548	14.206	3.568	0.127	0.119	0.943
51	1.284	2.125	5.828	7.791	26.972	5.678	0.383	0.357	1.769

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2	0.065	0.142	2.869	6.280	18.787	4.153	0.195	0.141	0.685
3	0.140	0.274	5.099	5.722	19.742	4.850	0.239	0.229	1.030
4	0.723	2.721	9.411	15.328	45.262	10.554	1.194	1.133	0.448
5	0.076	0.204	3.921	5.390	19.347	4.578	0.221	0.166	0.782
6	0.025	0.057	4.072	4.605	15.924	4.153	0.165	0.147	0.524
7	0.025	0.052	2.544	3.498	10.509	2.840	0.075	0.070	1.001
8	0.027	0.055	3.973	4.537	15.822	4.355	0.172	0.142	0.506
9	0.671	1.245	5.067	6.060	20.235	5.028	0.254	0.241	1.844
10	0.067	0.188	4.039	6.019	18.197	4.473	0.203	0.191	0.770
11	0.024	0.058	3.349	4.139	15.221	3.971	0.151	0.109	0.532
12	1.284	3.227	3.904	8.491	26.453	5.140	0.340	0.260	2.001
13	0.334	0.821	3.698	5.097	15.808	3.937	0.156	0.148	1.489
14	0.088	0.171	3.652	5.028	14.943	4.393	0.164	0.144	1.004
15	0.021	0.037	2.695	3.182	10.976	3.122	0.086	0.067	0.874
16	0.296	0.742	3.682	4.035	12.878	3.887	0.125	0.117	1.693
17	0.047	0.156	3.958	5.126	15.600	4.569	0.178	0.159	0.948
18	0.065	0.125	3.926	6.009	20.114	5.003	0.252	0.185	0.554
19	0.015	0.043	3.044	3.841	13.047	3.343	0.109	0.092	0.545
20	0.048	0.111	3.747	4.646	14.887	4.055	0.151	0.137	0.609
21	0.032	0.064	1.743	2.212	6.685	2.312	0.039	0.030	1.934
22	0.146	0.446	3.494	4.013	13.901	3.573	0.124	0.110	1.223
23	0.026	0.044	3.340	4.165	13.007	3.667	0.119	0.109	0.616
24	0.158	0.271	3.373	5.696	18.626	4.310	0.201	0.151	1.161
25	0.006	0.013	2.149	2.798	9.586	2.605	0.062	0.047	0.549
26	0.059	0.133	4.544	5.666	18.559	4.809	0.223	0.202	0.554
27	0.088	0.241	3.240	5.327	15.348	3.834	0.147	0.136	0.751
28	0.106	0.272	3.982	5.445	15.999	4.286	0.171	0.170	0.895
29	0.635	1.332	5.655	8.968	30.914	6.682	0.516	0.398	0.953
30	0.031	0.056	3.242	4.090	14.393	3.732	0.134	0.104	0.775
31	0.352	1.309	4.023	4.674	15.332	4.004	0.153	0.148	2.325
32	0.062	0.129	3.028	3.756	12.271	3.335	0.102	0.089	1.209
33	0.072	0.167	3.273	4.162	13.626	3.661	0.125	0.107	1.327
34	1.971	3.931	5.400	6.936	23.221	5.117	0.297	0.294	1.995
35	0.349	0.644	6.668	7.542	25.103	7.353	0.461	0.395	1.030
36	0.057	0.157	2.954	5.757	18.913	3.839	0.182	0.134	0.634
37	0.060	0.138	3.374	4.303	14.245	4.211	0.150	0.114	0.937
38	0.048	0.126	4.114	6.204	23.009	4.885	0.281	0.200	0.431
39	0.410	1.556	4.088	5.305	16.784	4.591	0.193	0.170	2.214
40	0.073	0.116	2.687	5.335	20.340	3.712	0.189	0.113	0.513
41	0.049	0.104	2.559	5.530	16.327	3.620	0.148	0.111	0.666
42	0.647	1.666	5.581	7.501	23.891	6.226	0.372	0.329	1.329
43	0.041	0.072	3.421	4.484	14.463	4.178	0.151	0.120	0.841
44	0.133	0.611	2.123	4.861	12.221	2.913	0.089	0.081	1.572
45	0.064	0.171	4.645	6.823	21.514	6.082	0.327	0.249	0.355
46	0.029	0.066	3.453	4.611	16.463	4.059	0.167	0.125	0.494
47	0.028	0.124	2.466	2.877	9.725	2.697	0.066	0.056	1.584
48	0.144	0.322	2.931	4.907	13.849	3.745	0.130	0.113	1.014
49	0.831	1.995	3.693	15.254	44.240	6.164	0.682	0.442	0.666
50	0.123	0.251	3.660	5.911	21.822	5.129	0.280	0.170	0.849
51	0.370	0.724	4.471	5.481	18.185	4.966	0.226	0.193	1.679
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2	0.138	0.387	3.088	3.831	12.450	3.565	0.111	0.093	2.122
3	9.561	17.746	2.961	18.027	50.338	5.556	0.699	0.419	1.193
4	0.010	0.022	2.536	3.340	10.417	2.938	0.077	0.067	0.611
5	0.028	0.068	2.961	3.628	12.388	3.587	0.111	0.084	1.019
6	0.007	0.017	2.669	3.062	9.724	3.065	0.075	0.064	0.485
7	0.709	1.350	6.233	9.921	32.559	7.095	0.578	0.486	1.059
8	0.177	0.312	3.682	5.598	18.267	4.597	0.210	0.162	1.131
9	0.030	0.083	3.109	3.713	13.372	4.008	0.134	0.091	0.945
10	0.043	0.083	2.949	4.596	16.118	4.349	0.175	0.106	0.652
11	0.019	0.034	3.058	3.824	11.763	3.366	0.099	0.092	0.673
12	0.041	0.094	2.402	3.999	11.654	2.840	0.083	0.075	0.993
13	0.005	0.016	1.871	3.149	9.064	2.252	0.051	0.046	0.473
14	0.011	0.029	2.480	2.749	9.781	2.680	0.066	0.054	0.838
15	0.105	0.295	5.164	6.092	19.890	5.675	0.282	0.247	0.940
16	0.071	0.166	3.647	5.591	18.794	4.024	0.189	0.160	0.718
17	0.154	0.247	3.845	5.198	17.087	4.221	0.180	0.157	1.182
18	0.433	1.019	7.600	9.255	32.052	7.377	0.591	0.552	0.759
19	0.946	2.323	5.854	9.288	29.079	6.525	0.474	0.427	1.117
20	5.822	10.316	10.249	12.646	43.430	9.687	1.052	1.018	1.517
21	0.133	0.375	4.577	4.981	16.951	4.848	0.205	0.179	1.257
22	0.457	1.342	6.603	9.821	38.845	7.126	0.692	0.509	0.530
23	0.021	0.096	4.180	5.671	18.176	4.536	0.206	0.186	0.300
24	0.173	0.291	5.563	7.294	22.990	5.826	0.335	0.319	0.738
25	0.033	0.091	1.425	2.956	8.692	2.091	0.045	0.033	1.531
26	0.242	0.482	6.692	7.545	27.655	7.023	0.486	0.397	0.804
27	0.673	2.261	4.714	7.341	25.595	5.352	0.342	0.272	0.918
28	0.014	0.028	3.033	3.304	11.382	3.083	0.088	0.079	0.715
29	0.705	2.209	3.936	5.479	16.917	4.038	0.171	0.169	1.545
30	0.017	0.035	2.888	3.555	11.320	3.126	0.088	0.081	0.700
31	0.012	0.028	2.723	3.744	12.259	3.122	0.096	0.080	0.511
32	0.062	0.177	3.927	4.189	14.081	3.967	0.140	0.129	1.205
33	0.129	0.299	3.261	4.724	14.375	3.444	0.124	0.121	1.255
34	0.223	0.408	1.690	6.942	22.424	2.675	0.150	0.092	0.807
35	0.604	2.576	9.516	16.051	57.167	9.204	1.315	1.200	0.288
36	0.133	0.416	3.427	4.118	13.379	3.487	0.117	0.111	1.722
37	0.190	0.611	4.209	5.875	18.330	4.775	0.219	0.194	1.392
38	0.200	0.582	4.580	5.781	20.002	5.026	0.251	0.208	1.487
39	0.052	0.127	4.276	4.986	17.482	4.697	0.205	0.167	0.779
40	1.463	2.581	5.536	7.179	23.516	5.577	0.328	0.312	1.939
41	1.064	3.380	4.917	12.472	34.457	5.794	0.499	0.482	1.010
42	0.294	0.489	4.505	8.378	31.391	5.719	0.449	0.296	0.719
43	0.301	0.601	6.063	8.092	28.011	6.899	0.483	0.385	0.865
44	0.323	0.806	3.486	7.314	23.602	4.859	0.287	0.200	1.297
45	0.227	0.354	3.933	6.501	22.813	5.068	0.289	0.201	0.960
46	0.072	0.173	4.796	6.793	21.520	5.804	0.312	0.256	0.533
47	0.054	0.126	2.981	3.763	11.219	3.091	0.087	0.088	1.153
48	0.002	0.005	1.667	2.050	6.305	1.717	0.027	0.027	0.561
49	0.080	0.202	3.798	4.688	14.879	3.770	0.140	0.140	0.865
50	0.003	0.011	2.058	2.646	8.188	2.184	0.045	0.043	0.390
51	0.364	0.676	4.880	7.274	20.777	5.344	0.278	0.279	1.165
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2	0.059	0.136	3.633	5.216	16.163	3.879	0.157	0.149	0.784
3	0.083	0.211	3.466	3.933	13.148	3.467	0.114	0.107	1.281
4	0.049	0.126	3.027	4.428	12.646	3.207	0.101	0.105	1.023
5	0.004	0.012	2.254	2.739	9.026	2.224	0.050	0.048	0.413
6	0.066	0.182	2.509	4.164	11.013	2.871	0.079	0.082	1.172
7	0.040	0.303	3.046	6.031	16.366	3.781	0.155	0.144	0.385
8	4.307	7.497	4.943	11.565	29.411	6.256	0.460	0.449	1.617
9	0.251	0.460	3.312	6.808	19.810	4.592	0.227	0.177	0.979
10	0.109	0.209	4.469	5.198	17.058	4.553	0.194	0.182	1.006
11	0.020	0.064	2.612	4.202	11.337	3.013	0.085	0.086	0.710
12	0.010	0.027	1.673	2.354	6.665	1.998	0.033	0.031	1.238
13	0.005	0.017	2.558	3.184	9.667	2.606	0.063	0.064	0.377
14	0.017	0.047	2.537	3.163	9.173	2.730	0.063	0.063	0.845
15	0.156	0.357	3.105	3.630	11.718	3.059	0.090	0.089	1.984
16	0.496	1.498	3.688	7.971	23.076	4.837	0.279	0.231	1.062
17	0.097	0.211	3.514	3.858	12.669	3.425	0.108	0.106	1.402
18	0.015	0.045	2.234	2.843	9.386	2.324	0.055	0.050	0.937
19	0.015	0.041	3.000	3.715	10.778	2.970	0.080	0.088	0.565
20	0.007	0.023	2.662	3.378	11.376	2.694	0.077	0.071	0.423
21	0.010	0.071	2.885	4.088	12.580	3.113	0.098	0.093	0.312
22	0.020	0.067	2.674	3.641	10.202	2.743	0.070	0.076	0.774
23	0.005	0.009	1.941	2.438	8.082	2.096	0.042	0.037	0.530
24	0.094	0.349	2.932	3.509	10.841	3.047	0.083	0.081	2.044
25	0.042	0.130	2.598	4.490	11.942	3.133	0.094	0.092	0.946
26	0.044	0.182	1.604	2.311	6.687	1.877	0.031	0.029	2.104
27	0.049	0.119	2.818	3.448	10.414	2.988	0.078	0.076	1.158
28	0.112	0.295	4.647	5.228	18.128	4.607	0.209	0.191	0.834
29	1.181	5.512	3.626	7.662	19.509	4.543	0.222	0.218	2.164
30	0.078	0.239	2.966	3.629	11.960	2.882	0.086	0.085	1.665
31	0.016	0.040	2.054	2.604	8.405	2.090	0.044	0.042	1.193
32	0.133	0.264	3.526	4.008	13.454	3.419	0.115	0.111	1.572
33	0.023	0.103	2.488	4.181	11.759	2.758	0.081	0.082	0.733
34	0.028	0.187	3.376	6.094	16.842	4.360	0.184	0.162	0.395
35	0.003	0.010	2.058	2.628	8.482	2.109	0.045	0.042	0.422
36	0.060	0.169	2.876	3.210	9.865	3.022	0.075	0.072	1.979
37	0.041	0.092	2.534	4.791	13.958	3.151	0.110	0.095	0.683
38	0.051	0.118	3.367	4.437	14.181	3.586	0.127	0.117	0.909
39	0.323	0.545	4.747	9.608	24.939	5.860	0.365	0.358	0.651
40	0.424	0.811	2.828	4.463	12.938	3.306	0.107	0.099	2.356
41	0.315	0.524	3.432	4.980	14.519	3.980	0.144	0.134	1.701
42	0.066	0.176	2.482	3.060	9.082	2.609	0.059	0.060	1.963
43	0.108	0.279	2.829	4.298	13.230	3.376	0.112	0.095	1.206
44	0.639	2.114	4.957	9.395	25.968	6.032	0.392	0.366	1.109
45	0.148	0.424	3.121	3.948	11.926	3.295	0.098	0.097	2.209
46	0.221	0.393	3.803	6.053	18.164	4.583	0.208	0.181	1.031
47	0.009	0.021	1.782	2.158	6.541	1.799	0.029	0.030	0.933
48	0.077	0.178	3.345	4.520	13.440	3.752	0.126	0.119	1.234
49	0.001	0.003	1.249	1.627	4.931	1.263	0.016	0.016	0.420
50	0.001	0.002	1.171	1.571	5.218	1.191	0.016	0.014	0.365
51	0.025	0.056	2.550	2.828	9.049	2.602	0.059	0.057	1.291
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2	0.003	0.008	1.614	2.232	6.529	1.706	0.028	0.028	0.544
3	0.004	0.008	2.024	2.328	7.829	1.956	0.038	0.037	0.595
4	0.152	0.463	3.752	6.083	20.202	4.746	0.240	0.179	0.764
5	0.110	0.280	3.307	5.198	14.592	3.553	0.130	0.135	1.248
6	0.074	0.206	2.337	3.921	10.721	2.726	0.073	0.072	1.265
7	0.054	0.145	3.253	4.288	12.309	3.606	0.111	0.110	0.924
8	0.130	0.248	3.443	4.427	13.709	3.601	0.123	0.120	1.325
9	0.020	0.057	2.337	2.977	8.842	2.448	0.054	0.055	1.207
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11	0.875	1.999	5.504	11.272	31.139	6.996	0.545	0.487	0.882
12	0.025	0.094	2.229	5.284	13.469	2.867	0.097	0.093	0.481
13	0.033	0.056	2.807	3.647	10.997	2.972	0.082	0.080	0.984
14	0.058	0.183	3.309	4.297	13.094	3.291	0.108	0.112	1.192
15	0.230	0.762	4.694	6.020	17.946	5.054	0.227	0.222	1.171
16	0.006	0.021	2.550	3.222	9.787	2.806	0.069	0.065	0.377
17	0.008	0.022	2.539	3.357	10.019	2.758	0.069	0.067	0.526
18	0.006	0.012	1.792	2.444	7.653	2.150	0.041	0.034	0.834
19	0.051	0.155	2.582	3.108	9.392	2.699	0.063	0.063	1.671
20	0.027	0.052	2.791	3.230	9.826	2.820	0.069	0.071	1.005
21	0.078	0.135	3.086	3.614	10.669	3.209	0.086	0.088	1.562
22	0.018	0.041	2.968	3.431	10.338	2.993	0.077	0.080	0.871
23	0.025	0.041	2.996	3.439	10.693	3.209	0.086	0.081	0.826
24	0.080	0.247	3.390	4.303	13.330	3.390	0.113	0.115	1.321
25	0.006	0.011	1.980	2.183	6.667	2.038	0.034	0.034	0.957
26	0.013	0.024	1.860	2.600	7.731	1.939	0.037	0.038	0.960
27	0.057	0.177	1.771	2.520	7.349	2.020	0.037	0.035	1.909
28	0.034	0.101	2.142	2.834	8.480	2.306	0.049	0.048	1.758
29	0.030	0.104	2.525	3.927	10.784	2.783	0.075	0.078	0.972
30	0.031	0.079	2.552	3.426	10.614	2.776	0.074	0.069	0.998
31	0.058	0.230	2.391	2.810	8.625	2.316	0.050	0.053	1.969
32	0.019	0.039	3.067	3.601	11.501	3.064	0.088	0.087	0.793
33	0.036	0.108	0.981	1.591	4.414	1.106	0.012	0.012	2.888
34	0.043	0.091	3.448	4.293	13.109	3.606	0.118	0.116	0.848
35	0.027	0.068	2.188	3.205	9.355	2.372	0.055	0.055	1.086
36	0.204	0.441	4.669	5.375	16.745	4.748	0.199	0.197	1.128
37	0.145	0.259	2.815	3.184	10.027	2.889	0.072	0.070	2.243
38	0.079	0.196	3.412	3.903	11.686	3.419	0.100	0.105	1.424
39	1.014	2.041	6.801	10.575	28.975	7.694	0.557	0.565	1.066
40	0.016	0.073	1.988	2.577	7.813	2.160	0.042	0.040	1.274
41	0.022	0.082	2.507	3.337	10.511	2.750	0.072	0.066	0.695
42	0.056	0.146	3.141	3.432	11.178	3.152	0.088	0.085	1.217
43	0.034	0.085	2.409	3.774	10.852	2.821	0.077	0.071	0.845
44	0.026	0.050	2.316	2.781	8.572	2.264	0.049	0.051	1.334
45	0.040	0.098	2.113	2.553	7.909	2.222	0.044	0.042	1.627
46	0.014	0.067	1.016	1.949	4.922	1.111	0.014	0.016	1.743
47	0.071	0.245	2.801	3.116	10.051	2.771	0.070	0.069	2.029
48	0.005	0.014	1.964	2.682	8.337	2.070	0.043	0.041	0.565
49	0.056	0.155	3.187	3.553	11.772	3.139	0.092	0.089	1.483
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eAR	BF	BL	NSI	AVSV	AASA	UI	EI	MAA	mm ⁻¹		
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5	1.625	1.471	0.153	0.270	0.485	0.671	0.079	0.240	0.318		
6	2.417	2.012	0.364	0.370	0.285	0.545	0.277	0.271	0.254		
7	1.534	1.000	0.052	0.311	0.311	0.529	0.101	0.282	0.322		
8	1.811	1.836	0.626	0.278	0.370	0.567	0.077	0.255	0.302		
9	1.739	1.358	0.340	0.270	0.390	0.580	0.023	0.264	0.325		
10	0.657	1.101	0.202	0.249	0.549	0.709	0.034	0.237	0.322		
11	2.499	2.064	0.491	0.257	0.555	0.721	0.045	0.234	0.090		
12	1.115	1.117	0.351	0.254	0.478	0.650	0.043	0.240	0.324		
13	0.821	1.004	0.019	0.258	0.555	0.723	0.037	0.247	0.308		
14	1.490	1.649	0.475	0.279	0.407	0.605	0.046	0.267	0.354		
15	1.441	1.113	0.499	0.236	0.639	0.770	0.018	0.231	0.239		
16	2.401	2.536	0.414	0.304	0.261	0.465	0.077	0.284	0.259		
17	1.644	1.768	0.543	0.249	0.431	0.603	0.027	0.240	0.216		
18	0.531	1.148	0.113	0.299	0.285	0.491	0.079	0.275	0.356		
19	0.805	1.000	0.010	0.291	0.460	0.667	0.039	0.276	0.401		
20	2.082	1.729	0.453	0.261	0.396	0.579	0.073	0.245	0.185		
21	0.798	1.000	0.031	0.289	0.441	0.647	0.037	0.277	0.666		
22	2.164	1.847	0.528	0.267	0.459	0.644	0.047	0.251	0.163		
23	1.052	1.172	0.466	0.239	0.628	0.766	0.017	0.233	0.524		
24	1.452	1.214	0.464	0.260	0.454	0.633	0.029	0.251	0.389		
25	1.513	1.531	0.674	0.275	0.390	0.584	0.074	0.252	0.292		
26	1.214	1.180	0.285	0.266	0.562	0.737	0.054	0.248	0.315		
27	1.924	1.583	0.324	0.243	0.494	0.655	0.022	0.235	0.179		
28	0.997	1.153	0.390	0.278	0.354	0.550	0.034	0.266	0.283		
29	1.402	1.454	0.443	0.226	0.748	0.845	0.016	0.220	0.200		
30	0.802	0.986	0.424	0.286	0.396	0.600	0.079	0.259	0.239		
31	0.701	0.998	0.026	0.297	0.377	0.589	0.080	0.272	0.357		
32	0.874	0.993	0.153	0.232	0.680	0.799	0.016	0.226	0.132		
33	1.016	1.204	0.520	0.299	0.349	0.561	0.112	0.264	0.321		
34	0.985	1.417	0.453	0.271	0.385	0.577	0.053	0.253	0.303		
35	1.330	1.958	0.536	0.354	0.188	0.404	0.204	0.300	0.317		
36	2.226	1.674	0.290	0.322	0.275	0.496	0.119	0.276	0.176		
37	1.023	1.178	0.492	0.254	0.522	0.690	0.024	0.245	0.337		
38	0.787	1.281	0.383	0.279	0.344	0.540	0.066	0.257	0.354		
39	1.444	1.163	0.261	0.307	0.277	0.486	0.099	0.278	0.371		
40	0.897	1.049	0.432	0.258	0.539	0.709	0.039	0.243	0.499		
41	1.353	1.145	0.347	0.266	0.404	0.591	0.042	0.253	0.325		
42	0.998	1.361	0.313	0.263	0.473	0.654	0.055	0.246	0.271		
43	1.134	1.112	0.234	0.247	0.595	0.746	0.033	0.231	0.128		
44	1.358	1.027	0.320	0.288	0.400	0.605	0.087	0.256	0.284		
45	0.780	1.024	0.204	0.259	0.578	0.743	0.032	0.248	0.335		
46	2.421	1.532	0.475	0.270	0.351	0.541	0.036	0.259	0.193		
47	3.215	1.713	0.478	0.224	0.662	0.777	0.012	0.220	0.088		
48	1.163	1.378	0.409	0.268	0.413	0.601	0.055	0.254	0.274		
49	1.594	2.251	0.194	0.327	0.241	0.456	0.136	0.277	0.212		
50	1.202	1.308	0.446	0.255	0.413	0.591	0.032	0.242	0.336		
51	2.428	1.802	0.503	0.242	0.588	0.734	0.027	0.232	0.135		
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2	1.036	0.977	0.145	0.297	0.405	0.618	0.109	0.264	0.331
3	1.215	1.183	0.417	0.254	0.499	0.669	0.022	0.244	0.258
4	0.651	1.059	0.327	0.319	0.256	0.470	0.037	0.304	0.154
5	0.920	1.169	0.349	0.271	0.352	0.543	0.052	0.257	0.345
6	0.581	1.000	0.015	0.318	0.415	0.647	0.050	0.301	0.368
7	1.233	1.019	0.561	0.280	0.437	0.635	0.069	0.258	0.435
8	0.527	1.000	0.154	0.309	0.456	0.680	0.067	0.284	0.343
9	2.223	1.872	0.519	0.236	0.528	0.679	0.019	0.229	0.169
10	1.037	1.000	0.024	0.329	0.323	0.556	0.099	0.287	0.313
11	0.555	1.091	0.219	0.279	0.399	0.596	0.047	0.265	0.413
12	3.305	1.703	0.484	0.262	0.382	0.566	0.041	0.252	0.142
13	1.927	2.168	0.604	0.306	0.347	0.565	0.145	0.256	0.232
14	1.149	1.205	0.410	0.246	0.503	0.666	0.026	0.237	0.314
15	0.890	1.187	0.333	0.238	0.559	0.706	0.019	0.231	0.494
16	1.757	2.633	0.381	0.268	0.380	0.569	0.049	0.251	0.223
17	1.063	1.000	0.054	0.332	0.264	0.489	0.126	0.292	0.373
18	0.666	0.999	0.185	0.282	0.488	0.685	0.059	0.262	0.302
19	0.626	1.000	0.072	0.336	0.313	0.550	0.102	0.301	0.437
20	0.698	1.278	0.503	0.299	0.383	0.597	0.104	0.257	0.391
21	1.850	1.899	0.554	0.259	0.479	0.656	0.059	0.239	0.432
22	1.374	2.359	0.431	0.279	0.312	0.506	0.047	0.264	0.285
23	0.700	1.000	0.077	0.267	0.568	0.742	0.027	0.255	0.443
24	1.534	1.155	0.439	0.242	0.569	0.719	0.027	0.233	0.261
25	0.590	0.998	0.009	0.309	0.405	0.630	0.084	0.281	0.578
26	0.653	1.067	0.304	0.284	0.437	0.638	0.025	0.274	0.355
27	1.043	1.303	0.312	0.347	0.290	0.533	0.202	0.281	0.330
28	1.137	1.351	0.350	0.262	0.379	0.563	0.031	0.253	0.321
29	1.279	1.434	0.449	0.258	0.453	0.630	0.051	0.244	0.176
30	0.850	0.997	0.026	0.264	0.531	0.708	0.044	0.248	0.397
31	2.714	1.699	0.589	0.288	0.251	0.443	0.067	0.270	0.220
32	1.361	1.480	0.572	0.244	0.470	0.635	0.018	0.238	0.367
33	1.509	1.147	0.305	0.255	0.420	0.597	0.025	0.247	0.326
34	2.705	2.766	0.544	0.245	0.488	0.652	0.027	0.235	0.119
35	1.056	1.184	0.275	0.268	0.505	0.688	0.068	0.237	0.167
36	0.951	0.962	0.134	0.271	0.346	0.537	0.041	0.258	0.334
37	0.957	1.203	0.325	0.298	0.388	0.602	0.103	0.263	0.331
38	0.547	0.970	0.043	0.307	0.353	0.572	0.072	0.283	0.258
39	2.558	2.061	0.539	0.335	0.221	0.436	0.163	0.293	0.213
40	0.738	0.964	0.338	0.238	0.616	0.754	0.029	0.228	0.320
41	1.018	0.996	0.078	0.276	0.444	0.639	0.063	0.252	0.293
42	1.601	1.728	0.463	0.272	0.366	0.558	0.059	0.250	0.157
43	0.902	0.999	0.139	0.280	0.526	0.718	0.069	0.254	0.354
44	2.623	1.546	0.263	0.339	0.185	0.389	0.152	0.296	0.310
45	0.398	0.991	0.076	0.300	0.349	0.562	0.070	0.277	0.298
46	0.561	1.013	0.325	0.291	0.396	0.605	0.081	0.264	0.374
47	1.690	1.350	0.455	0.324	0.203	0.405	0.088	0.304	0.462
48	1.328	1.691	0.552	0.279	0.413	0.610	0.078	0.251	0.273
49	1.649	1.000	0.110	0.263	0.403	0.588	0.033	0.255	0.148
50	0.979	1.218	0.257	0.267	0.457	0.642	0.070	0.248	0.296
51	1.853	1.713	0.549	0.256	0.488	0.661	0.045	0.239	0.181
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2	2.281	1.444	0.689	0.298	0.324	0.534	0.091	0.270	0.297
3	3.872	1.683	0.422	0.260	0.511	0.685	0.052	0.231	0.073
4	0.694	1.000	0.050	0.295	0.436	0.647	0.057	0.271	0.532
5	1.031	1.009	0.069	0.257	0.417	0.597	0.009	0.255	0.456
6	0.485	1.000	0.001	0.301	0.407	0.623	0.018	0.296	0.593
7	1.480	1.156	0.560	0.275	0.478	0.669	0.091	0.246	0.152
8	1.377	1.384	0.467	0.247	0.545	0.704	0.039	0.232	0.241
9	0.875	0.965	0.010	0.278	0.346	0.542	0.053	0.260	0.393
10	0.689	1.096	0.434	0.238	0.511	0.666	0.017	0.232	0.406
11	0.765	0.994	0.048	0.262	0.556	0.727	0.021	0.253	0.494
12	1.398	1.116	0.237	0.278	0.416	0.613	0.051	0.261	0.401
13	0.661	0.999	0.114	0.313	0.276	0.490	0.059	0.295	0.631
14	0.860	1.185	0.206	0.270	0.375	0.565	0.042	0.255	0.565
15	1.009	0.969	0.008	0.325	0.315	0.545	0.115	0.294	0.283
16	0.998	1.142	0.263	0.277	0.406	0.602	0.047	0.259	0.353
17	1.456	1.326	0.441	0.227	0.614	0.742	0.012	0.222	0.274
18	0.952	1.314	0.224	0.280	0.395	0.593	0.070	0.253	0.198
19	1.590	1.708	0.279	0.336	0.343	0.586	0.158	0.260	0.163
20	1.980	1.982	0.453	0.229	0.559	0.699	0.010	0.226	0.088
21	1.291	1.403	0.357	0.271	0.343	0.533	0.037	0.258	0.286
22	0.730	1.334	0.118	0.365	0.283	0.538	0.170	0.299	0.230
23	0.375	1.000	0.059	0.449	0.195	0.484	0.115	0.409	0.320
24	0.924	1.092	0.359	0.251	0.584	0.740	0.016	0.244	0.268
25	2.164	1.461	0.559	0.277	0.342	0.538	0.060	0.263	0.453
26	0.864	1.229	0.217	0.241	0.495	0.654	0.016	0.236	0.243
27	1.259	2.051	0.108	0.277	0.285	0.476	0.041	0.263	0.182
28	0.767	1.023	0.225	0.293	0.487	0.695	0.054	0.271	0.483
29	2.097	2.949	0.546	0.395	0.229	0.491	0.282	0.285	0.215
30	0.796	1.018	0.284	0.285	0.471	0.672	0.044	0.267	0.482
31	0.613	1.000	0.040	0.335	0.390	0.637	0.134	0.277	0.535
32	1.273	1.147	0.315	0.288	0.328	0.530	0.064	0.268	0.354
33	1.722	1.509	0.519	0.283	0.401	0.602	0.072	0.256	0.303
34	2.094	1.054	0.310	0.272	0.512	0.698	0.064	0.230	0.254
35	0.503	1.009	0.204	0.303	0.218	0.413	0.069	0.288	0.174
36	2.034	1.750	0.499	0.327	0.273	0.496	0.148	0.275	0.304
37	1.712	1.261	0.377	0.364	0.247	0.492	0.205	0.283	0.281
38	1.711	1.227	0.332	0.334	0.285	0.516	0.172	0.271	0.255
39	0.827	1.121	0.175	0.298	0.379	0.592	0.071	0.272	0.346
40	2.496	2.359	0.471	0.236	0.555	0.702	0.021	0.229	0.137
41	2.173	1.152	0.520	0.280	0.296	0.489	0.061	0.260	0.138
42	1.053	1.060	0.327	0.241	0.584	0.730	0.029	0.230	0.197
43	1.015	1.152	0.472	0.264	0.475	0.657	0.052	0.243	0.184
44	1.953	1.081	0.491	0.267	0.382	0.570	0.046	0.258	0.206
45	1.232	1.346	0.387	0.231	0.633	0.761	0.013	0.227	0.245
46	0.624	0.994	0.101	0.300	0.390	0.606	0.056	0.281	0.278
47	1.404	1.529	0.477	0.289	0.388	0.594	0.095	0.258	0.401
48	0.669	1.000	0.086	0.317	0.389	0.619	0.083	0.295	0.974
49	1.076	1.550	0.450	0.282	0.363	0.562	0.090	0.253	0.328
50	0.472	0.969	0.129	0.365	0.268	0.520	0.154	0.315	0.791
51	1.586	1.369	0.274	0.262	0.507	0.684	0.060	0.238	0.198
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2	1.054	1.201	0.355	0.310	0.384	0.608	0.117	0.267	0.349
3	1.453	1.452	0.652	0.279	0.363	0.561	0.078	0.254	0.339
4	1.412	1.316	0.338	0.345	0.316	0.563	0.180	0.278	0.418
5	0.509	0.985	0.000	0.415	0.237	0.520	0.241	0.341	0.717
6	1.700	1.489	0.626	0.290	0.329	0.532	0.091	0.265	0.359
7	0.615	1.352	0.249	0.387	0.104	0.287	0.215	0.329	0.418
8	2.990	1.941	0.524	0.242	0.556	0.709	0.032	0.227	0.092
9	1.452	1.358	0.550	0.269	0.507	0.691	0.070	0.243	0.237
10	1.149	1.250	0.248	0.317	0.447	0.680	0.142	0.259	0.296
11	0.990	1.009	0.242	0.339	0.281	0.514	0.113	0.296	0.459
12	1.459	1.117	0.411	0.319	0.310	0.533	0.146	0.276	0.646
13	0.461	0.915	0.154	0.420	0.217	0.495	0.213	0.349	0.588
14	0.979	1.289	0.449	0.293	0.344	0.552	0.055	0.274	0.566
15	2.355	1.916	0.548	0.264	0.415	0.599	0.051	0.247	0.269
16	1.750	1.650	0.095	0.378	0.242	0.495	0.270	0.279	0.226
17	1.580	1.845	0.205	0.313	0.394	0.622	0.141	0.263	0.347
18	1.146	1.285	0.421	0.284	0.318	0.516	0.080	0.254	0.594
19	0.706	1.000	0.010	0.303	0.334	0.548	0.075	0.282	0.538
20	0.530	1.000	0.157	0.402	0.233	0.503	0.195	0.355	0.507
21	0.410	1.061	0.241	0.443	0.113	0.333	0.239	0.370	0.537
22	1.027	1.194	0.485	0.299	0.280	0.485	0.078	0.273	0.501
23	0.617	1.045	0.099	0.340	0.394	0.647	0.200	0.262	0.841
24	2.354	1.474	0.312	0.305	0.248	0.451	0.079	0.280	0.315
25	1.355	1.113	0.287	0.305	0.291	0.501	0.098	0.269	0.398
26	2.590	2.710	0.626	0.371	0.190	0.417	0.218	0.305	0.462
27	1.336	1.605	0.479	0.265	0.392	0.579	0.050	0.246	0.397
28	0.946	1.511	0.221	0.295	0.336	0.544	0.118	0.249	0.289
29	3.649	1.959	0.320	0.326	0.199	0.401	0.074	0.305	0.151
30	2.097	1.414	0.346	0.366	0.243	0.487	0.261	0.285	0.355
31	1.486	1.127	0.438	0.271	0.360	0.551	0.091	0.247	0.546
32	1.842	1.648	0.293	0.274	0.465	0.656	0.076	0.247	0.279
33	1.112	0.957	0.276	0.323	0.186	0.382	0.159	0.290	0.471
34	0.552	0.987	0.043	0.396	0.123	0.326	0.180	0.344	0.392
35	0.526	0.996	0.113	0.357	0.279	0.527	0.180	0.317	0.764
36	2.102	1.299	0.521	0.280	0.343	0.540	0.042	0.268	0.364
37	1.039	1.074	0.564	0.284	0.403	0.605	0.100	0.246	0.419
38	1.125	1.149	0.251	0.288	0.390	0.595	0.102	0.251	0.378
39	1.068	1.010	0.476	0.279	0.533	0.725	0.101	0.237	0.207
40	3.180	2.032	0.487	0.236	0.514	0.666	0.017	0.229	0.207
41	2.128	1.947	0.420	0.240	0.584	0.730	0.029	0.230	0.211
42	2.303	1.525	0.379	0.275	0.350	0.544	0.072	0.252	0.354
43	1.536	1.691	0.692	0.313	0.333	0.554	0.138	0.256	0.331
44	1.728	1.239	0.351	0.339	0.242	0.466	0.201	0.274	0.189
45	2.647	1.653	0.685	0.319	0.299	0.522	0.142	0.279	0.284
46	1.362	1.469	0.396	0.257	0.529	0.699	0.059	0.233	0.244
47	1.119	1.538	0.595	0.288	0.384	0.589	0.086	0.261	0.685
48	1.487	1.206	0.279	0.306	0.371	0.590	0.138	0.259	0.331
49	0.542	0.946	0.453	0.346	0.283	0.523	0.186	0.289	1.245
50	0.481	0.962	0.216	0.379	0.260	0.520	0.222	0.310	1.290
51	1.403	1.314	0.236	0.291	0.404	0.612	0.096	0.258	0.498
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2	0.711	0.977	0.072	0.350	0.270	0.510	0.175	0.286	0.960
3	0.708	0.998	0.033	0.322	0.406	0.642	0.142	0.283	0.778
4	0.980	1.519	0.420	0.333	0.277	0.506	0.154	0.261	0.273
5	1.826	1.137	0.564	0.281	0.356	0.554	0.090	0.257	0.286
6	1.820	1.472	0.417	0.290	0.323	0.526	0.097	0.255	0.339
7	1.099	1.472	0.213	0.286	0.359	0.562	0.041	0.272	0.360
8	1.629	1.712	0.402	0.277	0.472	0.665	0.101	0.240	0.288
9	1.468	1.378	0.359	0.288	0.330	0.533	0.071	0.266	0.513
10	1.421	1.272	0.704	0.270	0.405	0.595	0.075	0.243	0.158
11	0.887	1.004	0.010	0.354	0.222	0.450	0.172	0.290	0.503
12	1.207	1.141	0.506	0.268	0.543	0.721	0.073	0.241	0.427
13	1.556	1.359	0.236	0.324	0.270	0.490	0.155	0.284	0.360
14	1.395	1.551	0.291	0.282	0.286	0.480	0.051	0.264	0.222
15	0.432	0.970	0.141	0.391	0.247	0.513	0.180	0.323	0.548
16	0.640	1.000	0.066	0.355	0.317	0.572	0.129	0.310	0.553
17	0.948	0.993	0.061	0.298	0.422	0.637	0.094	0.267	0.685
18	1.924	1.521	0.592	0.274	0.314	0.505	0.048	0.261	0.385
19	1.151	1.409	0.443	0.276	0.489	0.680	0.078	0.251	0.443
20	1.759	1.666	0.358	0.272	0.542	0.725	0.062	0.245	0.330
21	0.999	1.000	0.060	0.308	0.387	0.610	0.109	0.270	0.463
22	0.886	1.166	0.485	0.265	0.569	0.741	0.067	0.240	0.439
23	1.677	1.400	0.378	0.369	0.242	0.489	0.251	0.278	0.358
24	1.025	1.064	0.274	0.260	0.532	0.704	0.026	0.252	0.717
25	1.287	1.313	0.633	0.284	0.481	0.681	0.112	0.248	0.603
26	2.382	2.568	0.604	0.321	0.273	0.492	0.156	0.268	0.404
27	2.160	1.506	0.348	0.320	0.298	0.521	0.102	0.286	0.439
28	1.372	1.184	0.514	0.395	0.198	0.446	0.325	0.294	0.524
29	1.231	1.411	0.288	0.294	0.349	0.557	0.099	0.256	0.453
30	2.389	1.586	0.667	0.295	0.232	0.425	0.075	0.276	0.374
31	0.932	0.994	0.365	0.305	0.434	0.655	0.102	0.272	0.483
32	4.155	2.651	0.700	0.325	0.284	0.507	0.137	0.272	0.473
33	1.009	1.166	0.421	0.266	0.454	0.639	0.044	0.252	0.377
34	1.468	1.390	0.440	0.274	0.372	0.565	0.063	0.254	0.475
35	1.277	1.687	0.423	0.265	0.432	0.618	0.063	0.242	0.231
36	2.472	2.341	0.557	0.254	0.537	0.702	0.046	0.239	0.274
37	1.625	1.394	0.333	0.295	0.358	0.568	0.111	0.263	0.329
38	1.466	1.326	0.386	0.250	0.478	0.647	0.037	0.235	0.142
39	1.520	1.268	0.547	0.363	0.169	0.381	0.221	0.303	0.600
40	0.843	1.420	0.333	0.352	0.220	0.447	0.171	0.290	0.536
41	1.325	1.726	0.471	0.302	0.340	0.554	0.113	0.265	0.381
42	1.130	1.404	0.483	0.289	0.371	0.576	0.088	0.261	0.405
43	1.639	1.526	0.331	0.261	0.497	0.674	0.048	0.244	0.474
44	1.870	2.178	0.437	0.320	0.344	0.573	0.168	0.262	0.442
45	3.059	1.575	0.476	0.309	0.176	0.361	0.142	0.289	0.651
46	2.282	1.516	0.635	0.300	0.269	0.472	0.077	0.275	0.360
47	0.732	0.995	0.012	0.324	0.313	0.541	0.148	0.286	0.680
48	1.679	1.311	0.233	0.310	0.313	0.530	0.136	0.269	0.383
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	absMAA	MSD	HMC	MLN	GAA	absGAA	GSD	HGC	GLN
	mm ⁻¹	mm ⁻¹	%	-	mm ⁻²	mm ⁻²	mm ⁻²	%	-
5	0.370	0.303	27.483	0.329	0.069	0.227	0.376	170.270	2.699
6	0.328	0.307	99.650	0.491	0.034	0.179	0.308	561.209	5.898
7	0.382	0.330	39.608	0.316	0.048	0.220	0.383	193.206	2.283
8	0.343	0.255	35.989	0.317	0.050	0.192	0.287	202.369	2.361
9	0.337	0.247	25.724	0.306	0.081	0.152	0.244	111.783	1.818
10	0.348	0.234	10.601	0.264	0.090	0.155	0.217	56.300	1.293
11	0.140	0.155	68.740	0.506	0.006	0.030	0.072	337.335	7.205
12	0.379	0.315	27.518	0.311	0.080	0.199	0.306	125.715	1.876
13	0.325	0.237	-4.035	0.233	0.076	0.159	0.256	38.871	1.205
14	0.376	0.331	22.618	0.325	0.092	0.203	0.412	115.984	2.393
15	0.248	0.178	7.167	0.294	0.047	0.083	0.136	54.474	1.768
16	0.294	0.242	65.689	0.374	0.041	0.130	0.235	310.560	3.334
17	0.232	0.170	32.321	0.326	0.042	0.071	0.102	131.248	1.942
18	0.380	0.249	39.230	0.262	0.102	0.203	0.260	172.089	1.276
19	0.404	0.211	-2.756	0.215	0.132	0.193	0.229	12.202	0.746
20	0.215	0.197	46.687	0.382	0.024	0.082	0.158	281.687	4.003
21	0.671	0.414	-0.486	0.222	0.361	0.563	0.758	23.583	0.845
22	0.199	0.192	44.389	0.398	0.020	0.063	0.127	232.352	4.009
23	0.543	0.286	2.134	0.252	0.241	0.363	0.400	28.454	1.043
24	0.399	0.190	13.360	0.256	0.120	0.191	0.207	54.113	1.056
25	0.307	0.212	21.546	0.290	0.053	0.152	0.204	138.982	1.721
26	0.340	0.239	10.459	0.284	0.081	0.165	0.226	74.818	1.560
27	0.203	0.158	28.289	0.329	0.028	0.056	0.096	122.201	2.377
28	0.315	0.227	33.131	0.287	0.073	0.131	0.186	133.613	1.570
29	0.216	0.119	3.469	0.271	0.036	0.056	0.064	27.970	1.247
30	0.271	0.231	16.426	0.271	0.038	0.130	0.217	140.469	1.842
31	0.382	0.264	-3.851	0.197	0.096	0.246	0.282	55.765	0.735
32	0.140	0.088	2.641	0.257	0.016	0.025	0.033	36.799	1.203
33	0.387	0.372	50.037	0.365	0.077	0.284	0.468	327.761	3.296
34	0.333	0.246	41.619	0.324	0.085	0.154	0.209	177.817	1.951
35	0.354	0.270	84.214	0.364	0.055	0.217	0.303	487.876	2.950
36	0.237	0.244	86.955	0.450	0.019	0.087	0.200	441.938	5.629
37	0.371	0.235	13.847	0.266	0.100	0.161	0.201	51.703	1.185
38	0.439	0.399	46.462	0.326	0.087	0.306	0.492	240.832	2.349
39	0.407	0.281	37.388	0.281	0.076	0.231	0.343	163.135	1.613
40	0.570	0.384	4.723	0.241	0.184	0.475	0.580	60.221	1.122
41	0.362	0.272	20.362	0.280	0.081	0.167	0.275	85.294	1.573
42	0.308	0.246	27.931	0.317	0.060	0.144	0.226	147.719	2.208
43	0.164	0.148	40.176	0.378	0.015	0.033	0.059	142.546	2.862
44	0.343	0.312	37.421	0.341	0.048	0.213	0.351	242.425	2.908
45	0.387	0.269	3.259	0.237	0.098	0.204	0.253	45.488	1.042
46	0.226	0.209	46.111	0.364	0.027	0.073	0.137	206.103	2.868
47	0.096	0.068	19.469	0.339	0.007	0.012	0.020	92.486	2.471
48	0.289	0.212	30.106	0.314	0.061	0.121	0.182	145.513	1.983
49	0.281	0.269	107.395	0.461	0.030	0.133	0.249	629.400	5.743
50	0.393	0.319	32.247	0.311	0.093	0.194	0.294	119.328	1.750
51	0.165	0.153	31.289	0.381	0.015	0.037	0.066	136.383	2.960

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2	0.350	0.247	13.398	0.258	0.070	0.203	0.269	112.222	1.370
3	0.287	0.208	15.684	0.280	0.052	0.102	0.226	66.441	2.078
4	0.182	0.175	57.716	0.334	0.022	0.042	0.081	218.754	2.151
5	0.356	0.234	30.075	0.275	0.096	0.198	0.247	164.159	1.450
6	0.388	0.259	-7.566	0.195	0.122	0.195	0.277	10.566	0.715
7	0.460	0.300	6.766	0.251	0.122	0.315	0.390	69.545	1.155
8	0.407	0.329	-3.969	0.208	0.118	0.246	0.302	36.806	0.780
9	0.203	0.182	35.467	0.372	0.023	0.063	0.105	179.517	3.037
10	0.419	0.407	48.732	0.337	0.078	0.257	0.381	224.679	2.102
11	0.473	0.333	13.718	0.224	0.139	0.309	0.393	78.607	0.935
12	0.161	0.146	47.887	0.385	0.015	0.043	0.081	264.046	3.689
13	0.278	0.232	61.744	0.390	0.035	0.115	0.193	289.460	3.489
14	0.343	0.232	18.223	0.283	0.082	0.158	0.233	88.126	1.628
15	0.516	0.267	7.079	0.243	0.221	0.329	0.340	41.759	0.958
16	0.275	0.261	54.542	0.398	0.039	0.108	0.207	242.212	3.573
17	0.402	0.312	34.161	0.275	0.096	0.248	0.417	176.386	1.726
18	0.327	0.269	1.580	0.244	0.071	0.179	0.283	72.216	1.339
19	0.523	0.441	13.316	0.229	0.147	0.443	0.626	107.707	1.104
20	0.491	0.422	46.646	0.329	0.120	0.372	0.524	231.396	2.211
21	0.484	0.309	19.917	0.289	0.080	0.373	0.597	129.208	2.242
22	0.318	0.236	50.879	0.336	0.061	0.135	0.240	202.896	2.567
23	0.463	0.263	1.081	0.234	0.180	0.269	0.319	28.479	0.951
24	0.298	0.229	19.650	0.310	0.057	0.120	0.208	94.046	2.157
25	0.601	0.450	-12.547	0.189	0.274	0.589	0.757	24.710	0.673
26	0.368	0.232	16.362	0.257	0.120	0.161	0.209	60.852	1.110
27	0.385	0.324	48.503	0.340	0.063	0.256	0.413	281.276	2.831
28	0.340	0.253	36.700	0.321	0.085	0.162	0.290	161.584	2.334
29	0.205	0.197	40.081	0.374	0.025	0.068	0.150	216.724	3.849
30	0.437	0.302	3.354	0.240	0.136	0.240	0.328	34.409	1.029
31	0.234	0.160	59.080	0.336	0.034	0.082	0.108	276.784	2.173
32	0.374	0.216	17.165	0.279	0.114	0.175	0.261	71.811	1.539
33	0.356	0.235	21.604	0.277	0.073	0.173	0.277	101.693	1.713
34	0.163	0.184	59.477	0.479	0.013	0.047	0.138	347.994	8.316
35	0.268	0.333	43.610	0.421	0.021	0.093	0.193	166.645	3.114
36	0.398	0.341	33.368	0.288	0.094	0.204	0.327	128.610	1.558
37	0.415	0.393	32.874	0.323	0.084	0.229	0.342	134.917	1.756
38	0.320	0.293	-0.625	0.200	0.038	0.168	0.269	62.166	0.895
39	0.255	0.212	83.131	0.388	0.023	0.103	0.163	433.185	3.457
40	0.379	0.308	14.760	0.291	0.088	0.207	0.331	89.730	1.849
41	0.395	0.322	15.166	0.254	0.043	0.241	0.361	105.098	1.550
42	0.201	0.181	48.023	0.352	0.012	0.064	0.109	248.305	2.981
43	0.392	0.291	1.273	0.245	0.094	0.233	0.293	55.595	1.109
44	0.368	0.321	93.888	0.400	0.051	0.203	0.379	462.490	3.849
45	0.350	0.276	20.654	0.231	0.081	0.163	0.223	93.445	0.961
46	0.428	0.351	7.344	0.228	0.100	0.274	0.369	72.784	0.947
47	0.478	0.292	47.932	0.282	0.105	0.283	0.429	171.297	1.482
48	0.348	0.308	47.938	0.367	0.054	0.186	0.289	236.237	2.935
49	0.167	0.145	30.251	0.322	0.010	0.043	0.078	162.837	2.388
50	0.343	0.294	34.369	0.325	0.075	0.203	0.309	211.068	2.415
51	0.234	0.207	30.349	0.335	0.016	0.074	0.146	129.073	2.742
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2	0.310	0.203	40.308	0.321	0.062	0.127	0.156	158.831	1.680
3	0.134	0.159	116.852	0.652	0.004	0.032	0.070	729.119	12.129
4	0.582	0.368	1.515	0.213	0.245	0.414	0.448	25.923	0.694
5	0.456	0.212	15.229	0.243	0.171	0.207	0.272	32.309	0.940
6	0.596	0.330	-4.095	0.194	0.295	0.427	0.550	10.610	0.637
7	0.198	0.195	35.769	0.362	0.010	0.071	0.132	235.187	3.551
8	0.287	0.219	20.911	0.302	0.047	0.113	0.167	100.239	1.872
9	0.442	0.314	19.405	0.241	0.102	0.267	0.354	94.929	1.064
10	0.422	0.250	13.919	0.250	0.164	0.215	0.238	56.828	1.001
11	0.523	0.306	4.891	0.240	0.221	0.313	0.342	26.158	0.871
12	0.462	0.355	30.353	0.311	0.127	0.265	0.410	111.064	1.816
13	0.694	0.535	9.189	0.210	0.239	0.801	1.159	98.527	0.957
14	0.632	0.437	20.122	0.248	0.262	0.507	0.657	83.067	1.073
15	0.287	0.214	18.435	0.266	0.052	0.111	0.229	88.334	1.656
16	0.384	0.290	31.078	0.302	0.114	0.181	0.260	109.950	1.561
17	0.289	0.180	12.421	0.289	0.069	0.095	0.137	43.848	1.499
18	0.240	0.200	49.804	0.341	0.036	0.079	0.118	206.468	2.274
19	0.240	0.234	97.060	0.481	0.018	0.087	0.128	487.833	4.638
20	0.095	0.071	28.605	0.350	0.007	0.012	0.023	123.417	2.849
21	0.302	0.200	35.247	0.296	0.068	0.112	0.147	124.830	1.462
22	0.324	0.338	121.985	0.512	0.040	0.148	0.249	593.122	4.969
23	0.334	0.280	-5.348	0.180	0.085	0.189	0.332	52.250	0.772
24	0.271	0.137	11.424	0.266	0.071	0.080	0.092	34.642	1.143
25	0.472	0.278	31.700	0.294	0.131	0.275	0.419	114.179	1.681
26	0.246	0.119	19.664	0.260	0.058	0.064	0.064	51.720	1.000
27	0.233	0.223	89.689	0.436	0.028	0.080	0.135	433.125	3.965
28	0.534	0.370	0.416	0.228	0.195	0.369	0.501	30.857	0.949
29	0.312	0.312	151.925	0.593	0.026	0.159	0.256	935.858	7.911
30	0.526	0.357	6.666	0.243	0.197	0.375	0.483	54.078	1.073
31	0.559	0.295	4.862	0.210	0.250	0.355	0.369	25.014	0.660
32	0.363	0.233	26.305	0.276	0.093	0.198	0.265	140.458	1.494
33	0.359	0.305	48.969	0.371	0.077	0.185	0.285	219.141	2.764
34	0.335	0.338	54.332	0.440	0.050	0.171	0.468	262.402	6.402
35	0.199	0.168	69.450	0.300	0.016	0.056	0.091	303.266	1.787
36	0.363	0.302	68.165	0.377	0.052	0.219	0.295	369.005	2.910
37	0.349	0.311	83.616	0.408	0.044	0.209	0.311	478.957	3.737
38	0.334	0.316	73.015	0.394	0.042	0.195	0.284	424.433	3.396
39	0.377	0.293	17.496	0.259	0.093	0.191	0.292	85.111	1.259
40	0.154	0.123	31.337	0.360	0.016	0.033	0.058	137.452	2.922
41	0.155	0.120	44.422	0.320	0.010	0.037	0.061	224.235	2.390
42	0.227	0.165	11.027	0.270	0.029	0.076	0.109	80.816	1.565
43	0.255	0.255	33.511	0.334	0.026	0.107	0.171	194.240	2.452
44	0.209	0.129	20.799	0.280	0.026	0.060	0.102	100.045	1.762
45	0.253	0.159	10.847	0.290	0.056	0.080	0.103	53.801	1.446
46	0.317	0.254	9.439	0.232	0.058	0.141	0.240	68.197	1.174
47	0.436	0.318	35.395	0.324	0.115	0.280	0.420	170.562	2.199
48	0.974	0.334	4.159	0.204	0.852	0.945	0.784	8.047	0.571
49	0.372	0.298	35.316	0.314	0.074	0.231	0.414	206.100	2.662
50	0.791	0.300	8.528	0.188	0.627	0.663	0.529	24.912	0.511
51	0.225	0.170	22.277	0.313	0.034	0.068	0.114	101.540	2.151
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2	0.395	0.337	26.292	0.304	0.106	0.215	0.343	119.503	1.779
3	0.345	0.208	27.427	0.291	0.095	0.150	0.229	104.142	1.671
4	0.481	0.370	49.783	0.340	0.141	0.339	0.471	228.326	2.284
5	0.717	0.172	0.717	0.165	0.476	0.494	0.292	-2.452	0.350
6	0.360	0.183	26.541	0.277	0.083	0.154	0.221	89.651	1.407
7	0.420	0.192	75.210	0.252	0.135	0.181	0.207	215.113	0.927
8	0.114	0.110	38.262	0.407	0.008	0.019	0.049	180.146	5.047
9	0.242	0.132	15.827	0.287	0.046	0.076	0.105	73.711	1.611
10	0.363	0.333	33.399	0.348	0.076	0.189	0.303	155.409	2.388
11	0.545	0.457	35.031	0.288	0.193	0.368	0.588	125.531	1.531
12	0.664	0.437	23.027	0.275	0.240	0.730	0.921	150.513	1.489
13	0.589	0.286	-5.813	0.161	0.347	0.429	0.381	9.752	0.395
14	0.568	0.184	26.758	0.252	0.283	0.309	0.258	53.829	0.861
15	0.297	0.218	30.931	0.323	0.053	0.124	0.194	140.585	2.194
16	0.290	0.329	105.626	0.537	0.032	0.148	0.425	646.131	9.678
17	0.393	0.341	45.084	0.379	0.096	0.269	0.401	266.984	3.148
18	0.594	0.180	30.718	0.252	0.316	0.331	0.285	60.140	0.880
19	0.569	0.351	21.800	0.248	0.239	0.421	1.604	92.936	3.043
20	0.523	0.311	-7.988	0.163	0.232	0.306	0.414	-5.200	0.449
21	0.543	0.371	39.201	0.218	0.241	0.362	0.570	137.911	0.872
22	0.546	0.364	37.232	0.277	0.195	0.408	0.621	157.810	1.634
23	0.873	0.447	13.886	0.235	0.691	0.832	0.948	41.574	0.896
24	0.341	0.238	48.851	0.314	0.055	0.157	0.237	200.304	1.940
25	0.440	0.311	38.254	0.292	0.125	0.259	0.359	156.080	1.601
26	0.524	0.447	84.399	0.402	0.138	0.440	0.790	445.200	3.938
27	0.431	0.279	31.785	0.299	0.136	0.222	0.294	107.420	1.554
28	0.362	0.304	49.502	0.326	0.067	0.191	0.295	224.935	2.304
29	0.165	0.136	80.958	0.391	0.015	0.035	0.074	323.417	3.489
30	0.391	0.288	50.280	0.329	0.069	0.237	0.307	251.364	2.052
31	0.551	0.257	16.638	0.248	0.216	0.402	0.423	80.139	1.007
32	0.322	0.285	28.080	0.346	0.058	0.168	0.298	165.452	2.882
33	0.482	0.297	40.044	0.252	0.141	0.354	0.464	199.146	1.251
34	0.407	0.307	44.513	0.228	0.099	0.252	0.444	217.488	1.200
35	0.767	0.275	3.142	0.177	0.594	0.632	0.378	14.077	0.420
36	0.364	0.139	24.614	0.263	0.095	0.133	0.144	56.210	0.992
37	0.425	0.219	19.227	0.263	0.137	0.223	0.314	75.266	1.328
38	0.403	0.274	22.733	0.279	0.113	0.232	0.333	114.462	1.583
39	0.264	0.252	33.935	0.365	0.031	0.116	0.252	198.855	3.979
40	0.223	0.159	28.928	0.341	0.039	0.065	0.143	118.067	3.175
41	0.256	0.244	28.024	0.377	0.031	0.105	0.236	163.323	4.077
42	0.381	0.243	32.272	0.299	0.085	0.197	0.259	138.150	1.661
43	0.385	0.313	55.871	0.369	0.082	0.234	0.360	283.973	3.034
44	0.241	0.245	92.100	0.448	0.020	0.098	0.167	521.985	4.429
45	0.308	0.213	43.675	0.325	0.043	0.134	0.208	190.504	2.243
46	0.276	0.227	25.543	0.336	0.051	0.108	0.209	122.525	2.754
47	0.703	0.413	20.526	0.276	0.370	0.689	0.789	102.406	1.304
48	0.387	0.315	34.960	0.321	0.076	0.237	0.340	188.784	2.155
49	1.246	0.507	5.409	0.190	1.456	1.771	1.521	26.783	0.528
50	1.290	0.436	2.759	0.174	1.617	1.792	1.226	13.602	0.418
51	0.520	0.377	23.268	0.304	0.197	0.380	0.577	113.641	1.815
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2	0.978	0.554	22.089	0.237	0.888	1.297	1.236	102.055	0.872
3	0.793	0.359	-1.413	0.201	0.561	0.741	0.666	14.568	0.599
4	0.371	0.370	78.107	0.406	0.058	0.229	0.371	427.990	3.659
5	0.320	0.265	29.756	0.313	0.050	0.157	0.273	158.021	2.246
6	0.414	0.326	51.809	0.338	0.073	0.248	0.370	232.553	2.444
7	0.395	0.282	28.826	0.291	0.104	0.216	0.310	129.108	1.660
8	0.349	0.308	36.082	0.359	0.061	0.192	0.311	192.483	2.890
9	0.566	0.434	35.500	0.307	0.218	0.438	0.681	150.907	1.871
10	0.201	0.237	57.108	0.454	0.011	0.091	0.499	454.480	15.975
11	0.572	0.377	61.654	0.298	0.184	0.483	0.553	285.505	1.644
12	0.450	0.243	6.697	0.256	0.150	0.274	0.309	54.358	1.170
13	0.423	0.363	49.203	0.329	0.083	0.279	0.447	246.705	2.375
14	0.270	0.257	52.916	0.353	0.041	0.090	0.158	189.102	2.229
15	0.677	0.576	15.981	0.220	0.295	0.543	0.734	59.595	0.760
16	0.615	0.430	6.457	0.213	0.291	0.469	0.609	40.678	0.786
17	0.717	0.438	1.433	0.223	0.383	0.619	0.769	23.782	0.812
18	0.394	0.224	31.241	0.284	0.101	0.197	0.275	118.561	1.495
19	0.501	0.363	15.854	0.284	0.148	0.372	0.510	98.952	1.638
20	0.416	0.481	32.256	0.425	-0.035	0.396	3.326	301.410	22.151
21	0.517	0.364	10.600	0.245	0.156	0.394	0.477	79.837	1.090
22	0.474	0.330	1.492	0.255	0.155	0.349	0.439	60.040	1.264
23	0.443	0.394	72.470	0.383	0.091	0.325	0.686	393.159	4.508
24	0.717	0.244	-0.307	0.223	0.459	0.548	0.439	5.803	0.691
25	0.631	0.386	13.614	0.279	0.315	0.503	0.598	63.297	1.292
26	0.436	0.294	51.879	0.336	0.092	0.240	0.339	190.884	1.993
27	0.492	0.408	42.402	0.337	0.126	0.340	0.542	184.095	2.209
28	0.552	0.458	60.888	0.351	0.111	0.581	0.852	393.852	2.740
29	0.518	0.409	38.234	0.316	0.150	0.401	0.663	185.284	2.293
30	0.418	0.324	58.963	0.335	0.073	0.282	0.490	307.733	2.848
31	0.529	0.450	11.413	0.276	0.194	0.421	0.745	86.600	1.692
32	0.609	0.623	80.026	0.459	0.130	0.591	1.244	415.731	5.422
33	0.409	0.258	14.050	0.259	0.115	0.203	0.303	57.781	1.302
34	0.498	0.281	25.777	0.277	0.205	0.274	0.301	75.337	1.155
35	0.297	0.299	40.100	0.372	0.042	0.133	0.260	195.973	3.215
36	0.297	0.221	17.446	0.320	0.050	0.129	0.218	100.845	2.327
37	0.380	0.315	37.038	0.330	0.069	0.253	0.385	228.068	2.567
38	0.171	0.152	34.278	0.350	0.015	0.043	0.100	163.667	3.608
39	0.611	0.415	58.447	0.307	0.181	0.614	0.818	313.327	1.864
40	0.594	0.462	60.049	0.326	0.204	0.578	0.816	319.459	2.242
41	0.424	0.366	38.583	0.340	0.107	0.296	0.508	215.801	2.702
42	0.486	0.372	32.390	0.297	0.110	0.312	0.450	131.456	1.699
43	0.513	0.295	16.990	0.278	0.186	0.333	0.424	73.202	1.443
44	0.511	0.407	46.090	0.352	0.083	0.447	0.953	264.583	4.138
45	0.653	0.286	64.988	0.297	0.187	0.566	0.711	260.920	1.612
46	0.397	0.269	54.190	0.324	0.089	0.203	0.300	205.775	2.049
47	0.742	0.476	10.353	0.216	0.421	0.637	0.722	40.798	0.712
48	0.478	0.451	59.272	0.379	0.099	0.390	0.685	332.115	3.557
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STROBE Statement—Checklist of items that should be included in reports of *cohort studies*

	Item No	Recommendation	Page No
Title and abstract	1	(a) Indicate the study's design with a commonly used term in the title or the abstract	1
		(b) Provide in the abstract an informative and balanced summary of what was done and what was found	2
Introduction			
Background/rationale	2	Explain the scientific background and rationale for the investigation being reported	3
Objectives	3	State specific objectives, including any prespecified hypotheses	3-4
Methods			
Study design	4	Present key elements of study design early in the paper	5-8
Setting	5	Describe the setting, locations, and relevant dates, including periods of recruitment, exposure, follow-up, and data collection	n.a.
Participants	6	(a) Give the eligibility criteria, and the sources and methods of selection of participants. Describe methods of follow-up (b) For matched studies, give matching criteria and number of exposed and unexposed	n.a.
Variables	7	Clearly define all outcomes, exposures, predictors, potential confounders, and effect modifiers. Give diagnostic criteria, if applicable	6-8
Data sources/ measurement	8*	For each variable of interest, give sources of data and details of methods of assessment (measurement). Describe comparability of assessment methods if there is more than one group	5
Bias	9	Describe any efforts to address potential sources of bias	13
Study size	10	Explain how the study size was arrived at	5
Quantitative variables	11	Explain how quantitative variables were handled in the analyses. If applicable, describe which groupings were chosen and why	6-7
Statistical methods	12	(a) Describe all statistical methods, including those used to control for confounding	8
		(b) Describe any methods used to examine subgroups and interactions	8
		(c) Explain how missing data were addressed	n.a.
		(d) If applicable, explain how loss to follow-up was addressed	n.a.
		(e) Describe any sensitivity analyses	5-8
Results			
Participants	13*	(a) Report numbers of individuals at each stage of study—eg numbers potentially eligible, examined for eligibility, confirmed eligible, included in the study, completing follow-up, and analysed	5
		(b) Give reasons for non-participation at each stage	n.a.
		(c) Consider use of a flow diagram	n.a.
Descriptive data	14*	(a) Give characteristics of study participants (eg demographic, clinical, social) and information on exposures and potential confounders	n.a.
		(b) Indicate number of participants with missing data for each variable of interest	n.a.
		(c) Summarise follow-up time (eg, average and total amount)	n.a.
Outcome data	15*	Report numbers of outcome events or summary measures over time	n.a.

1	Main results	16	(a) Give unadjusted estimates and, if applicable, confounder-adjusted estimates and their precision (eg, 95% confidence interval). Make clear which confounders were adjusted for and why they were included	9-10
2			(b) Report category boundaries when continuous variables were categorized	n.a.
3			(c) If relevant, consider translating estimates of relative risk into absolute risk for a meaningful time period	n.a.
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6	Other analyses	17	Report other analyses done—eg analyses of subgroups and interactions, and sensitivity analyses	9-10
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11	Discussion			
12	Key results	18	Summarise key results with reference to study objectives	11
13	Limitations	19	Discuss limitations of the study, taking into account sources of potential bias or imprecision. Discuss both direction and magnitude of any potential bias	13
14				
15	Interpretation	20	Give a cautious overall interpretation of results considering objectives, limitations, multiplicity of analyses, results from similar studies, and other relevant evidence	13
16				
17	Generalisability	21	Discuss the generalisability (external validity) of the study results	11-12
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21	Other information			
22	Funding	22	Give the source of funding and the role of the funders for the present study and, if applicable, for the original study on which the present article is based	14
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*Give information separately for exposed and unexposed groups.

Note: An Explanation and Elaboration article discusses each checklist item and gives methodological background and published examples of transparent reporting. The STROBE checklist is best used in conjunction with this article (freely available on the Web sites of PLoS Medicine at <http://www.plosmedicine.org/>, Annals of Internal Medicine at <http://www.annals.org/>, and Epidemiology at <http://www.epidem.com/>). Information on the STROBE Initiative is available at <http://www.strobe-statement.org>.